

EXPLOITING NONLINEARITY IN VIBRATION CONTROL DEVICES

dr. ir. Kevin Dekemele

ABOUT ME: CAREER GHENT

- MA Electromechanical engineer: control engineering (2015)
- Teaching assistant (2015-2021)
 - 40 % Teaching (Dynamical systems/Vibrations)
 - 60 % Research
 - Promotor: professor Mia Loccufier
- Post-doc (04/2021-...)
 - Short-time projects (until 11/2022) & National Fellowship (11/2022 --)
 - Research stay in Budapest (Hungary) (02/2022-04/2022)
 - Research stay ENSAM Lille (France) (02/2023-02/2024)
- 2 PhD students + 3 Visiting from Southeast University /Tongji/ Lodz



ABOUT ME: BELGIUM



ABOUT ME: BELGIUM

Stoofvlees / Carbonade Flamand



Frietkot/
Baraque à frites



Belgian Beers



Moule frites



Matching beer glass (don't mix)



ABOUT ME: BELGIAN SWEETS

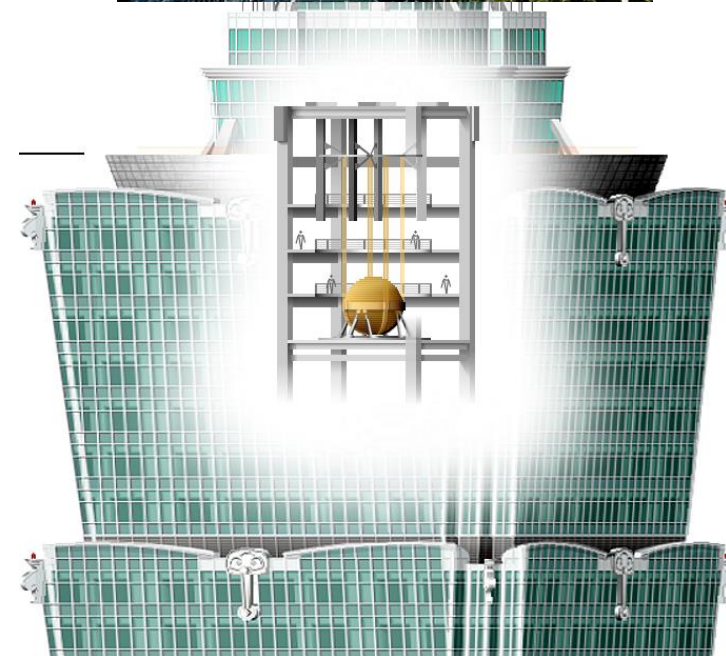
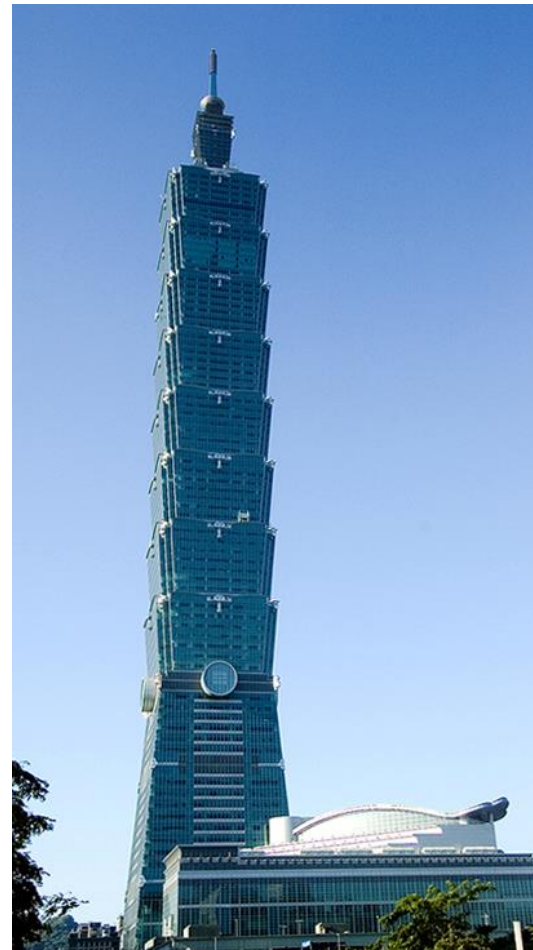
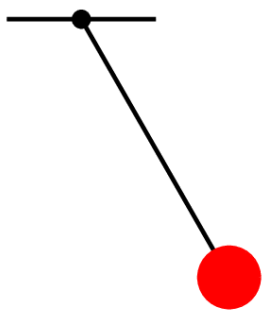


ABOUT ME: GHENT



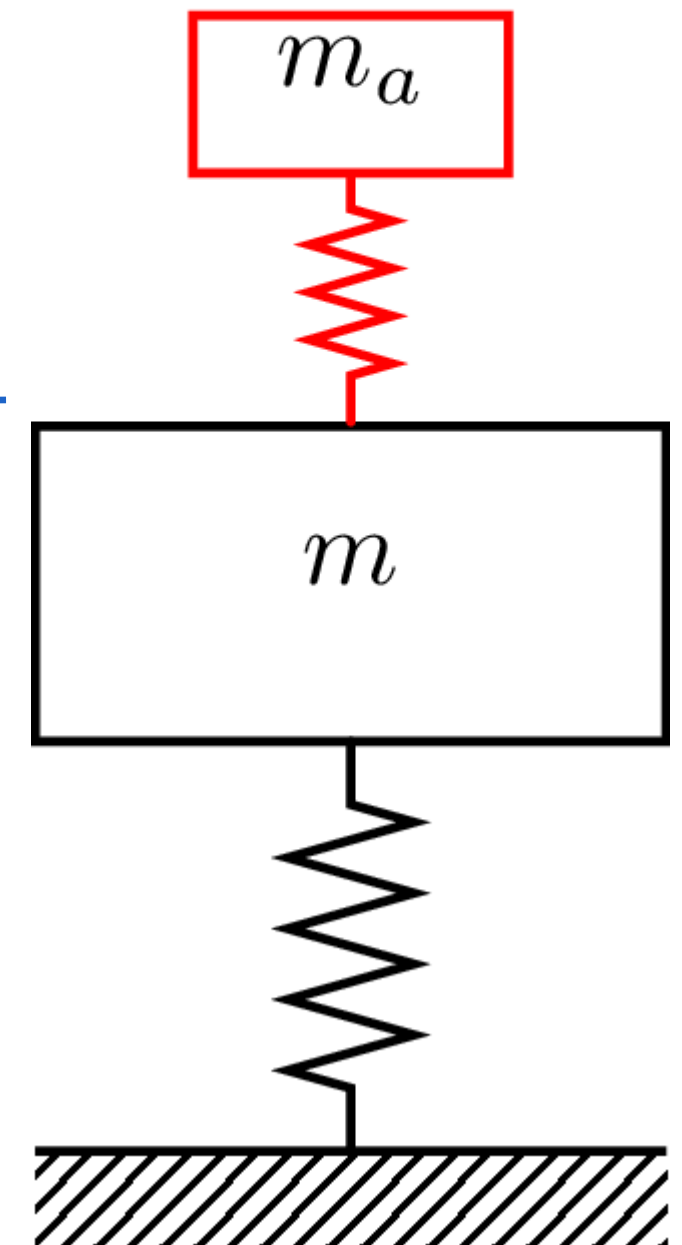
RESEARCH: NONLINEAR ENERGY SINK

DYNAMIC VIBRATION ABSORBER (DVA)



Auxiliary
system
DVA

Primary
system



ON-SITE VISITS

Millenium Bridge, London



GHENT
UNIVERSITY

Shanghai Tower, Shanghai



PROBLEM CONVENTIONAL DVA

- Sensitive to only 1 frequency
 1. Shifting vibration frequency?
 2. Multiple vibration frequencies?

PROBLEM CONVENTIONAL DVA

- Sensitive to only 1 frequency

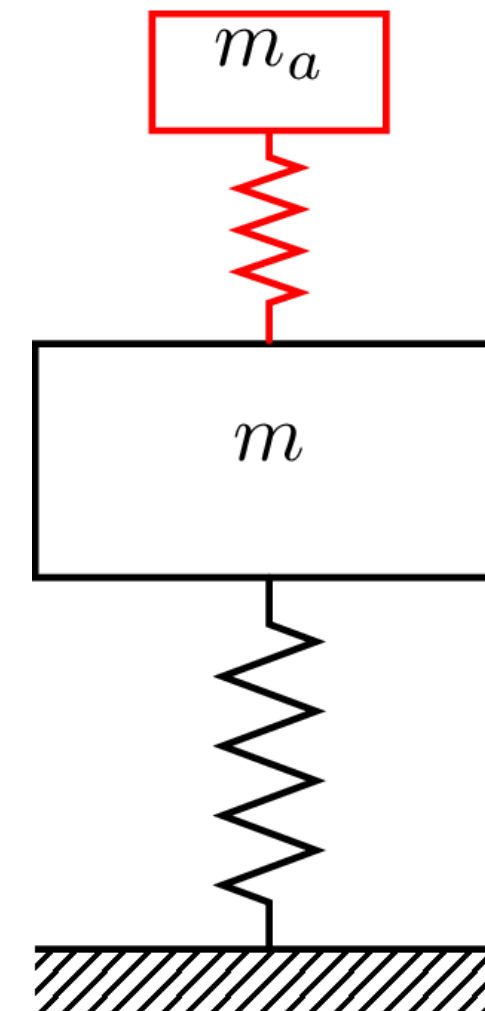
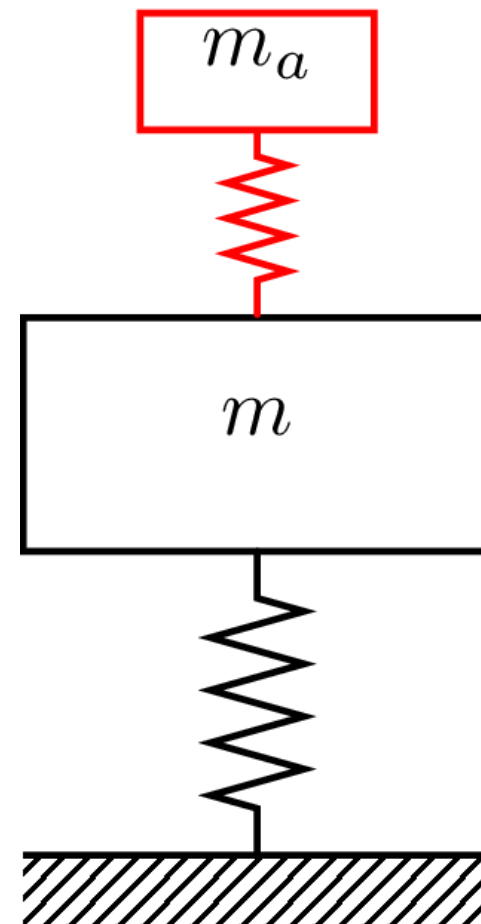
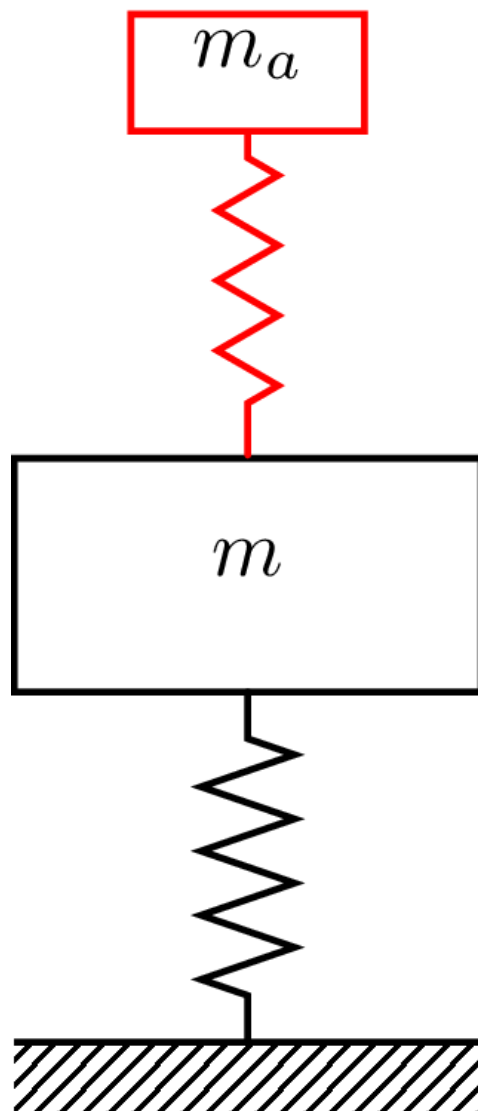
1. Shifting vibration frequency?

2. Multiple vibration frequencies?

$$f < f_{n,DVA}$$

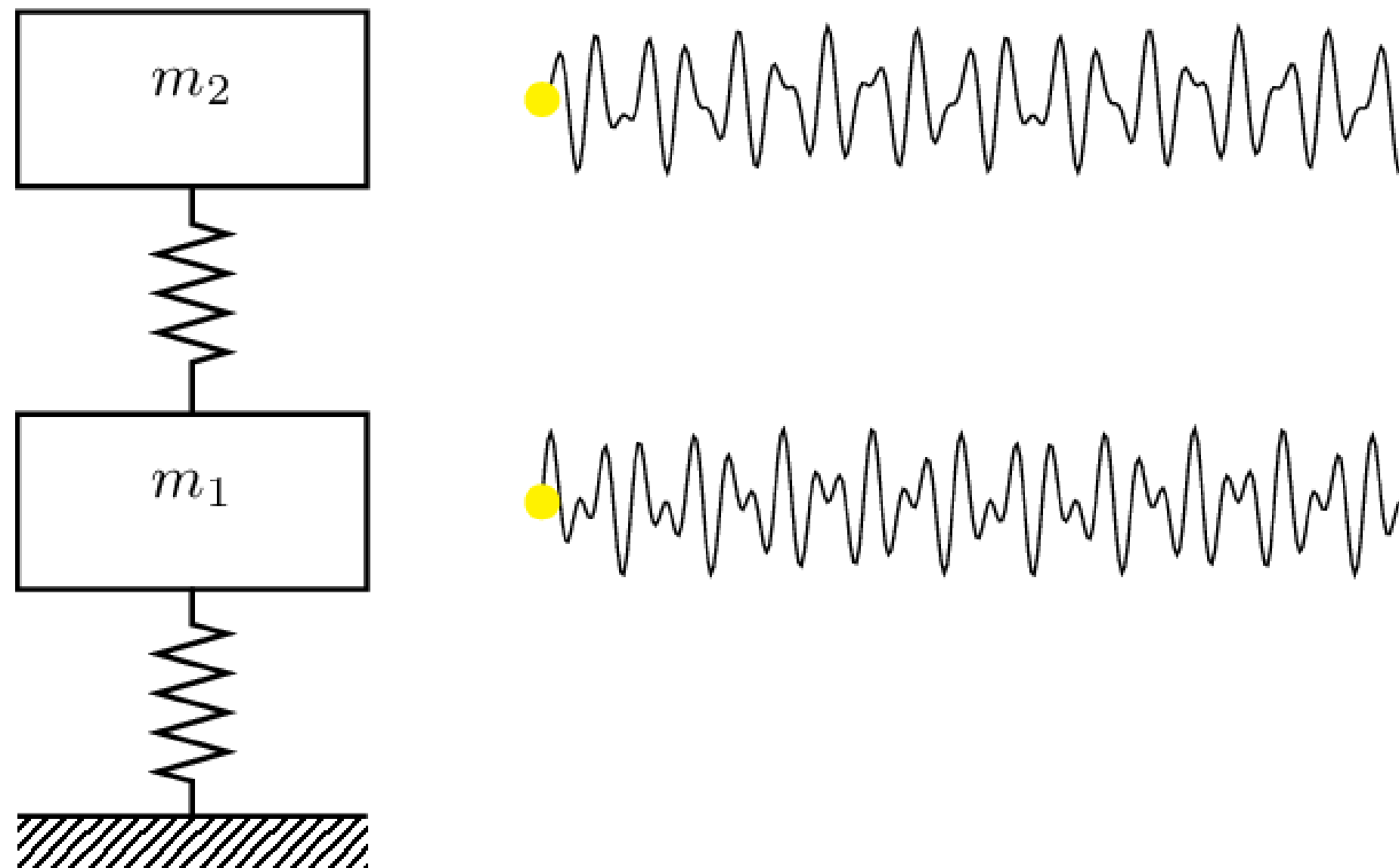
$$f \approx f_{n,DVA}$$

$$f > f_{n,DVA}$$



PROBLEM CONVENTIONAL DVA

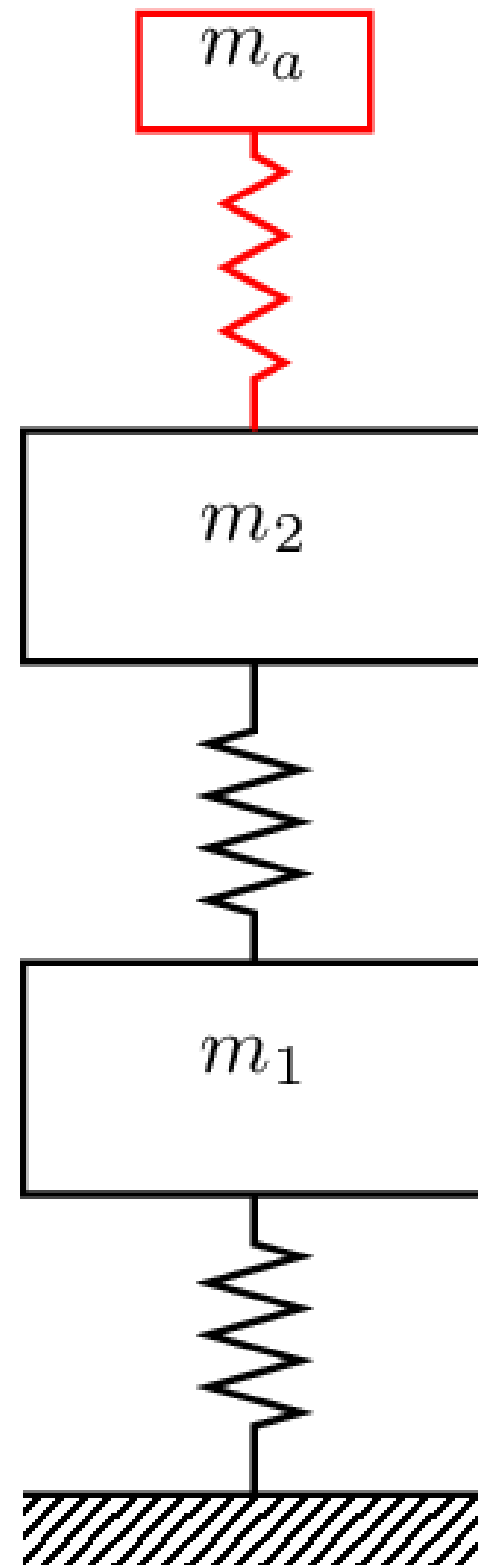
- Sensitive to only 1 frequency
 1. Shifting vibration frequency?
 2. Multiple vibration frequencies? $A_1 \sin(2\pi f_1 t + \phi_1) + A_2 \sin(2\pi f_2 t + \phi_2)$



ADD LINEAR DYNAMIC VIBRATION ABSORBER

$$f_{n,DVA} = f_2$$

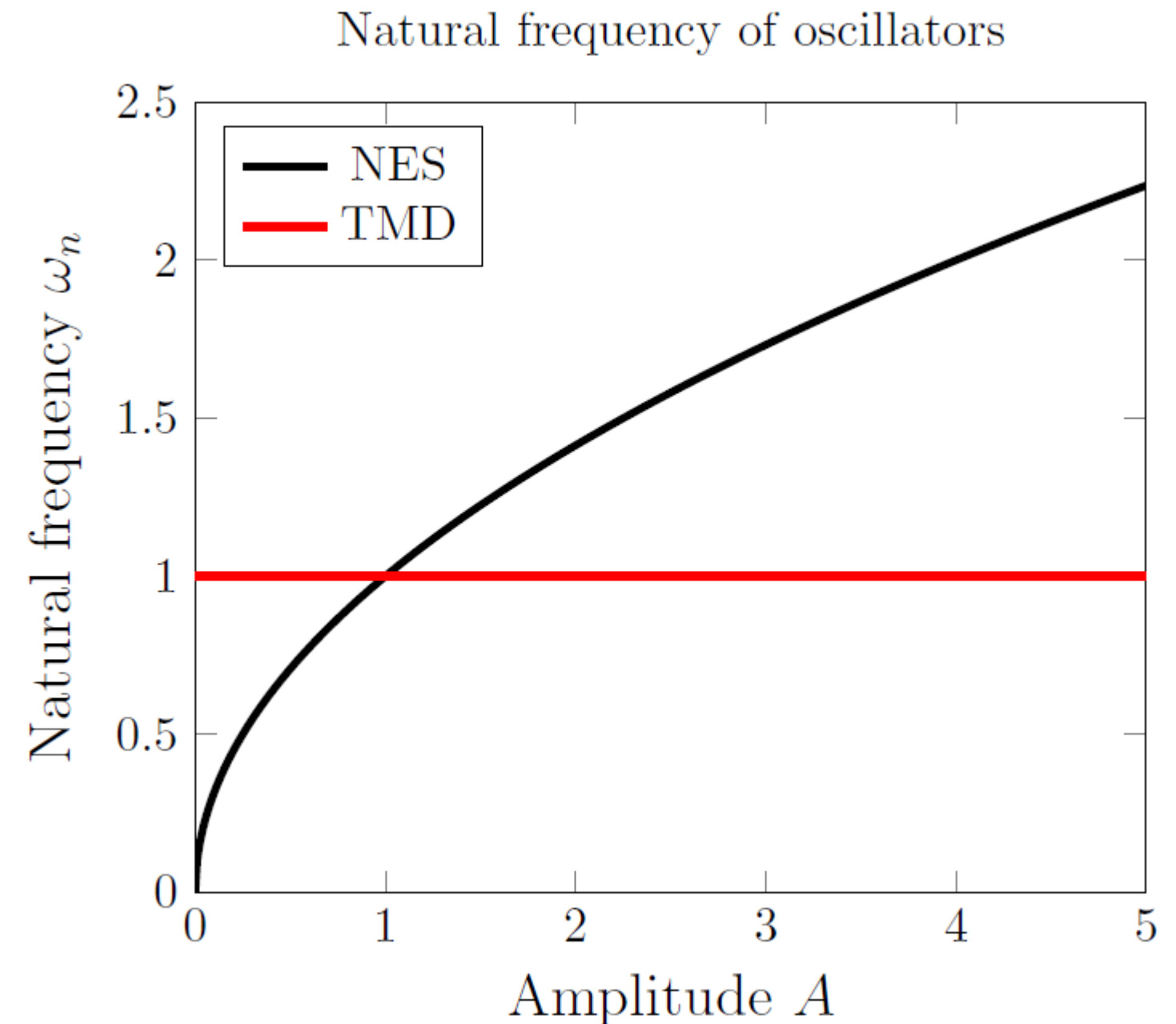
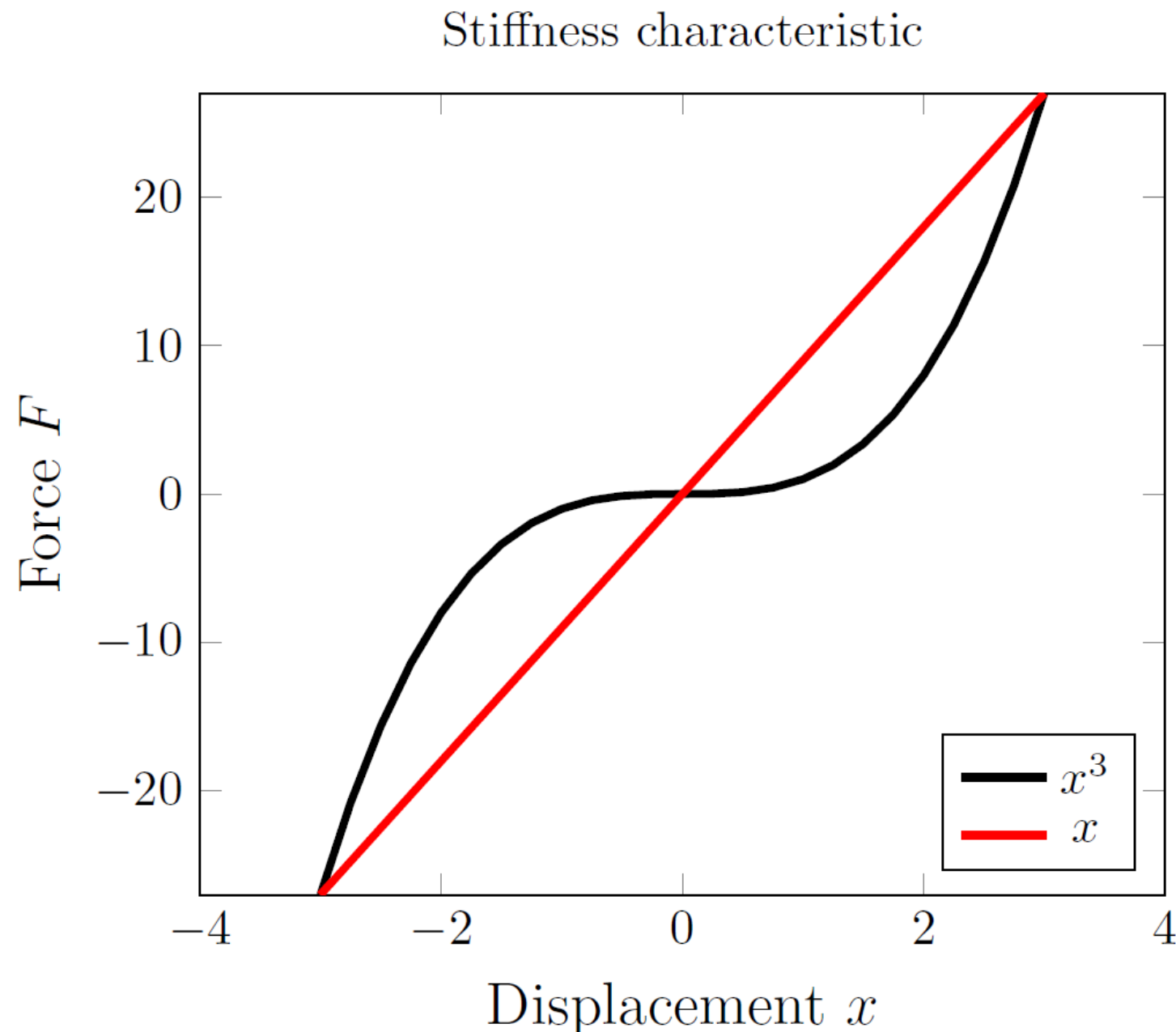
Primary
System



PROBLEM CONVENTIONAL DVA

- Reason: Hooke's law
- Nonlinear DVA: Nonlinear energy sink

$$f_{n,DVA} = \frac{1}{2\pi} \sqrt{\frac{k_a}{m_a}}$$

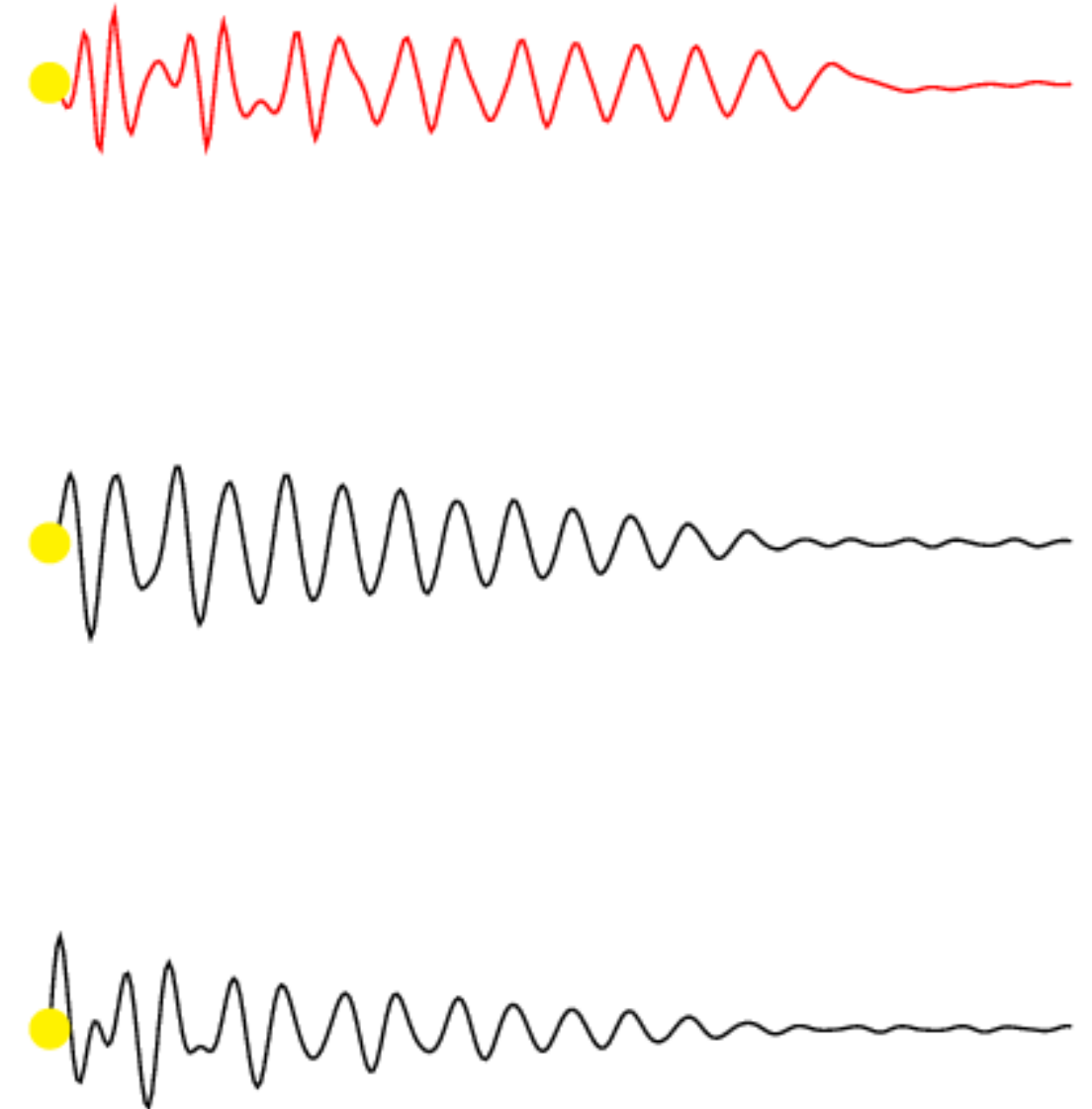
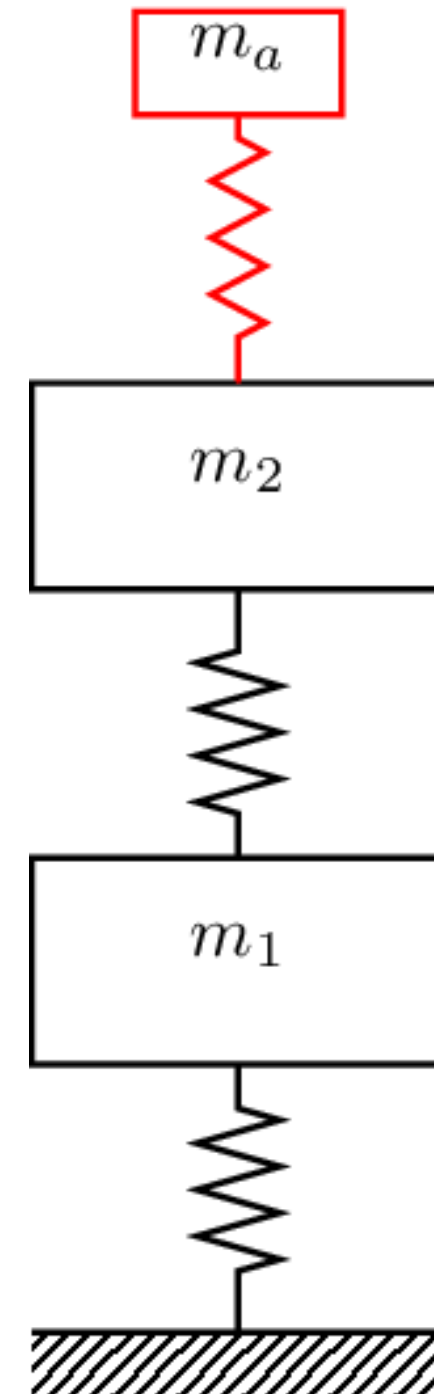


CONTENT

- **Resonance Capture Cascade (Transient Load)**
- Practical realization
- Harmonic load: Hardening
- Harmonic load: Softening
- Piezoelectrical NES

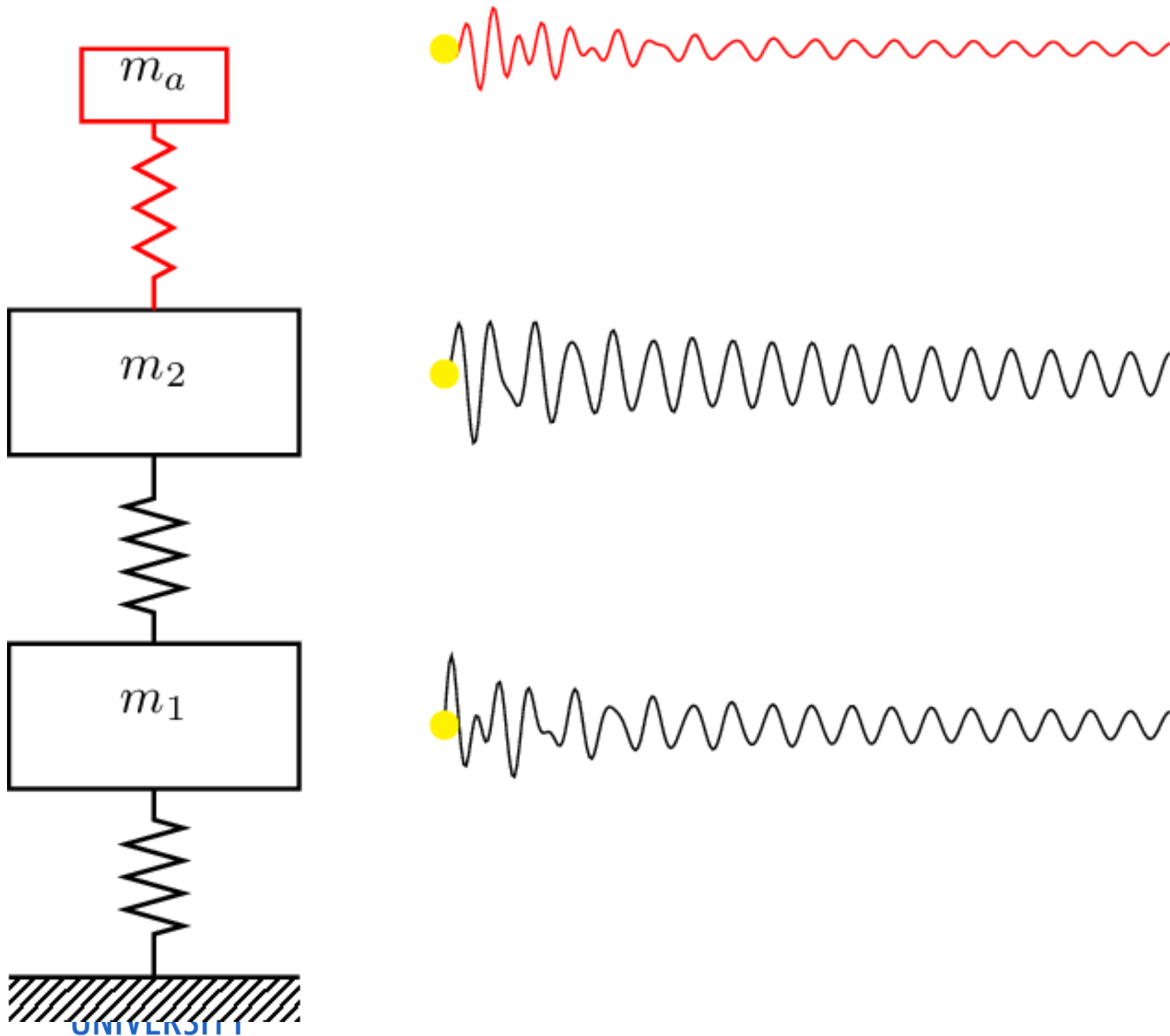
NONLINEAR ENERGY SINK (NES)

- Resonance capture cascade (RCC):
 - NES self-tunes to frequencies
 - Both frequencies damped

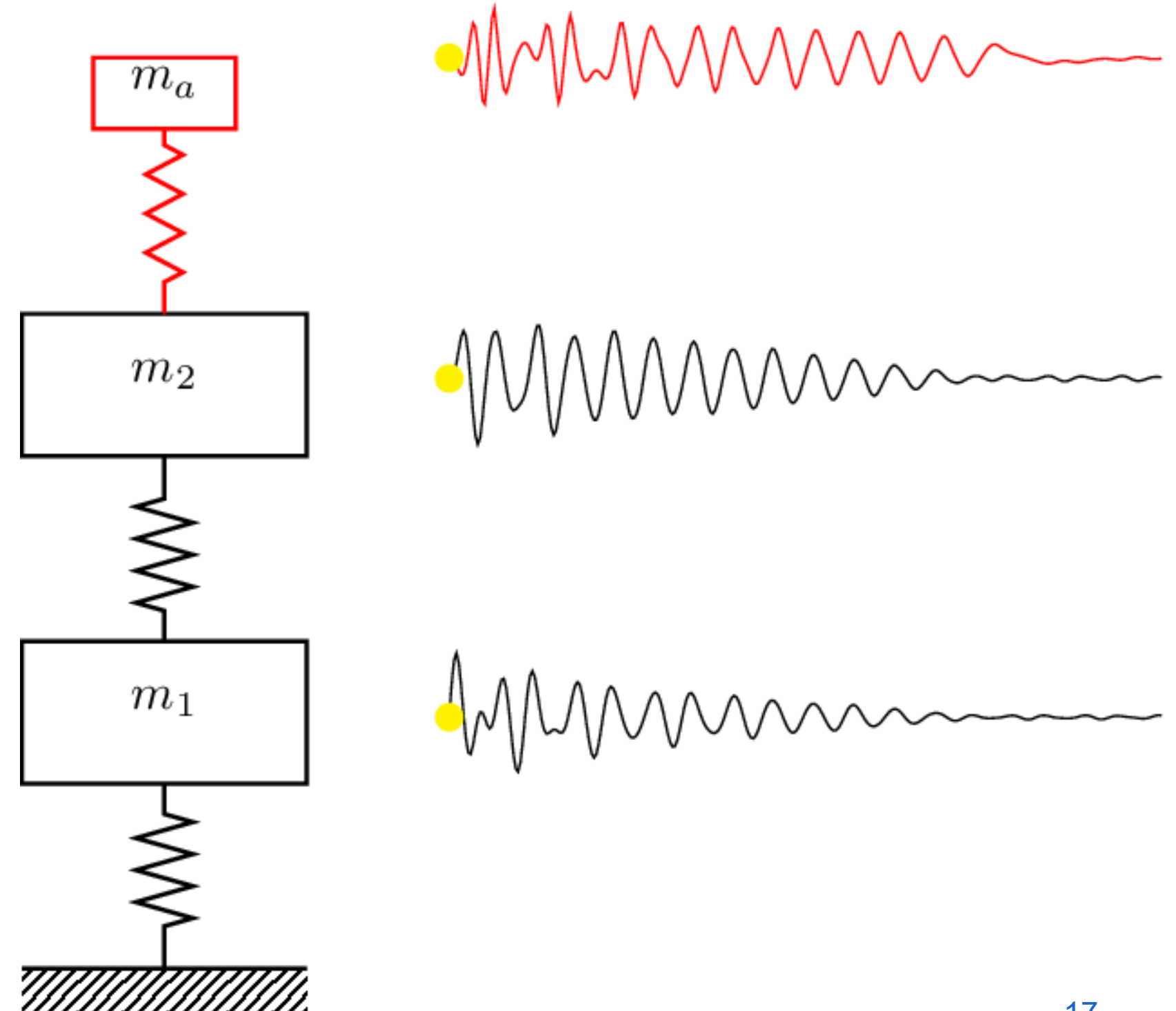


NONLINEAR ENERGY SINK

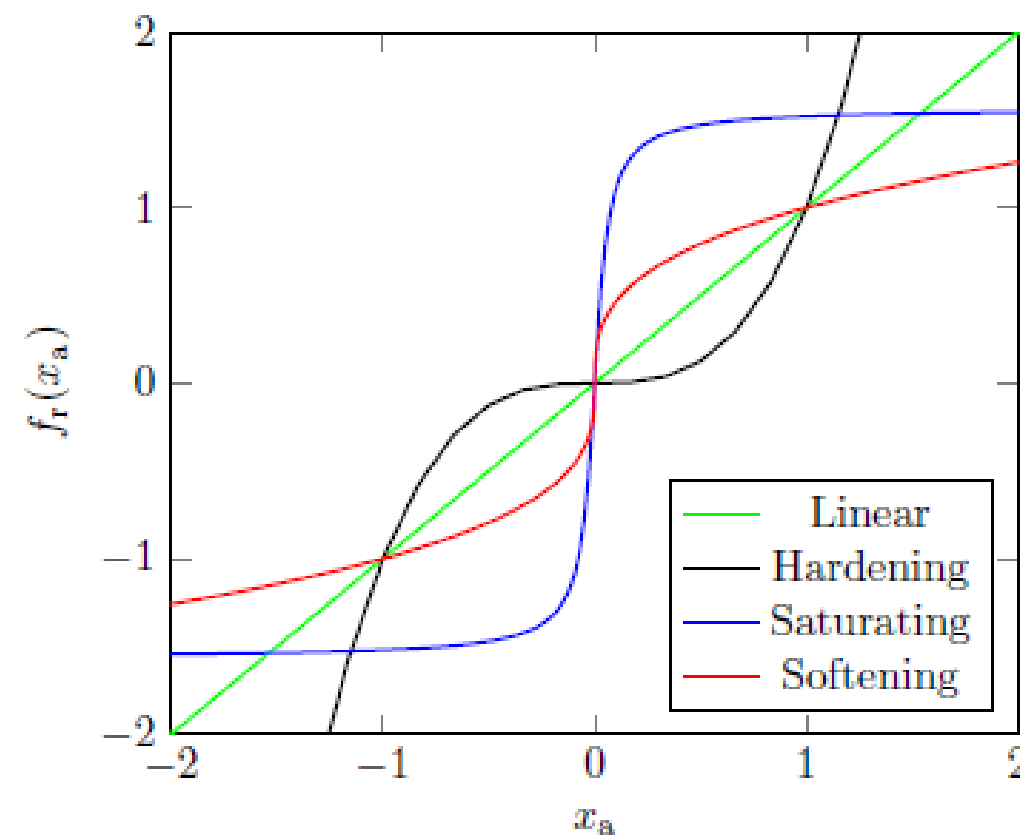
Conventional DVA



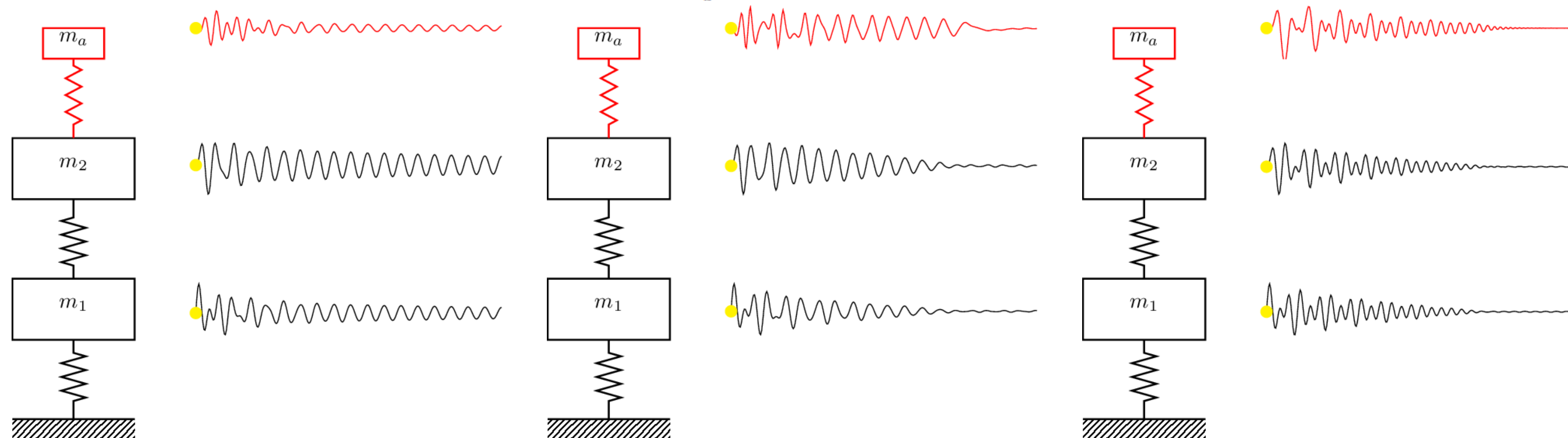
NES: RCC



SOFTENING SPRING

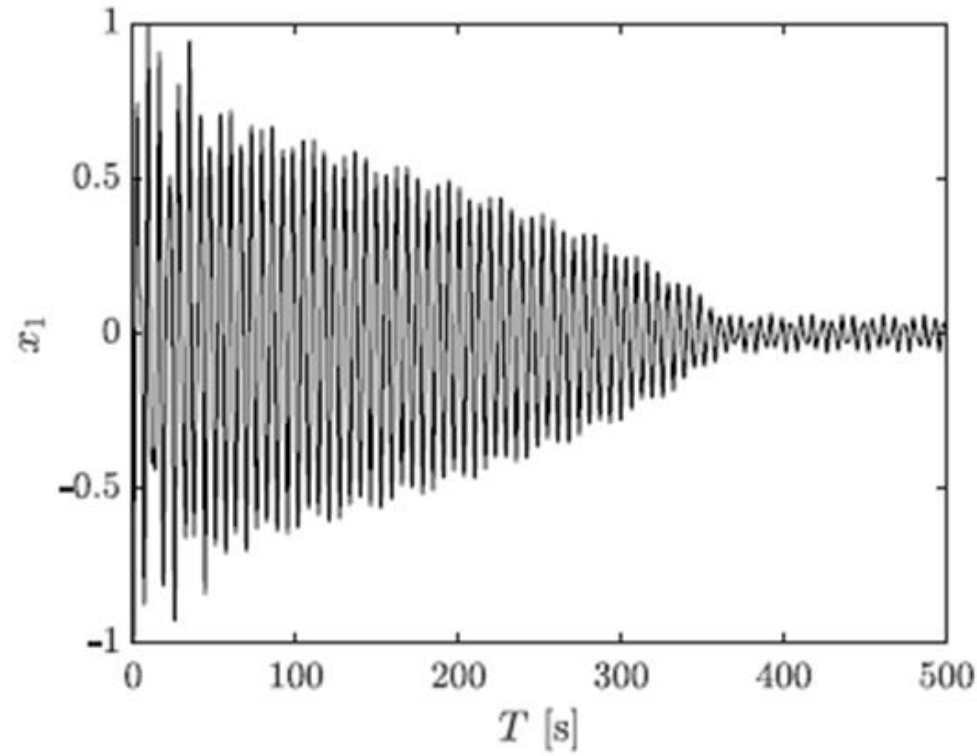


Softening Spring:
RCC from low to high
Frequency

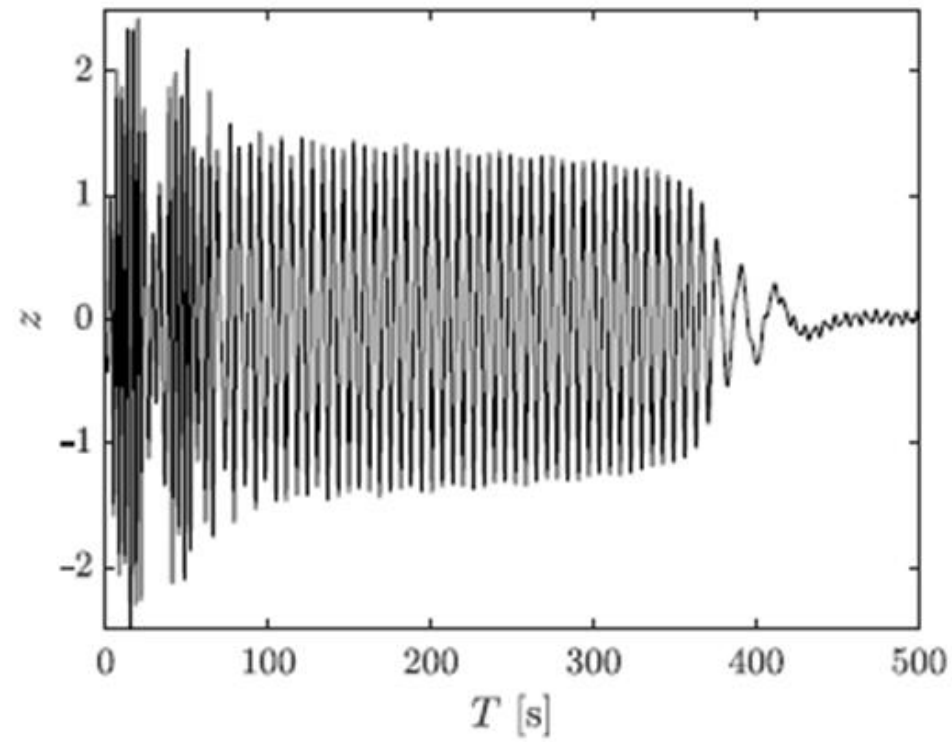


TIME SIMULATION HARDENING STIFFNESS

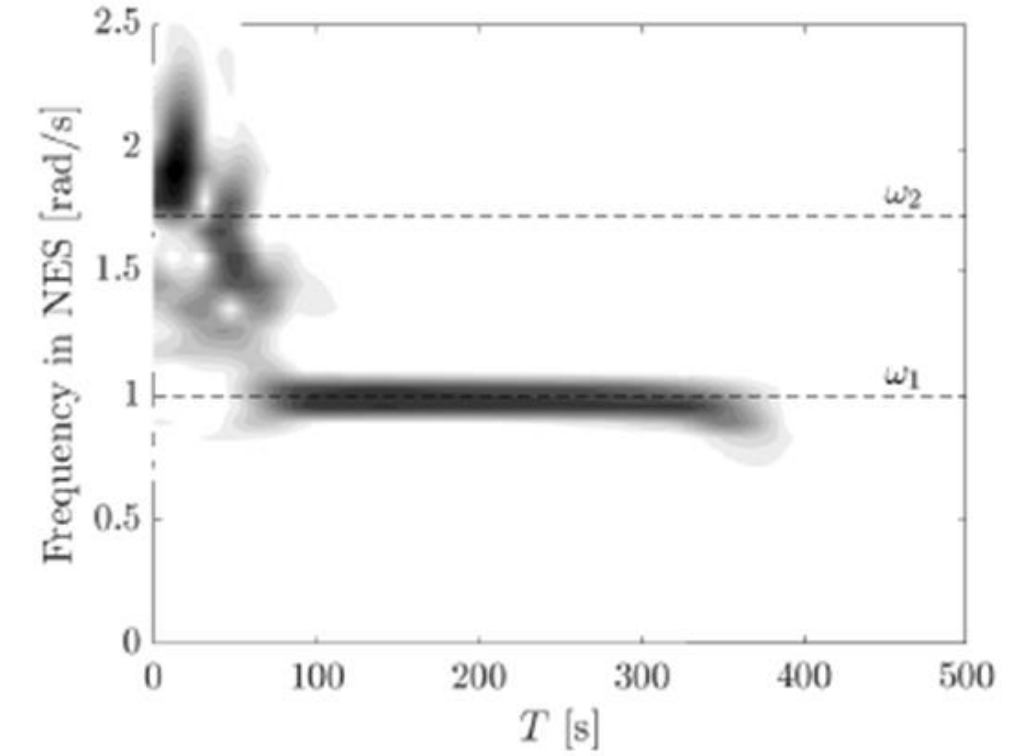
Physical vibrations x1



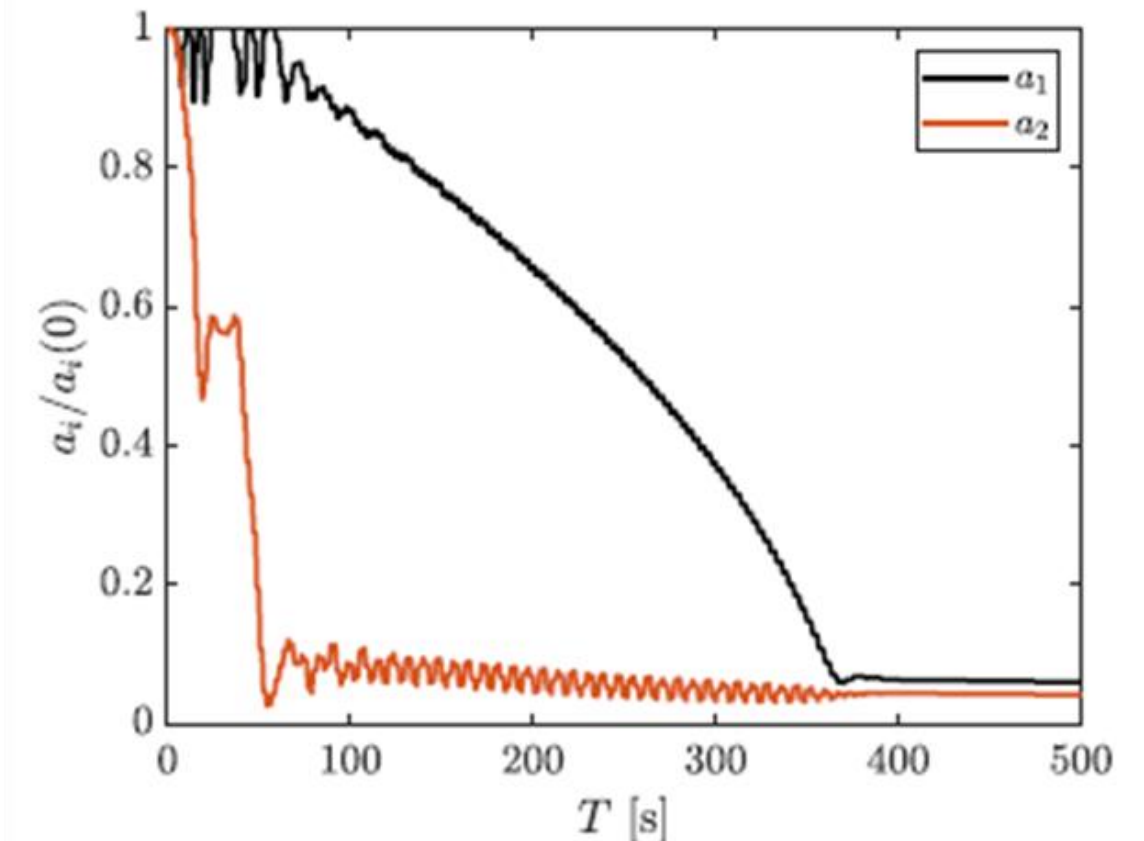
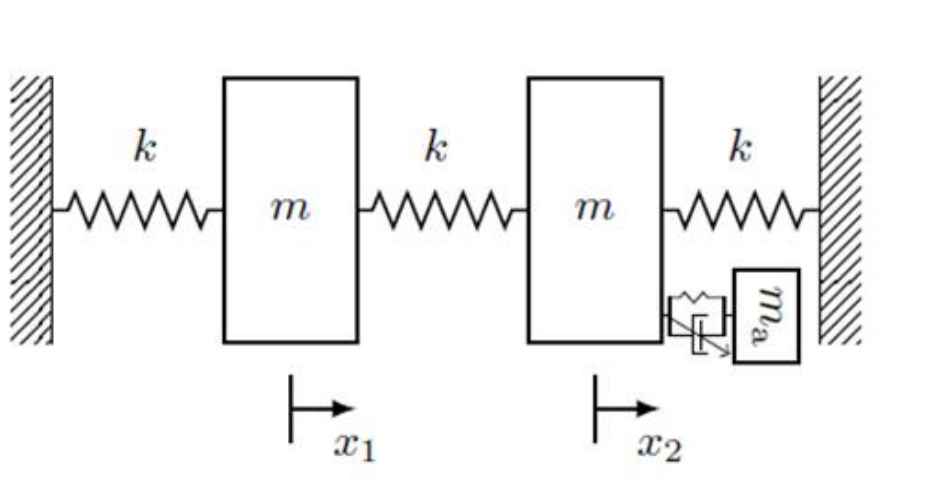
Relative absorber



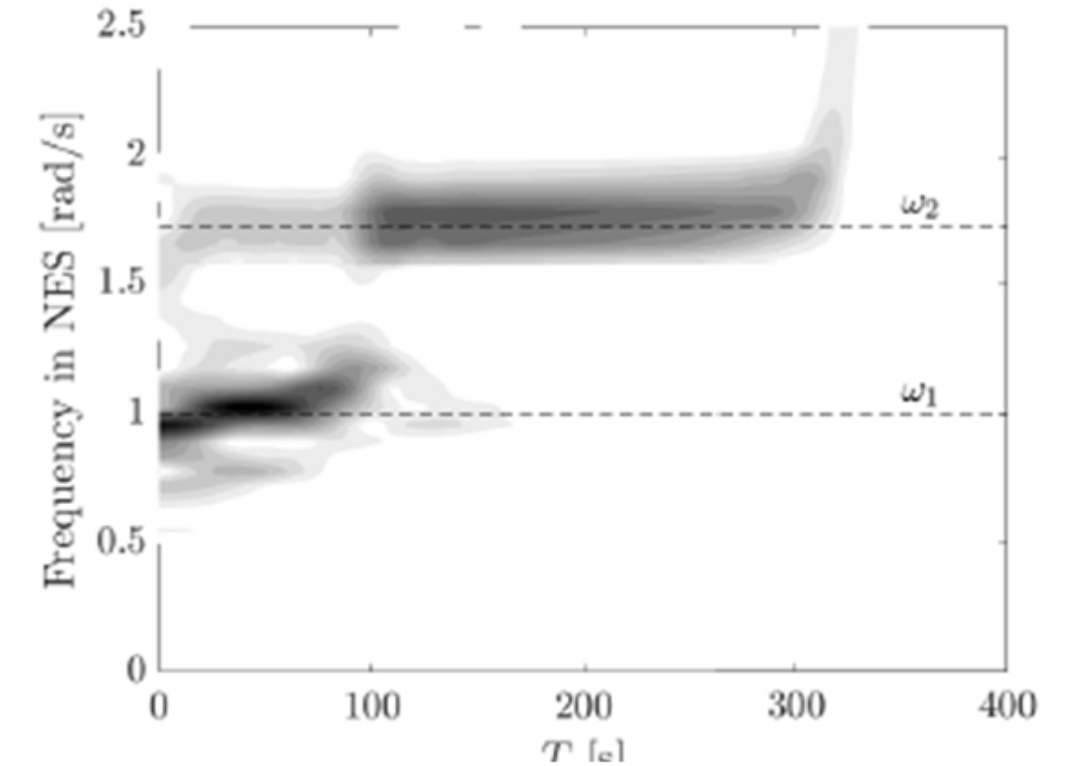
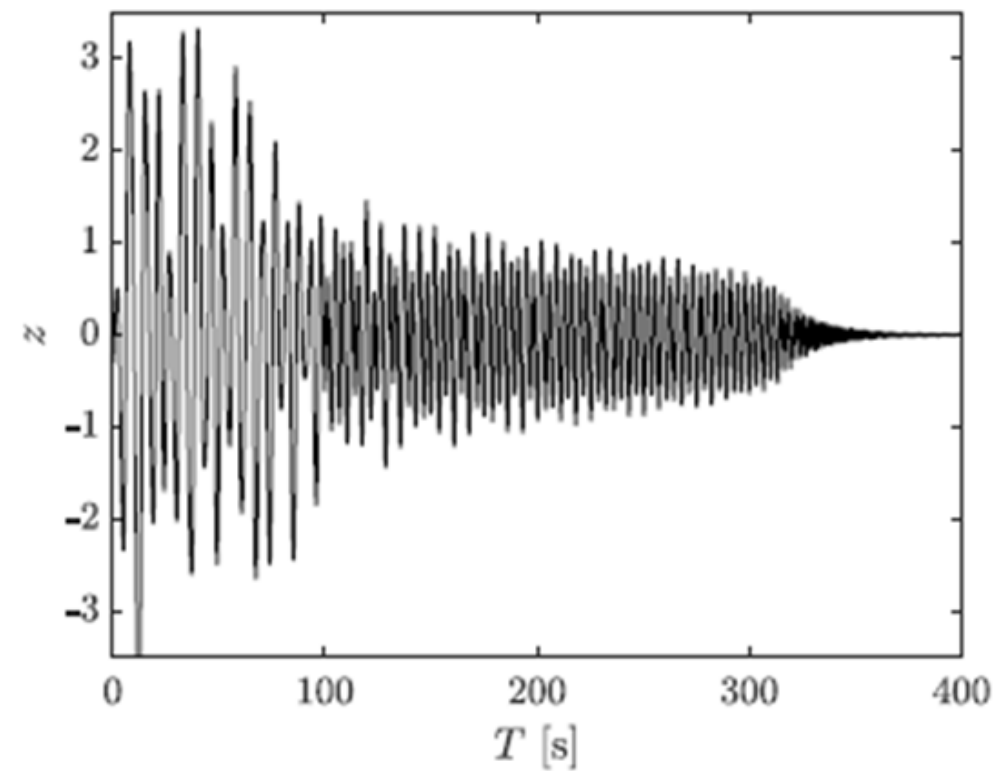
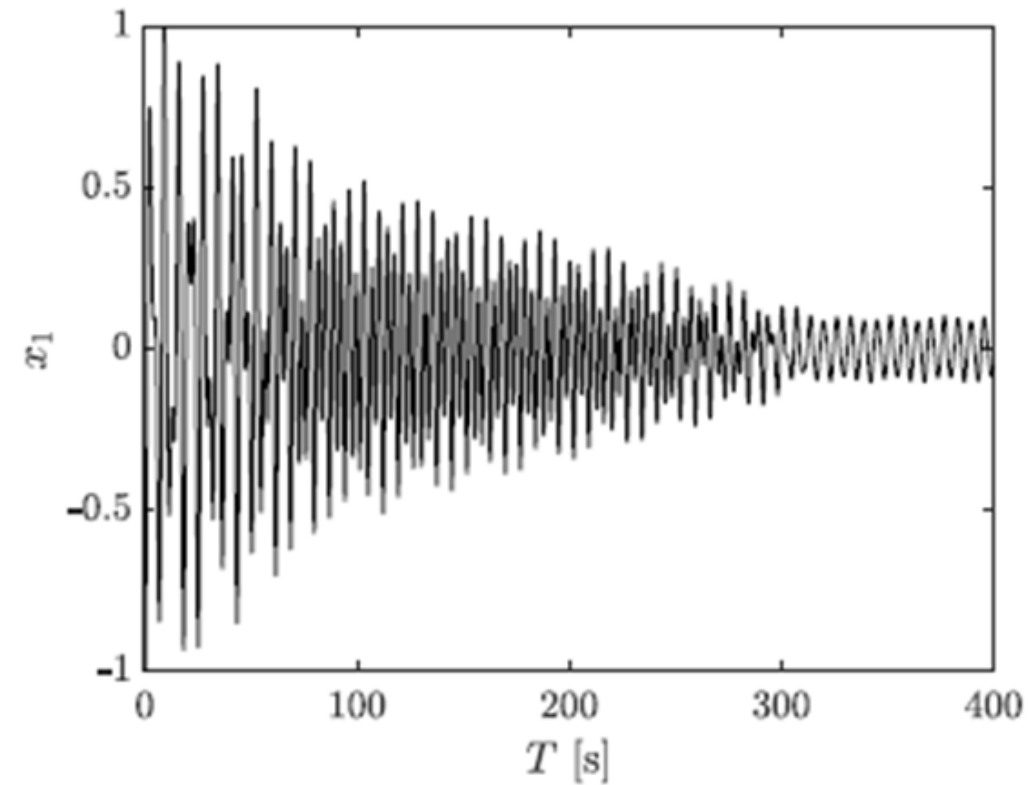
Wavelet absorber



Modal vibrations

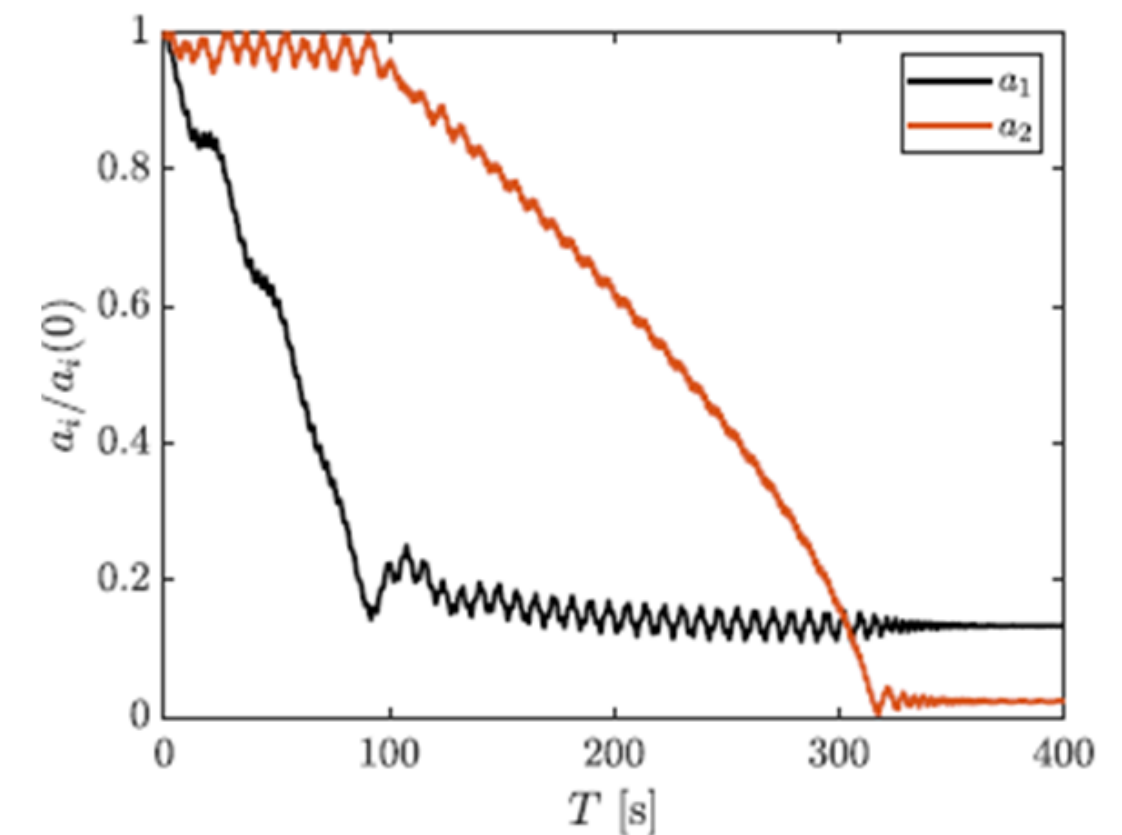


TIME SIMULATION SOFTENING STIFFNESS:



Modal vibrations

Dekemele, K., Habib, G. Inverted resonance capture cascade: modal interactions of a nonlinear energy sink with softening stiffness. *Nonlinear Dyn* **111**, 9839–9861 (2023).
<https://doi.org/10.1007/s11071-023-08423-9>

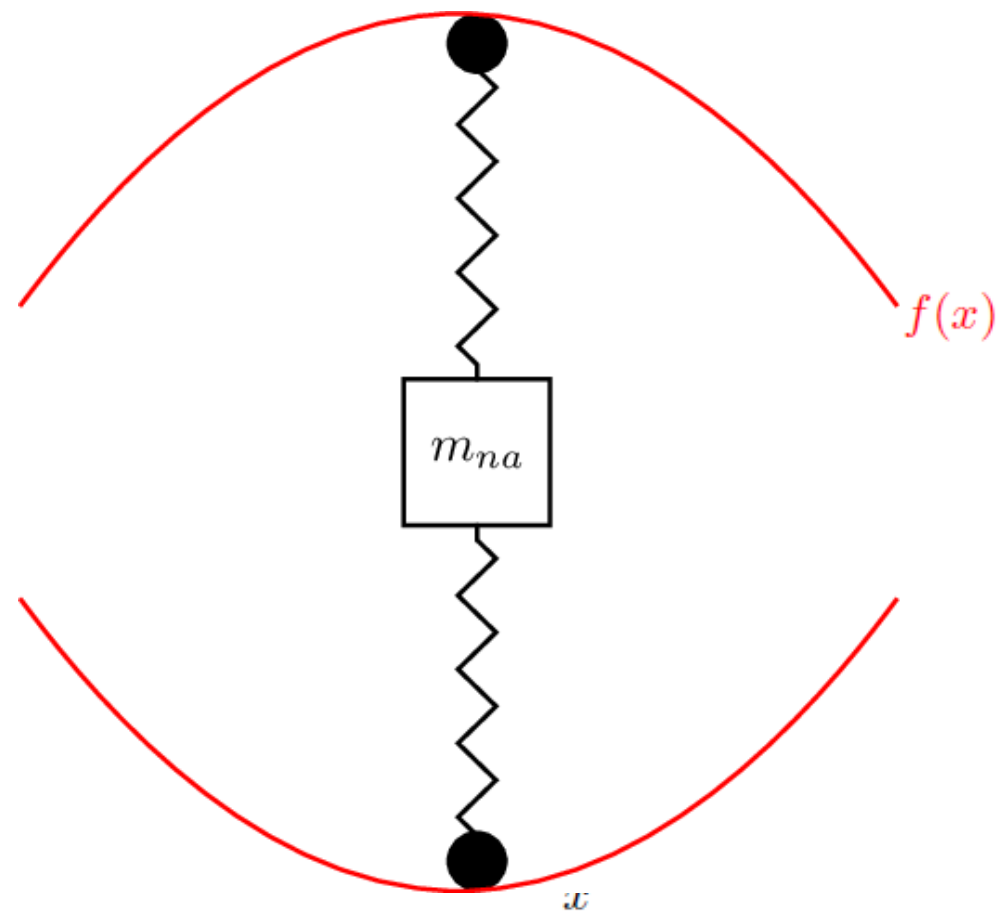


CONTENT

- Resonance Capture Cascade (Transient Load)
- **Practical realization**
- Harmonic load: Hardening
- Harmonic load: Softening
- Piezoelectrical NES

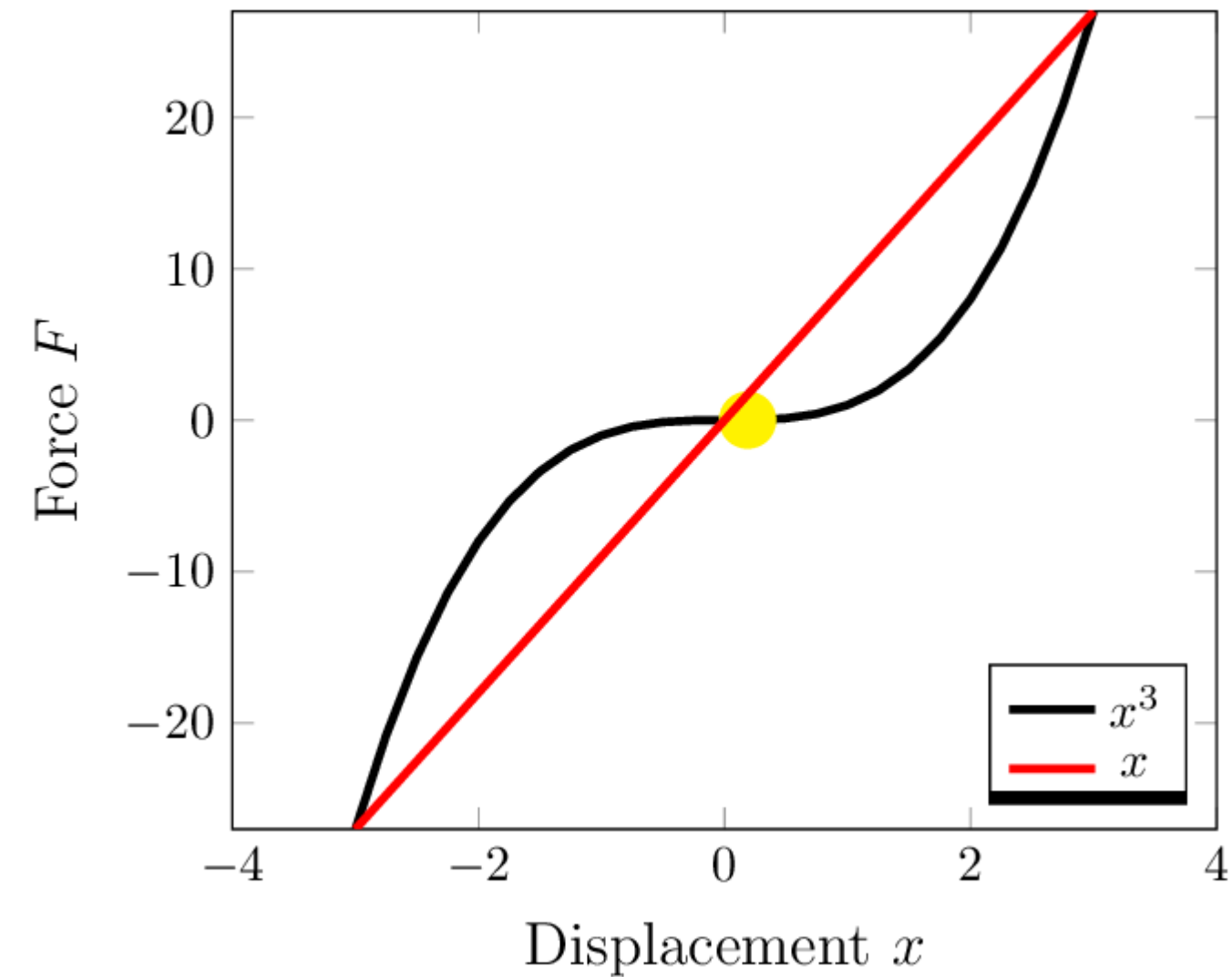
NES REALIZATION: GHENT UNIVERSITY

Mechanism



Result

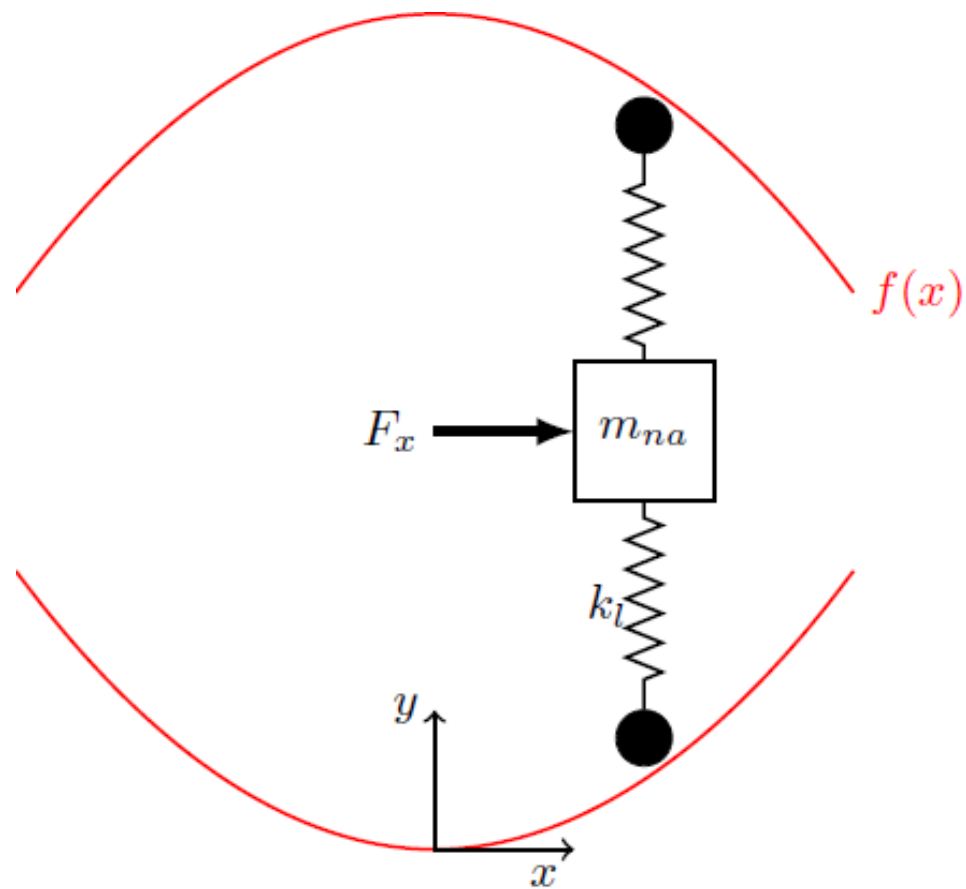
Stiffness characteristic



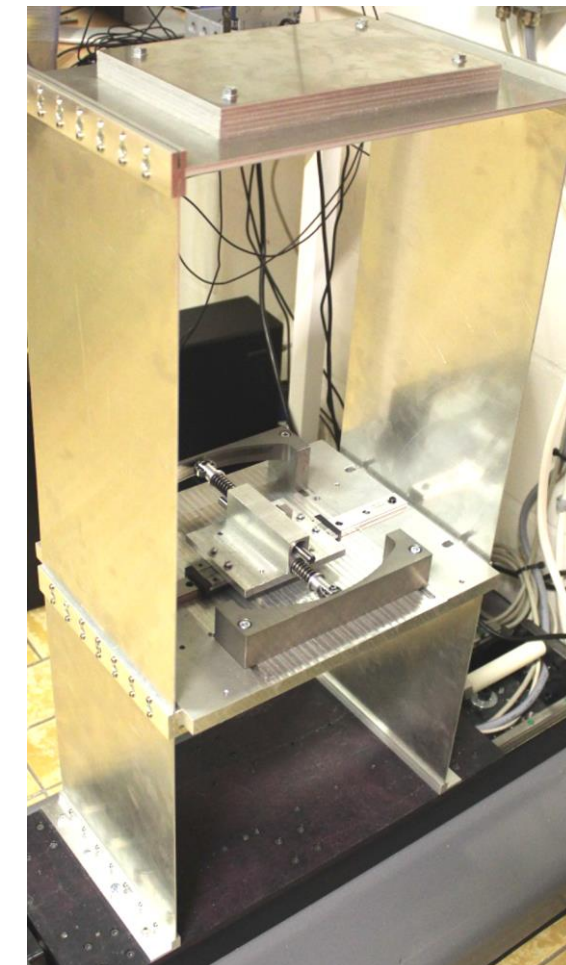
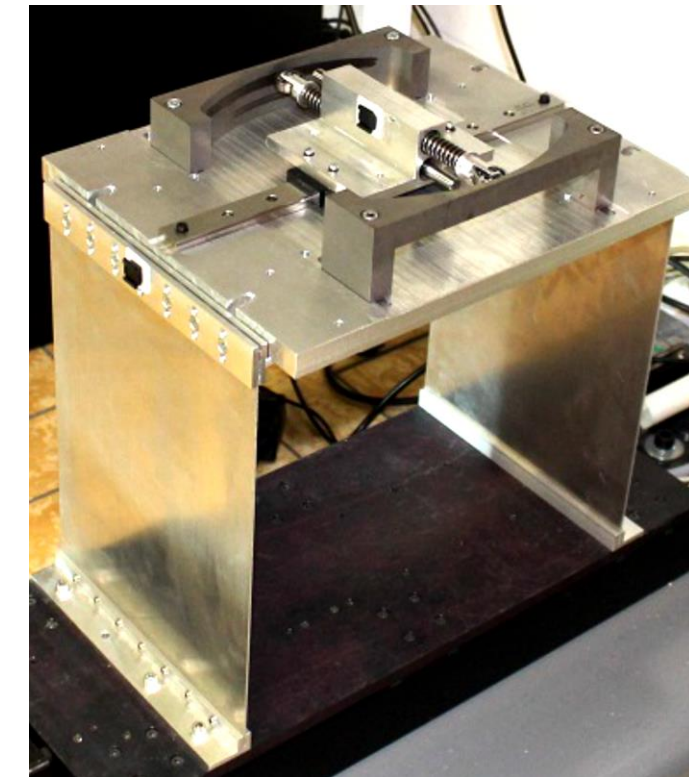
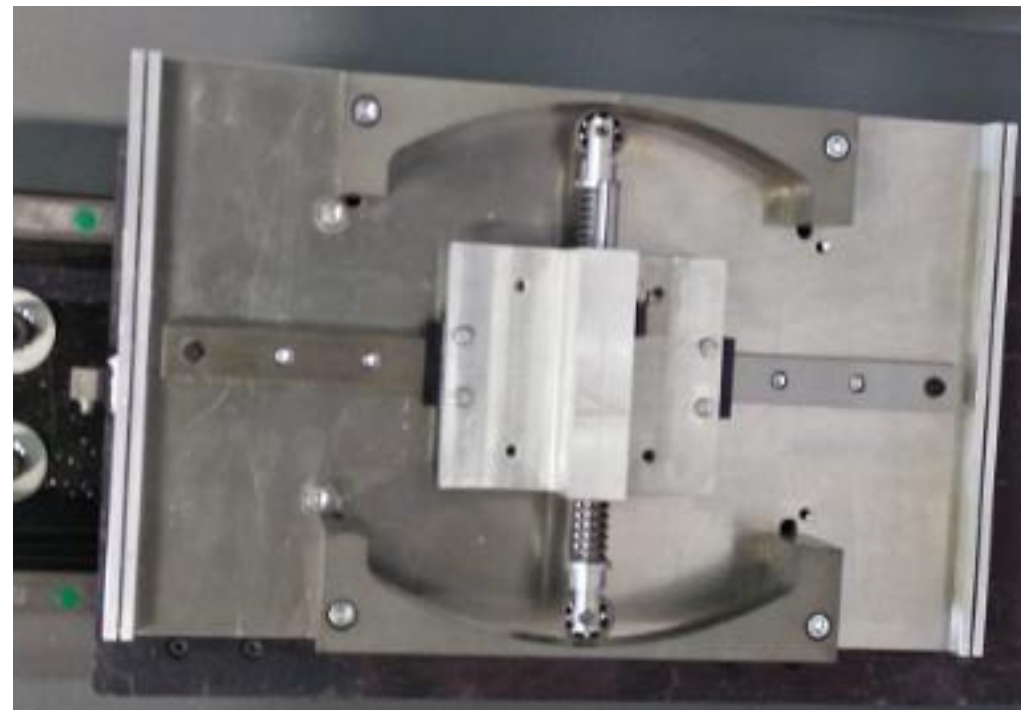
NES REALIZATION

Implementation

Mechanism



Realization

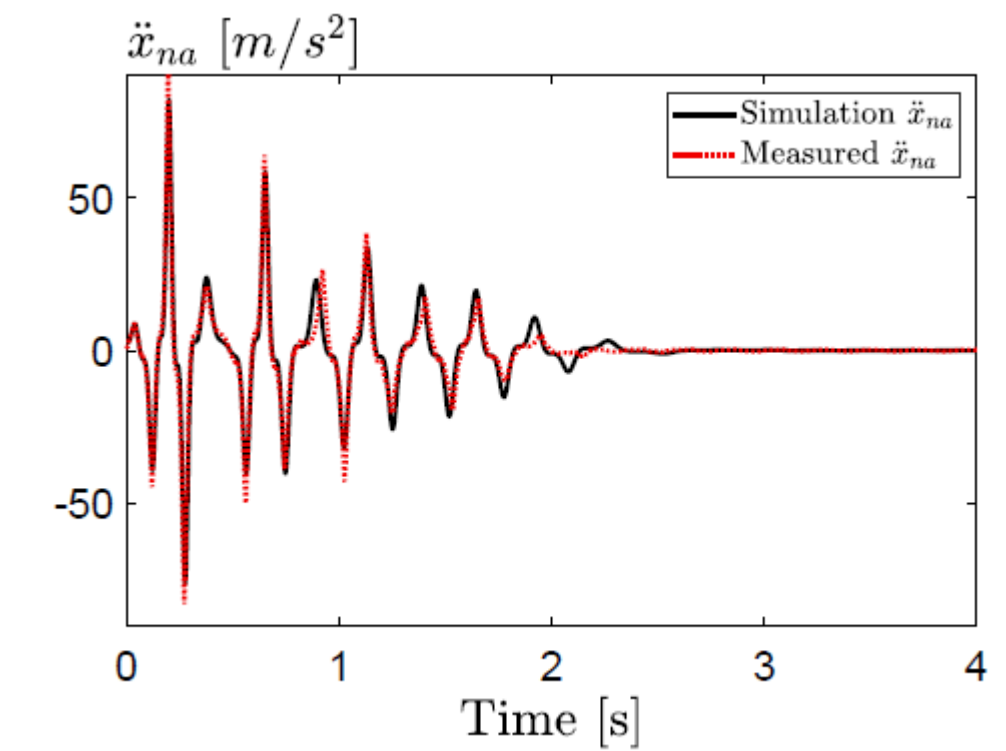
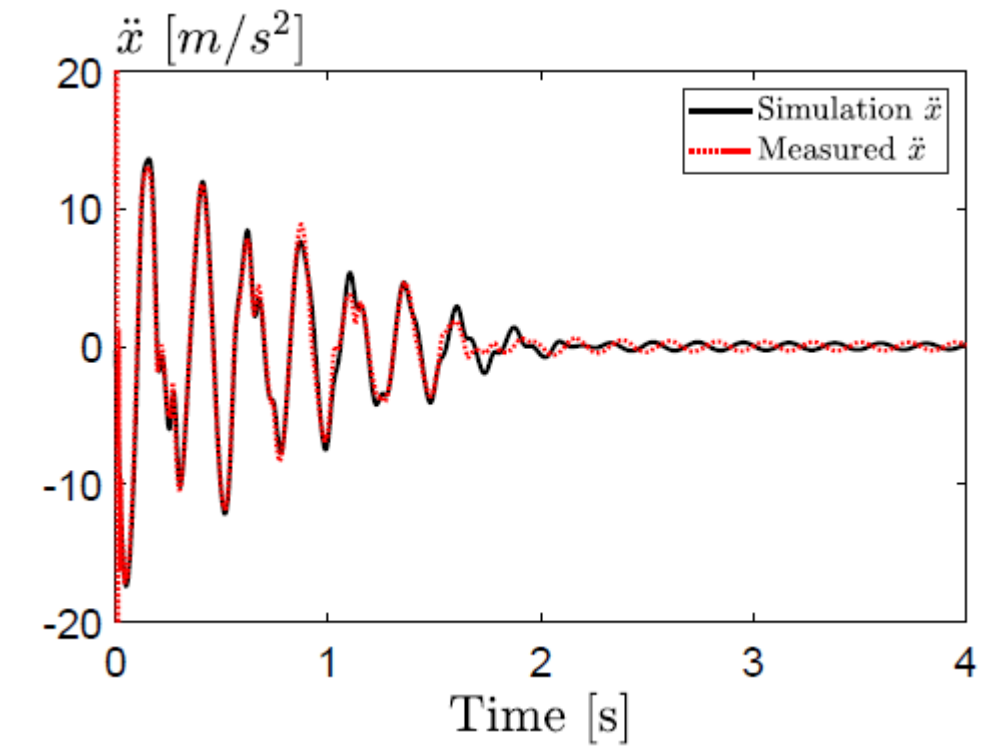


NES REALIZATION: EXPERIMENT

Without NES



With NES



NES REALIZATION: EXPERIMENT

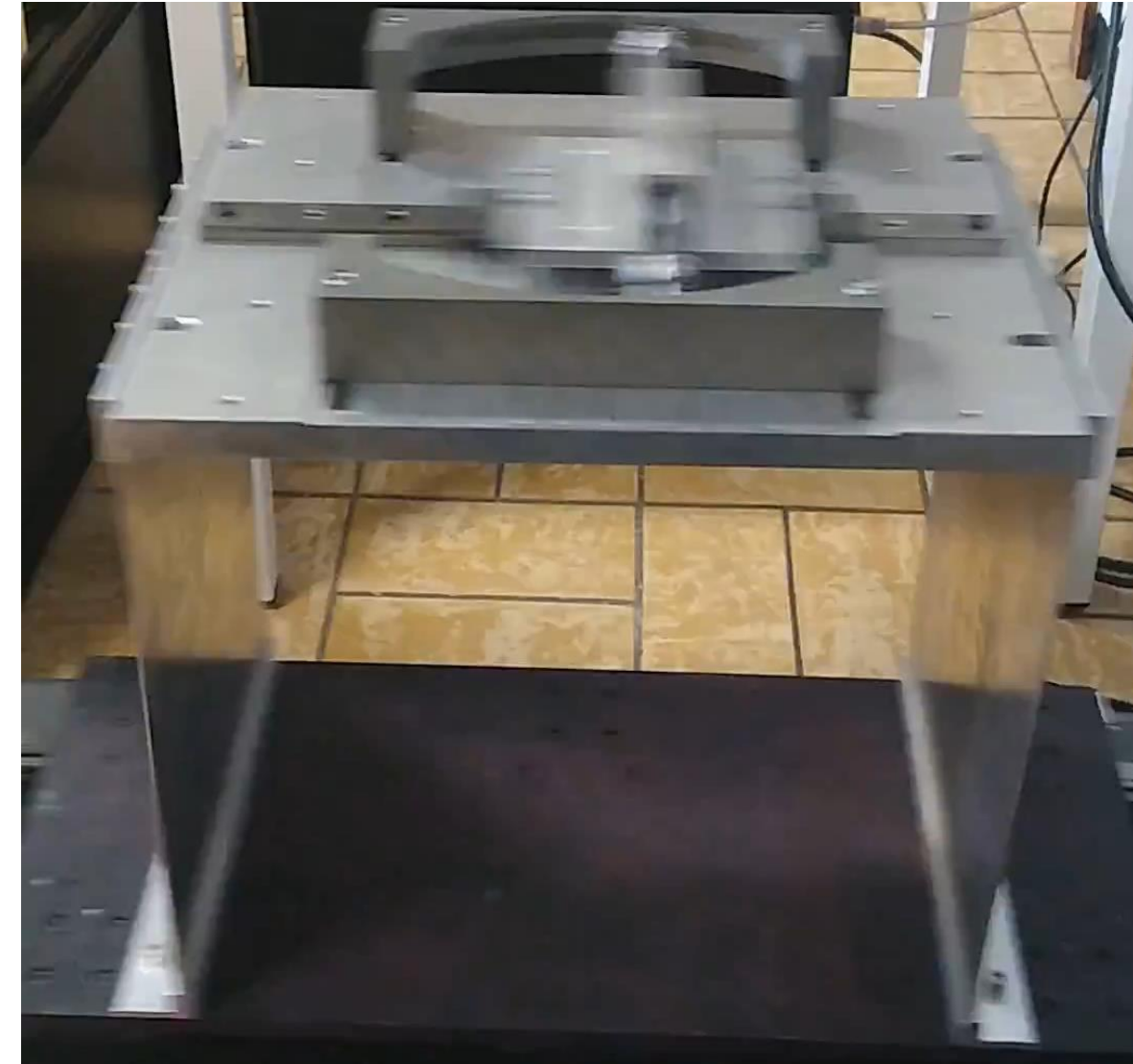
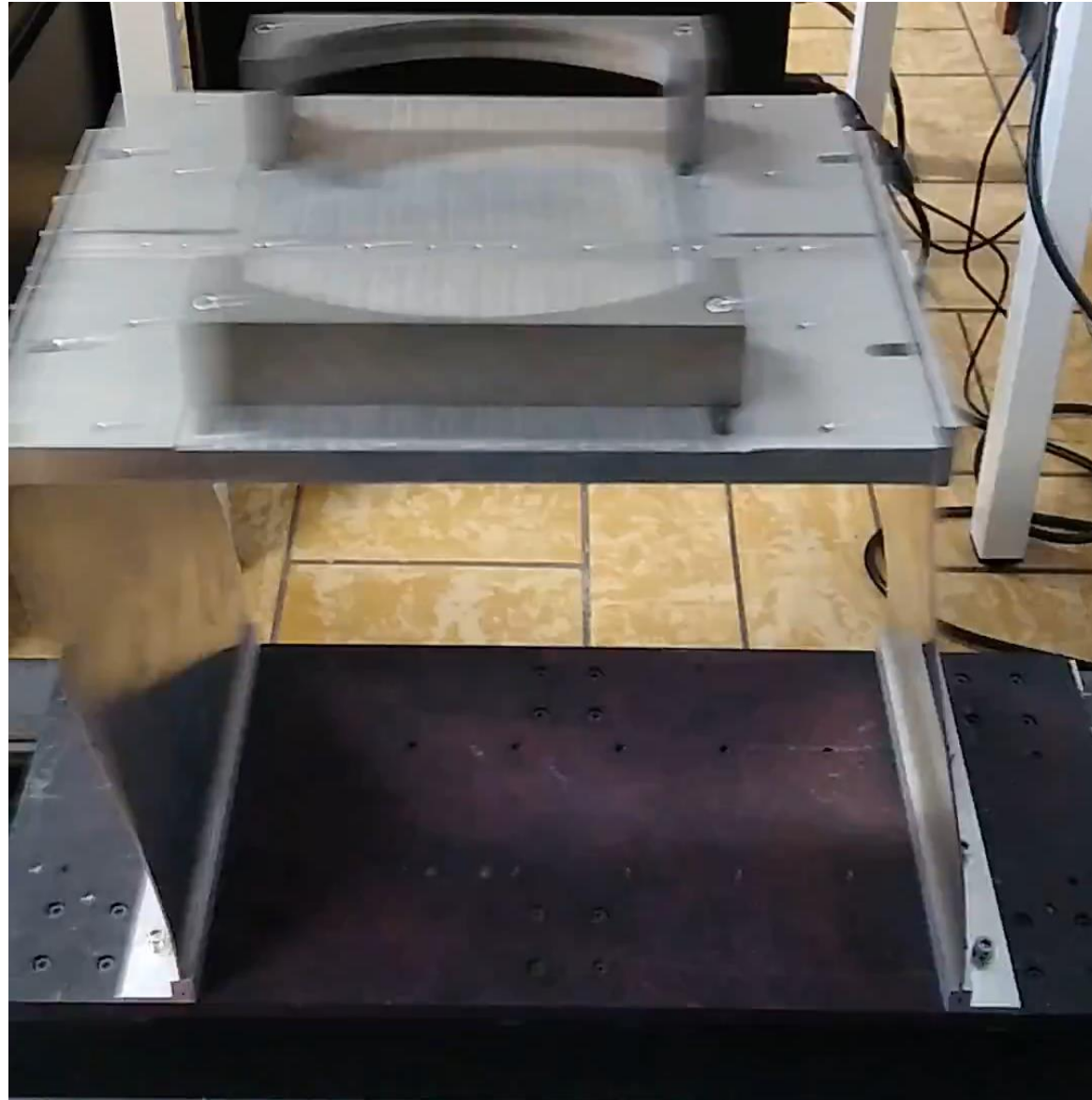
Without NES



With NES

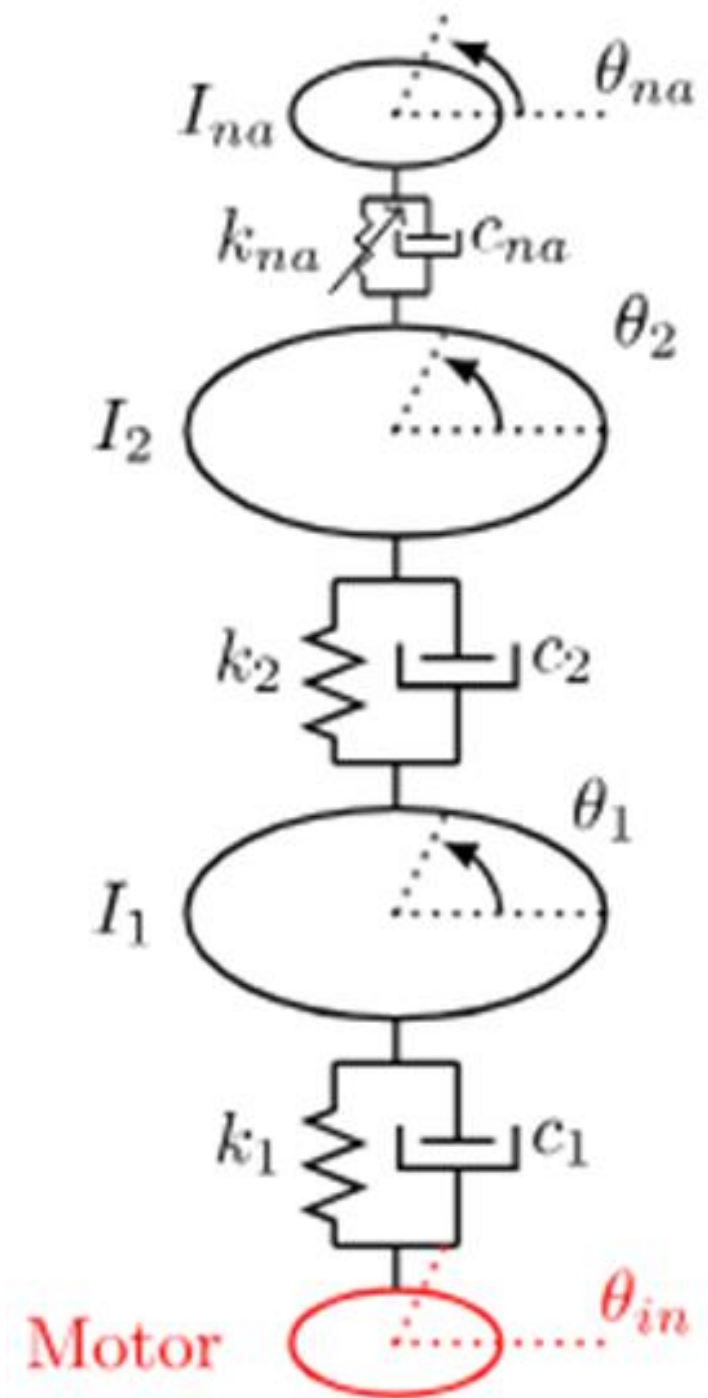
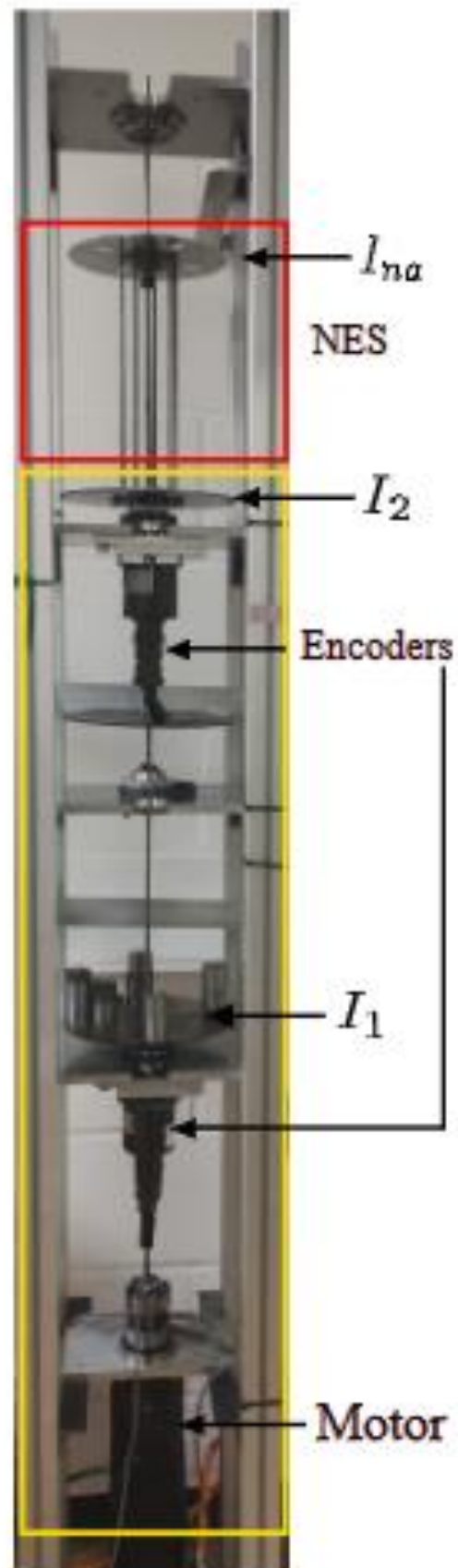


NES REALIZATION: EXPERIMENT HARMONIC

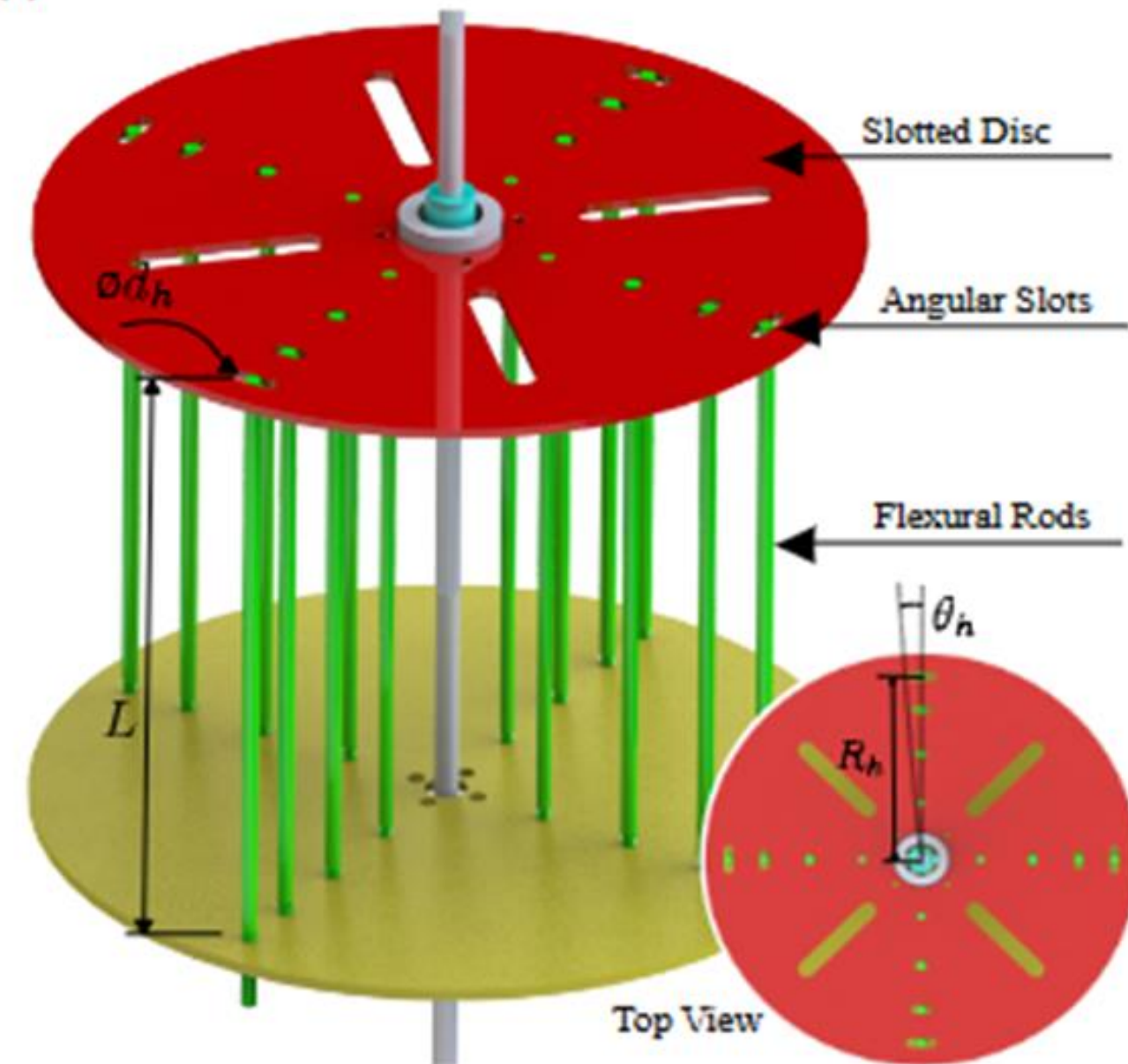


NES REALIZATION: TORSIONAL PLANT

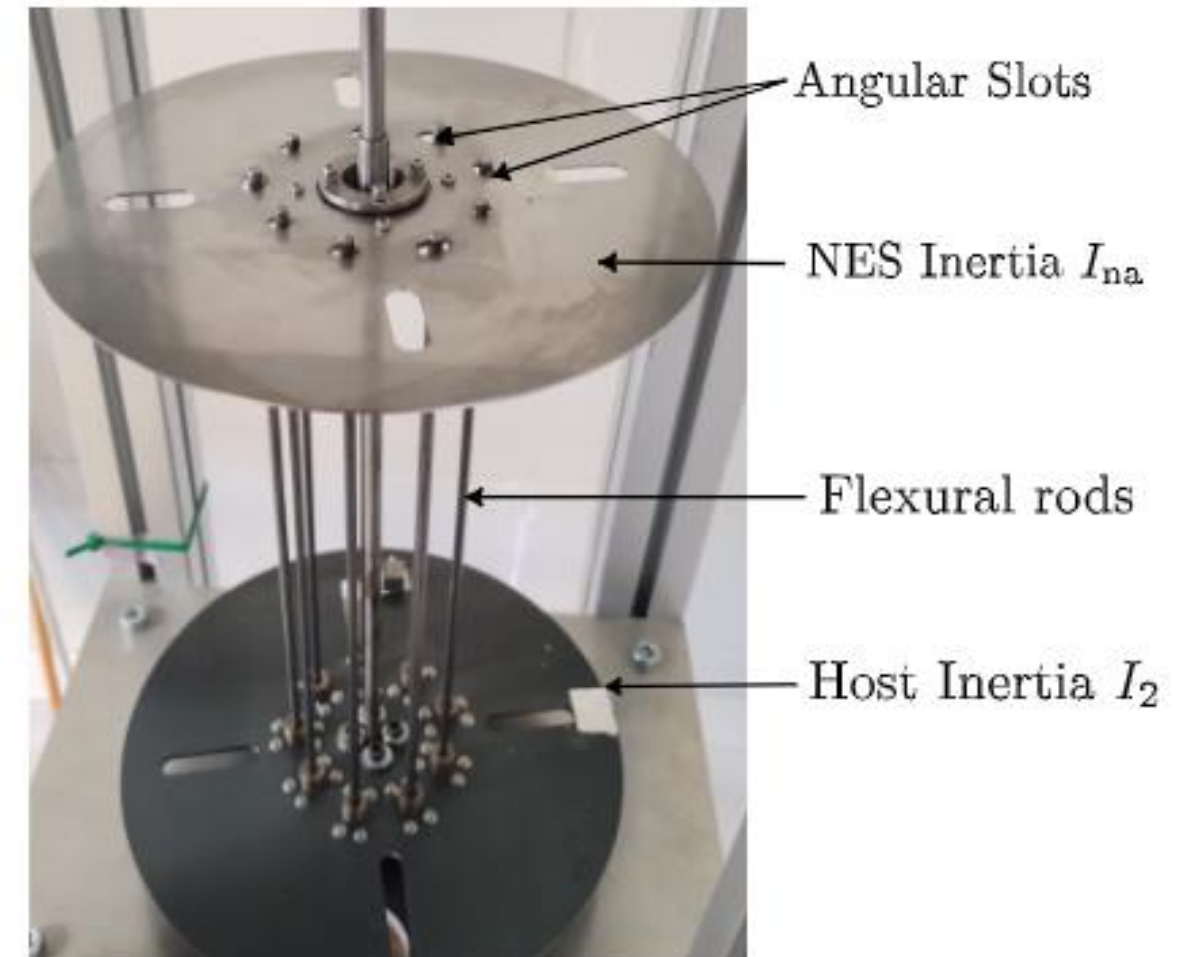
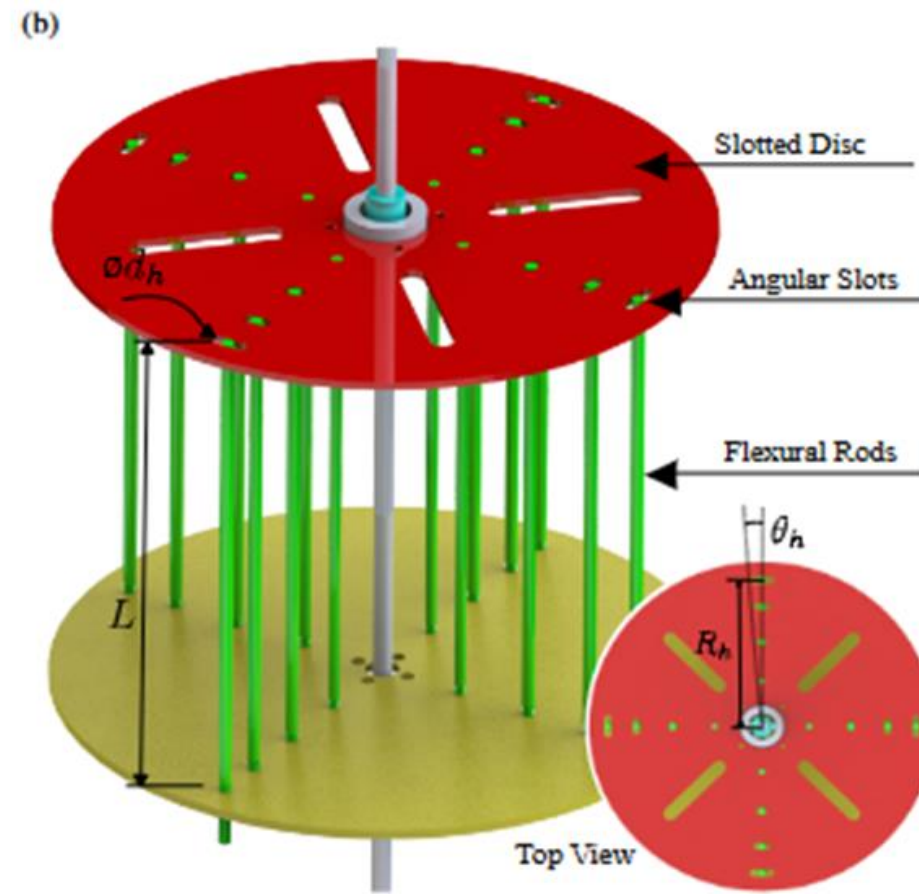
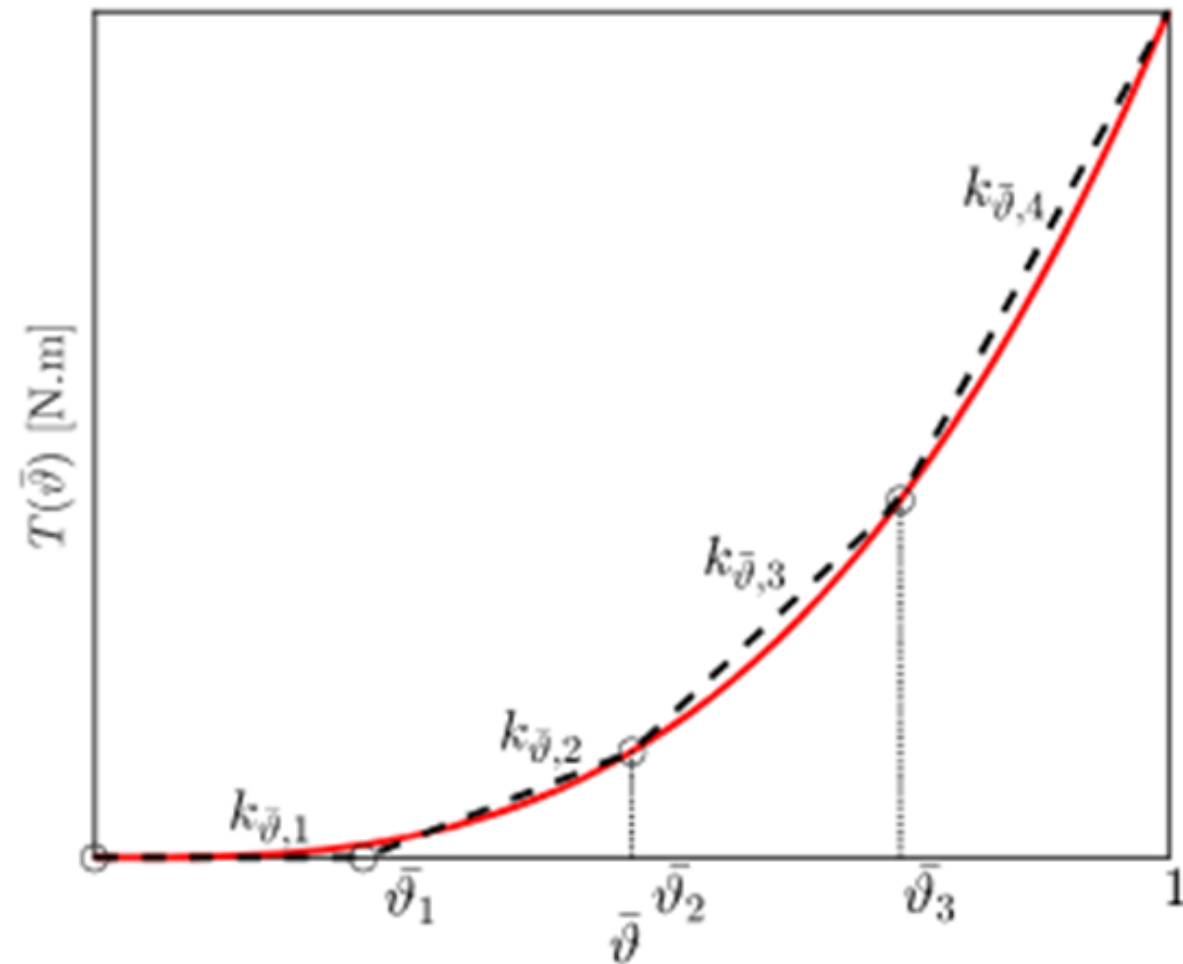
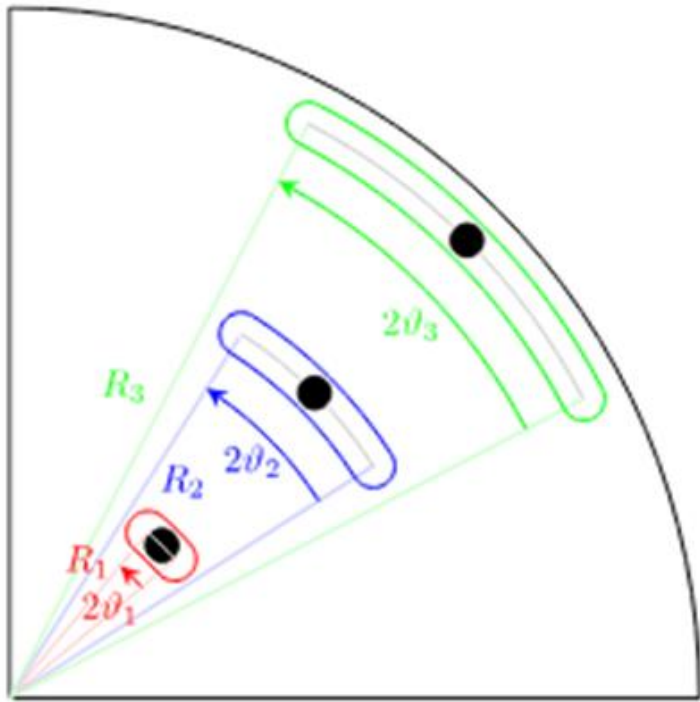
(a)



(b)



NES REALIZATION: TORSIONAL PLANT

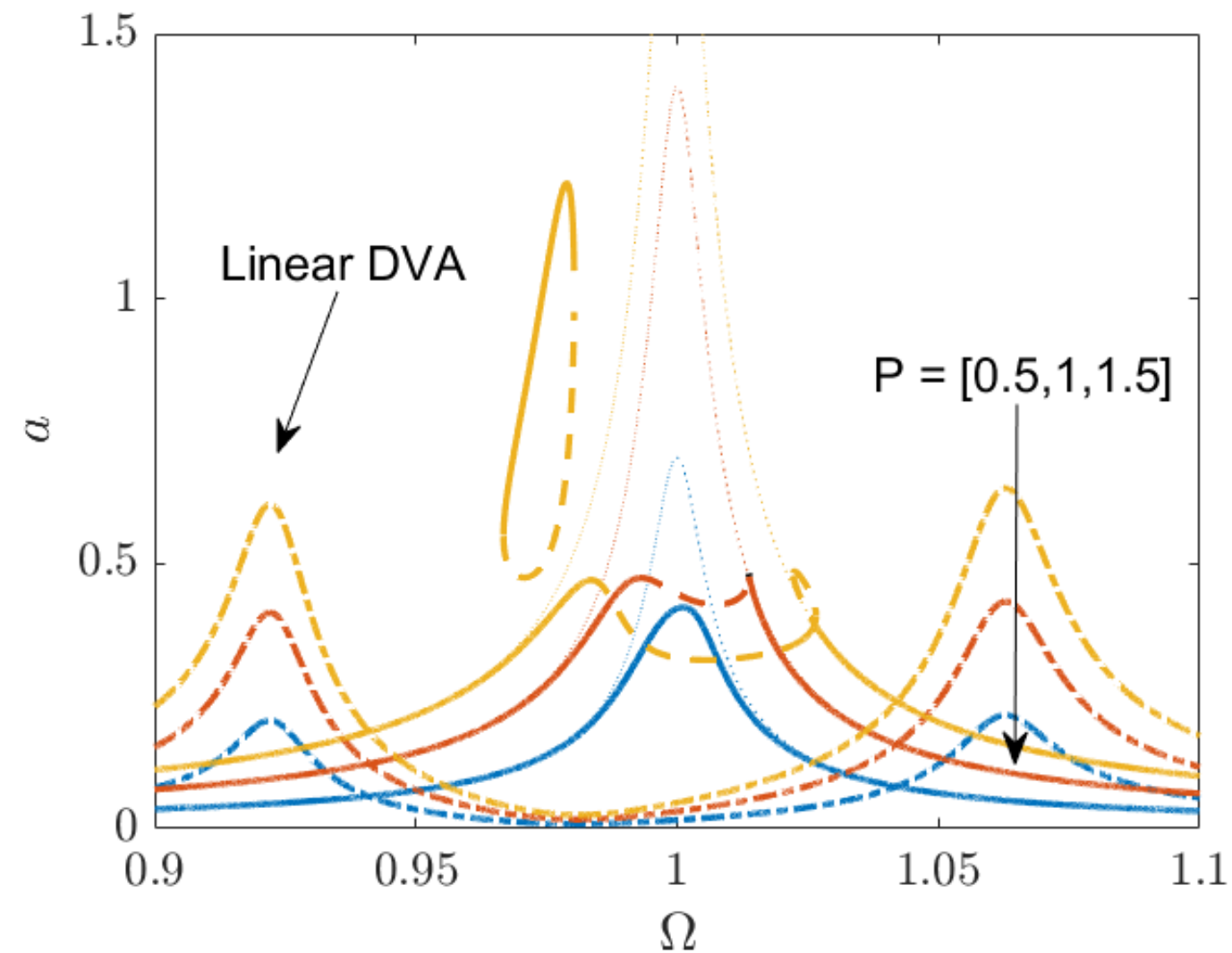
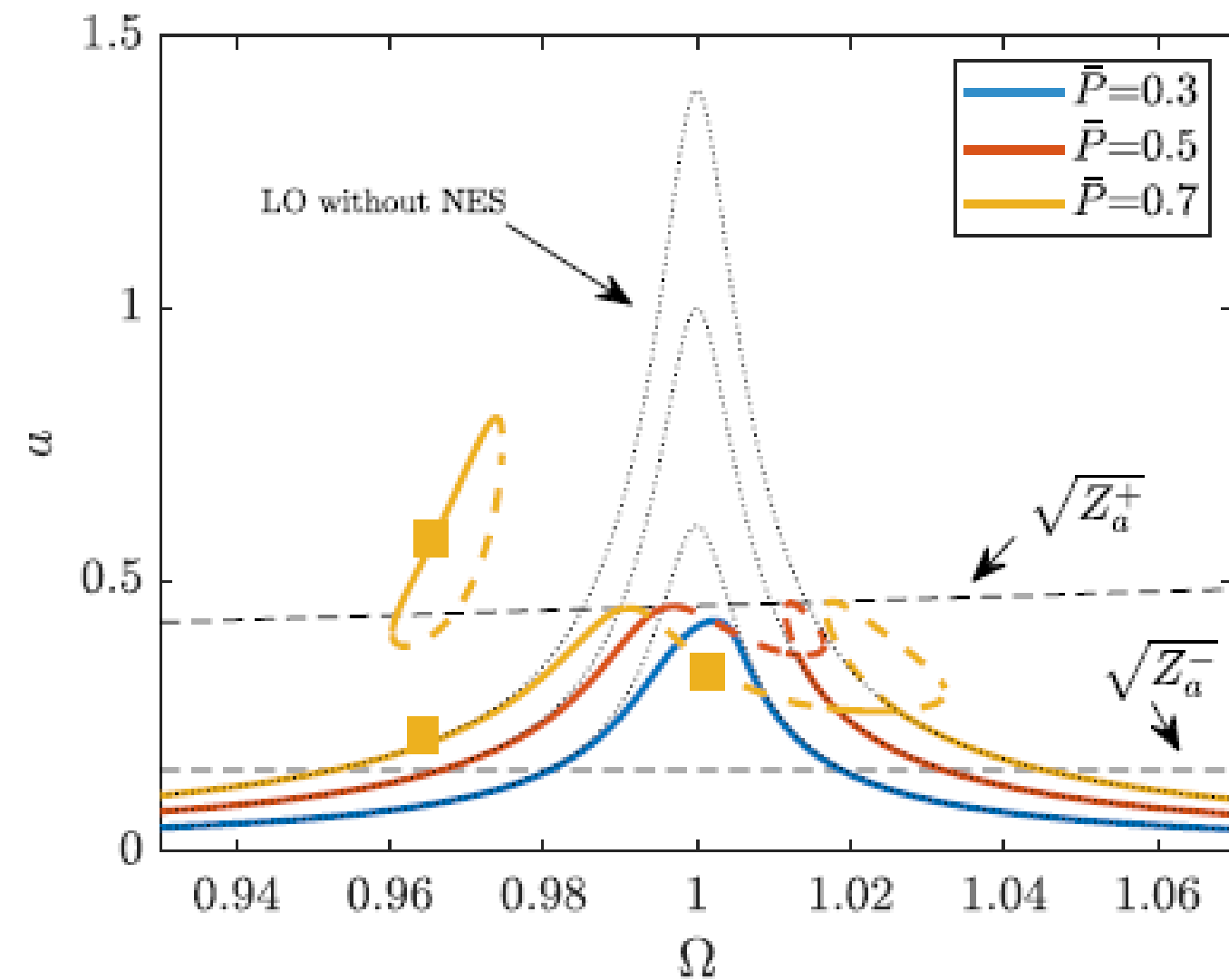


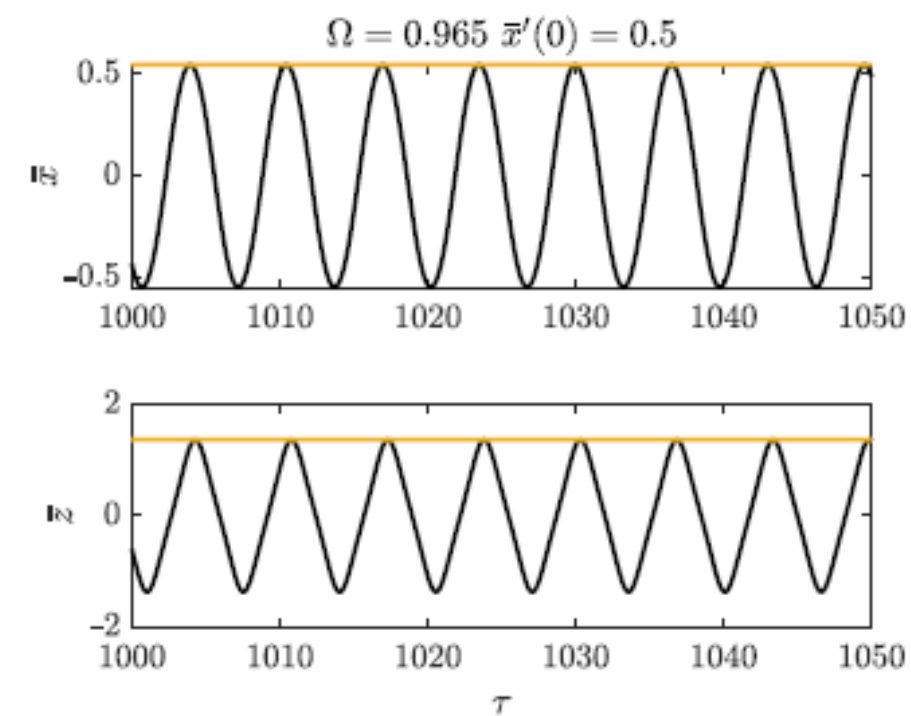
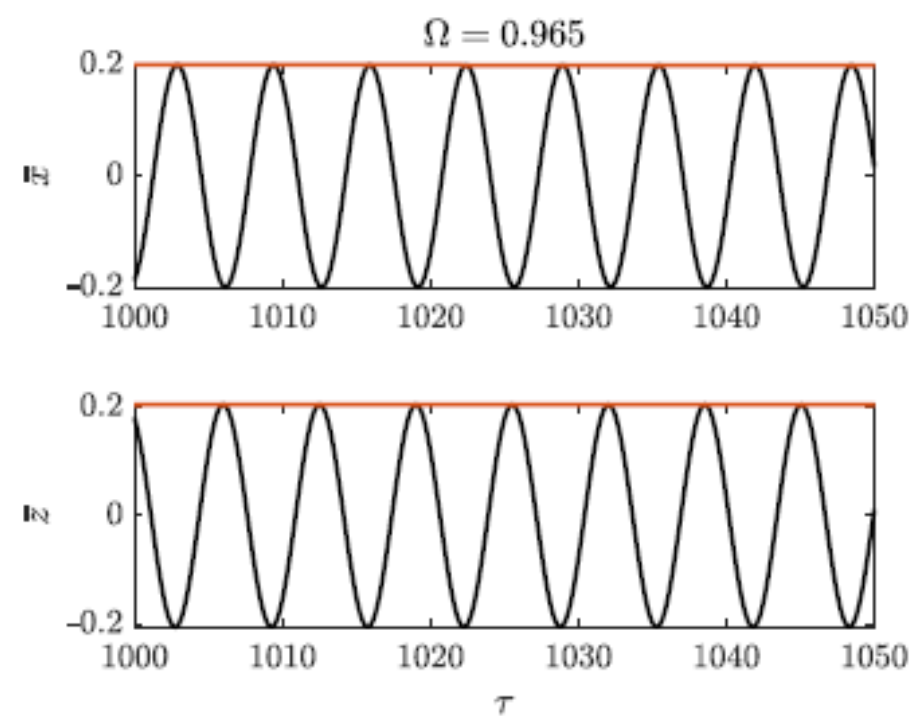
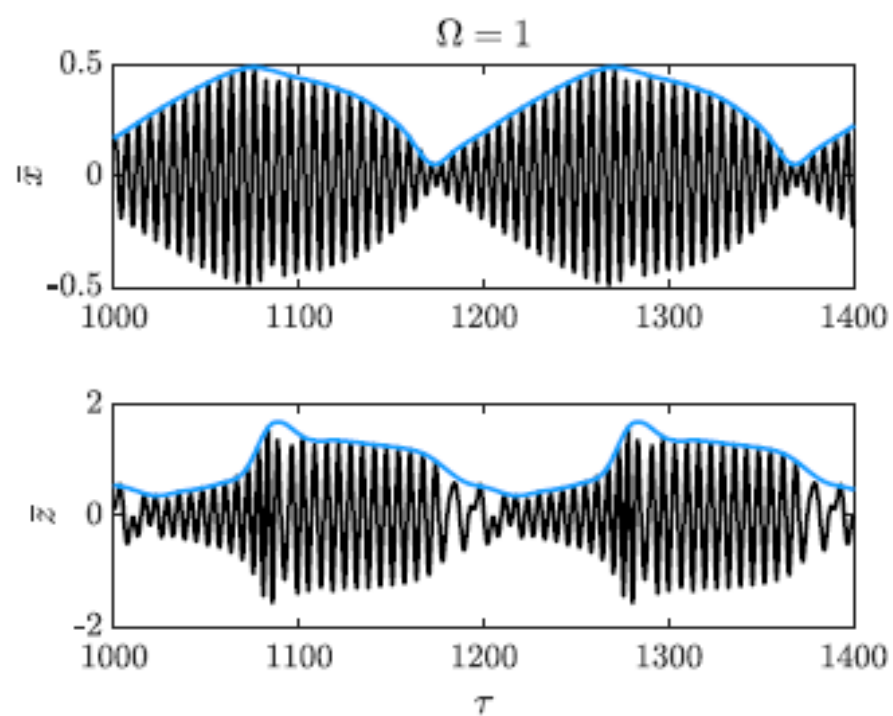
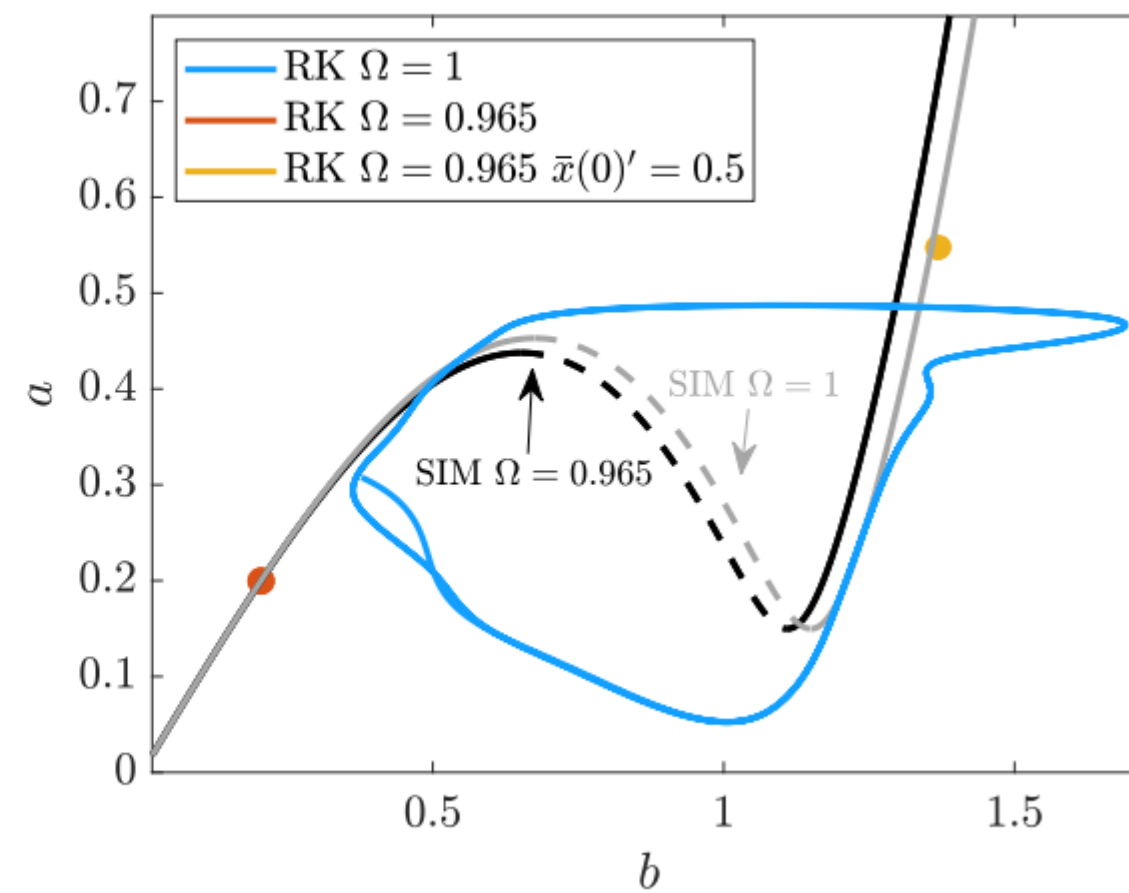
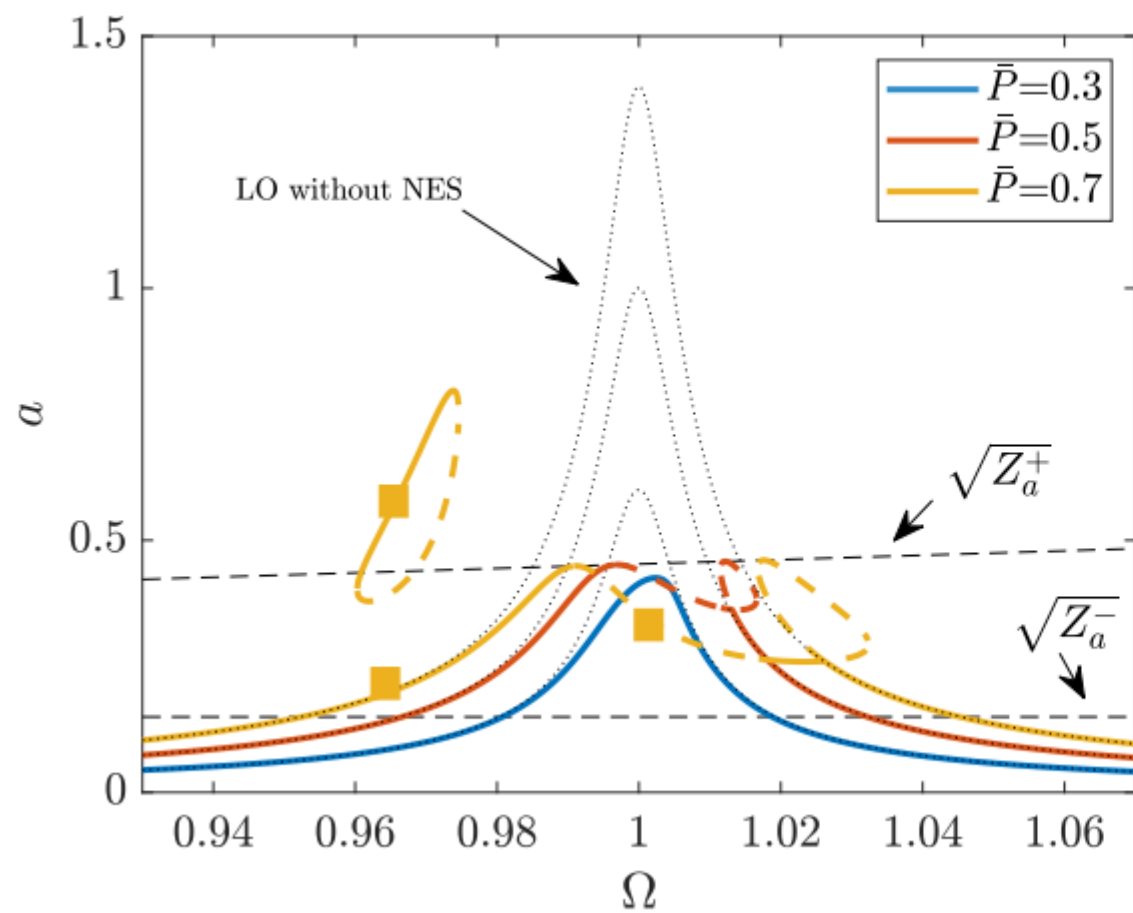
CONTENT

- Resonance Capture Cascade (Transient Load)
- Practical realization
- **Harmonic load: Hardening**
- Harmonic load: Softening
- Piezoelectrical NES

FORCED RESPONSE

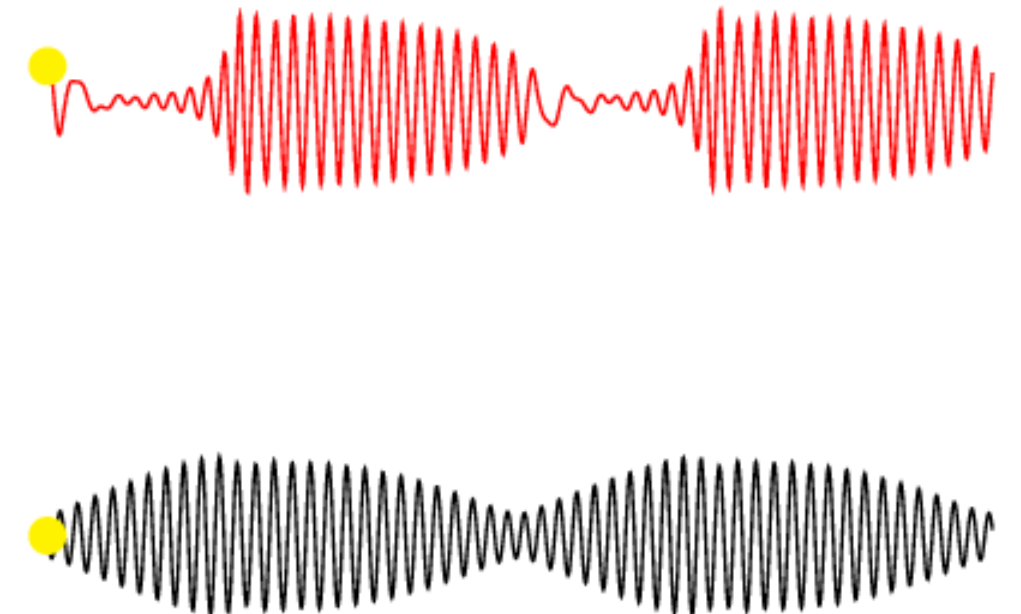
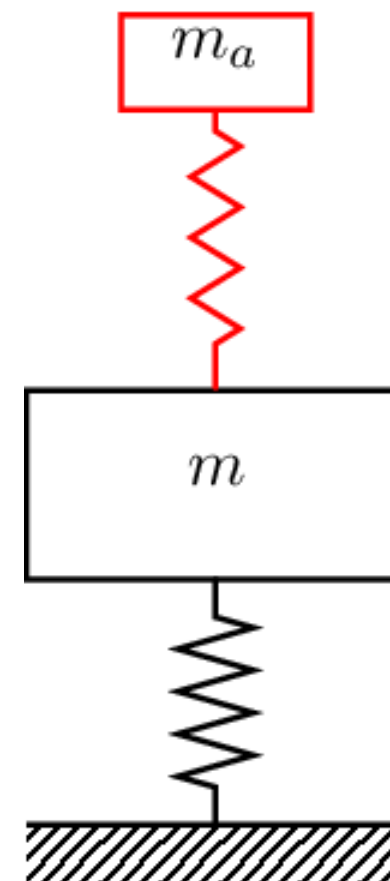
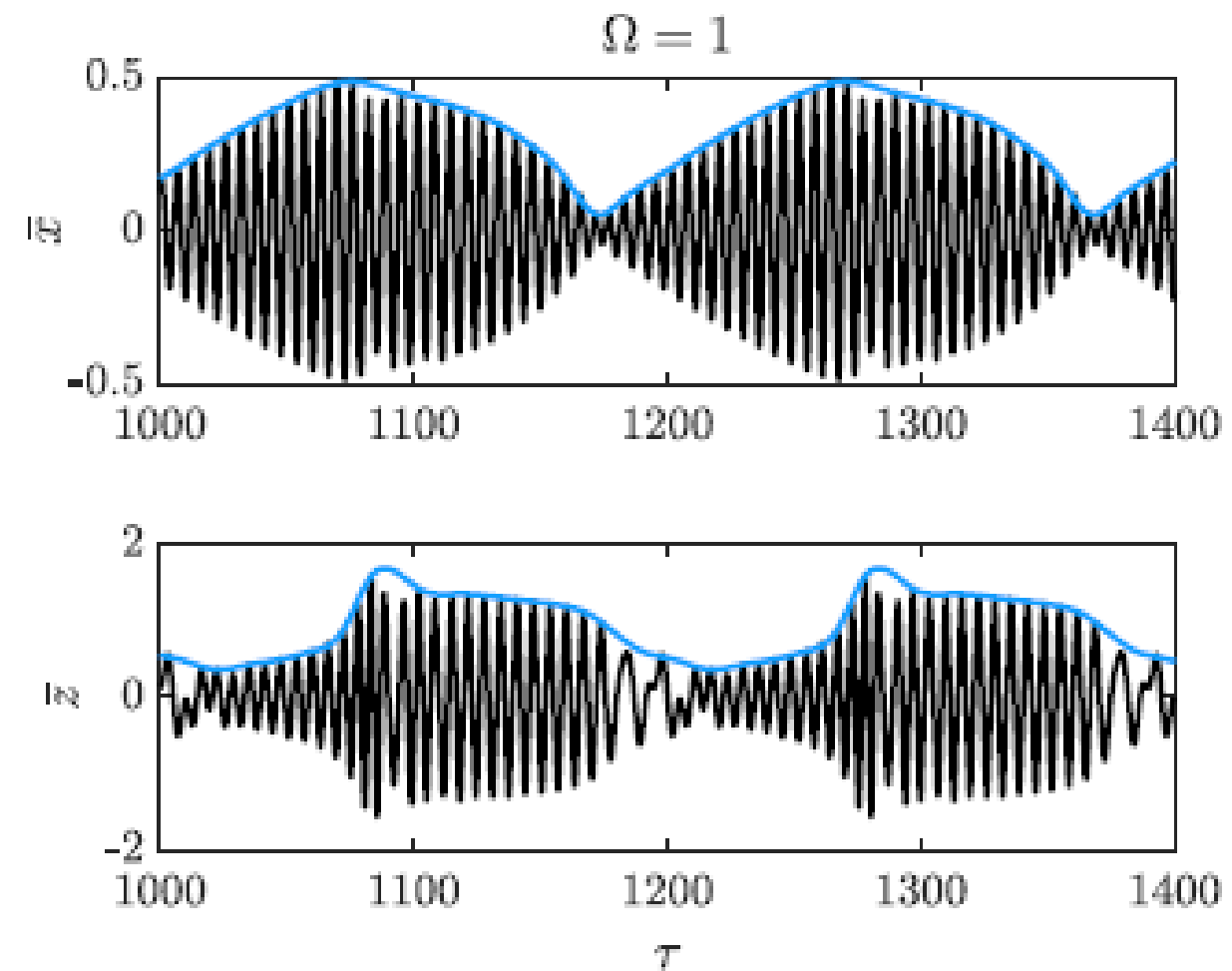
Kevin Dekemele, Tailored nonlinear stiffness and geometric damping: Applied to a bistable vibration absorber, *International Journal of Non-Linear Mechanics*, 2023, <https://doi.org/10.1016/j.ijnonlinmec.2023.104548>.





Time simulation

QUASI-PERIODIC VIBRATIONS



QUASI-PERIODIC VIBRATIONS

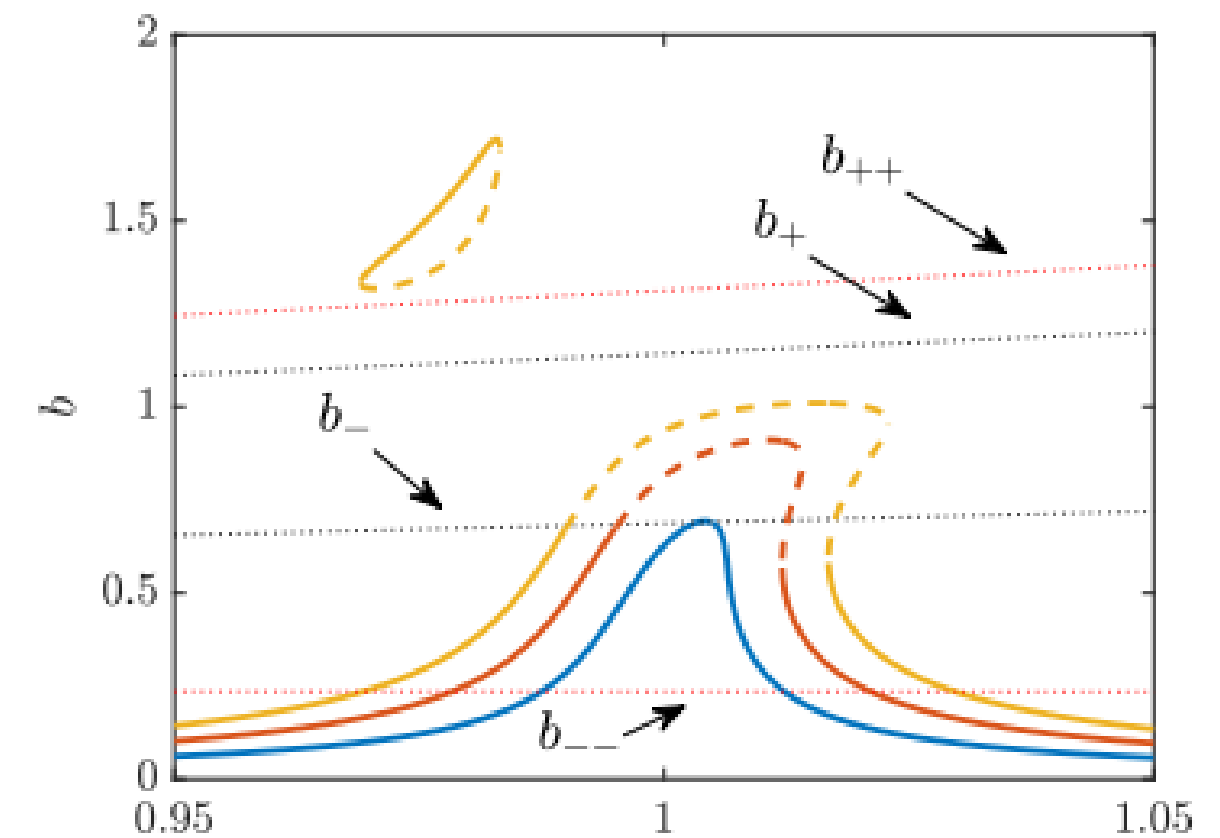
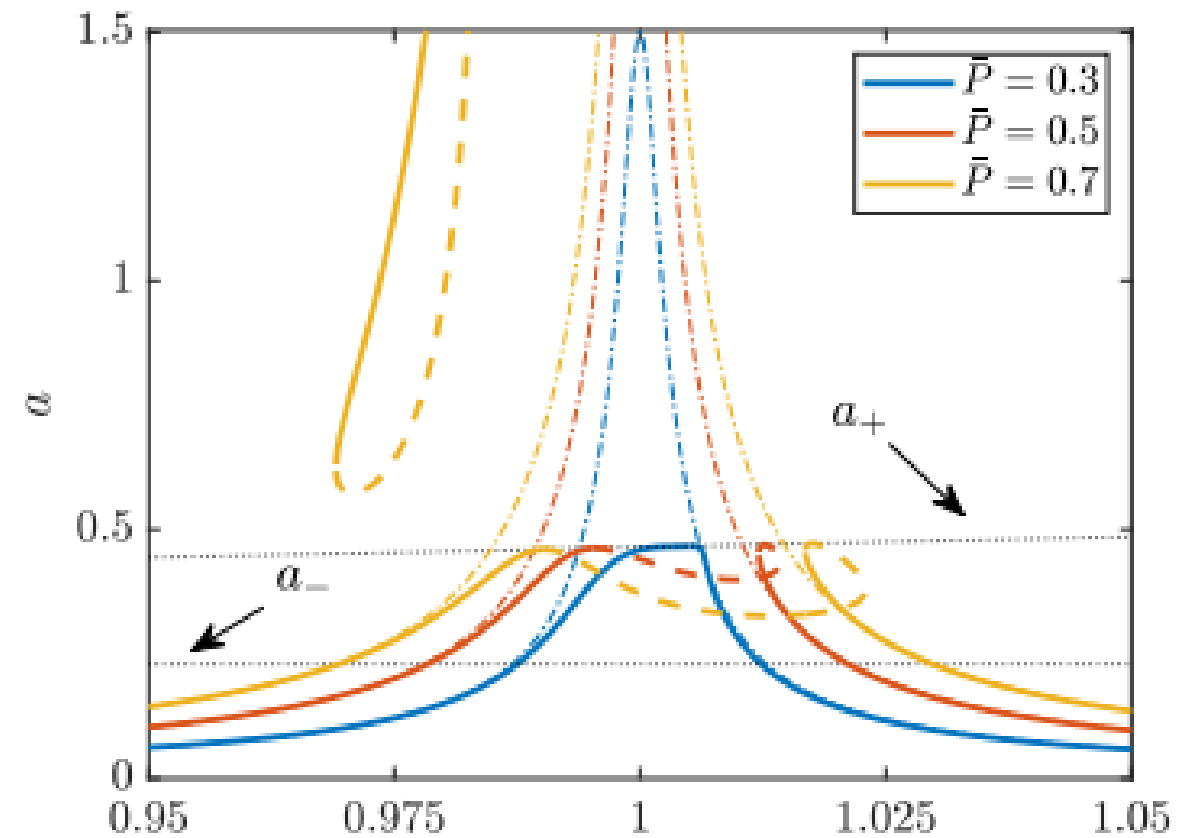


CONTENT

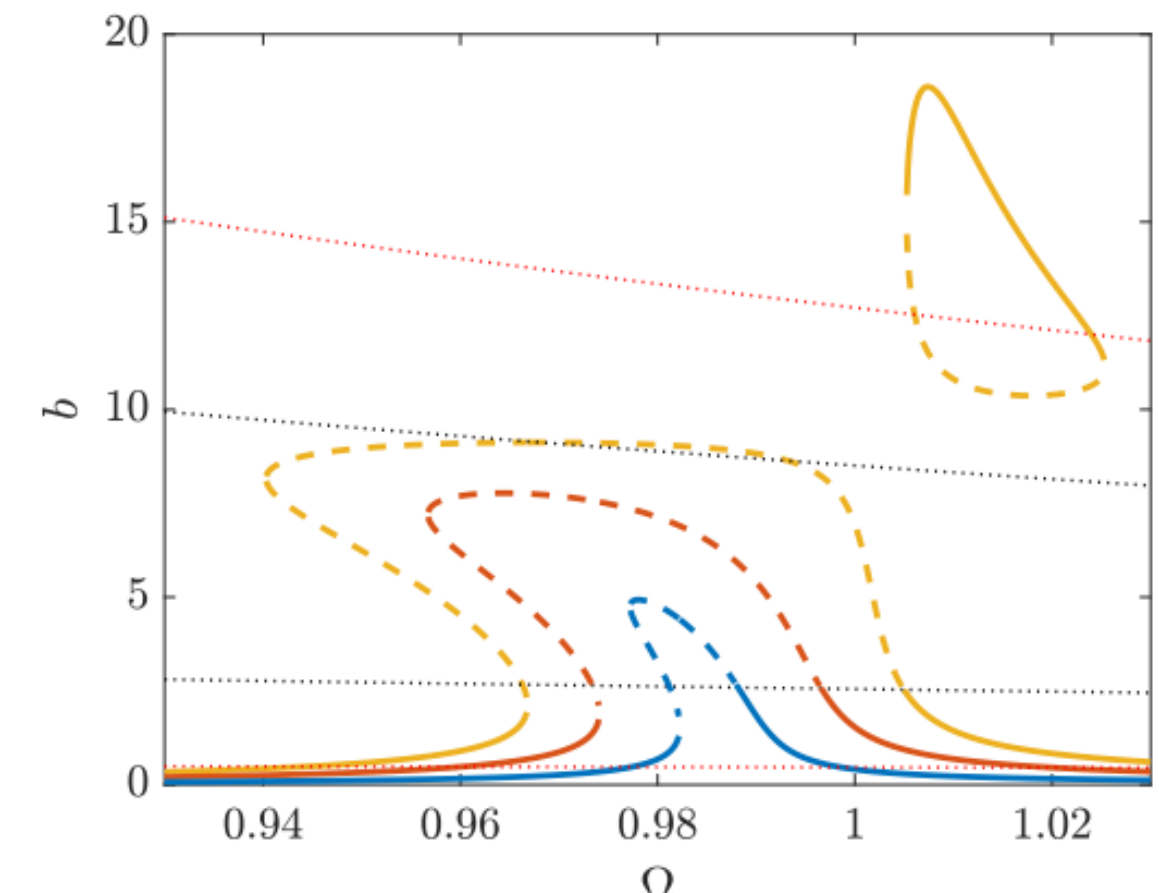
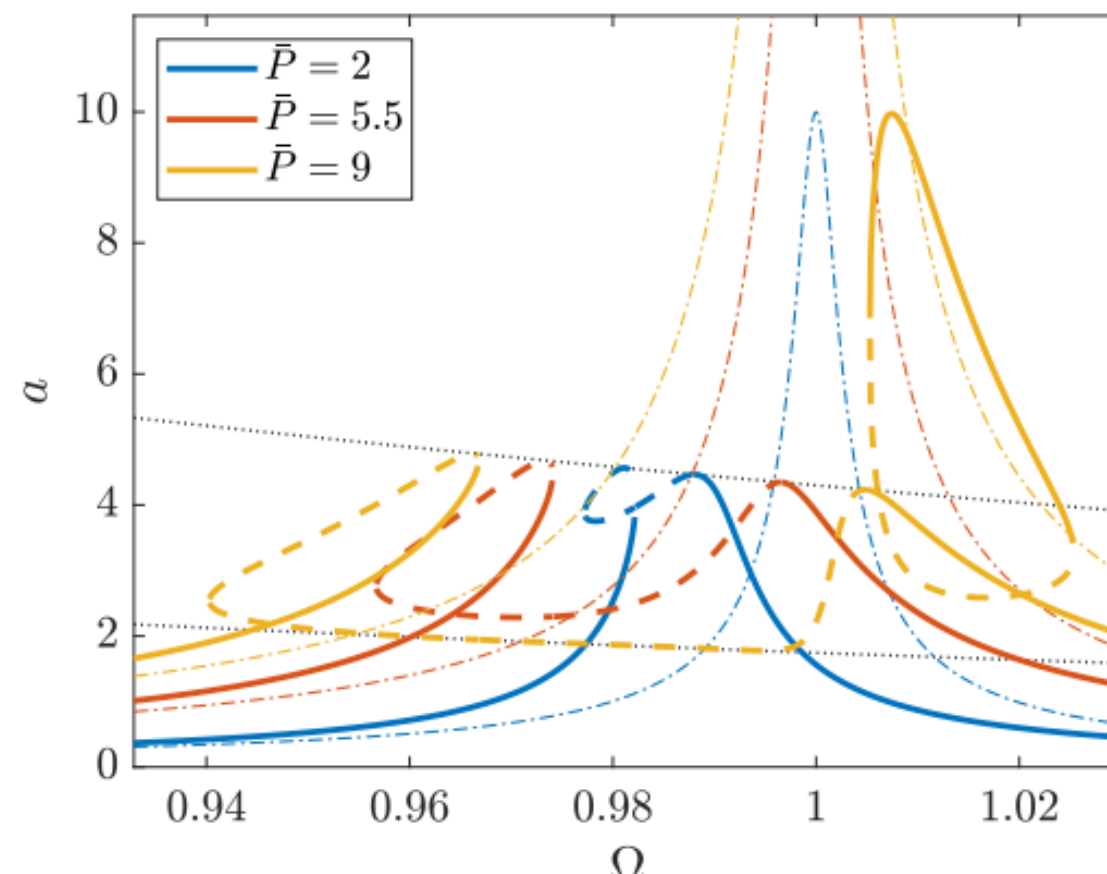
- Resonance Capture Cascade (Transient Load)
- Practical realization
- Harmonic load: Hardening
- **Harmonic load: Softening**
- Piezoelectrical NES

SOFTENING NONLINEAR ENERGY SINK

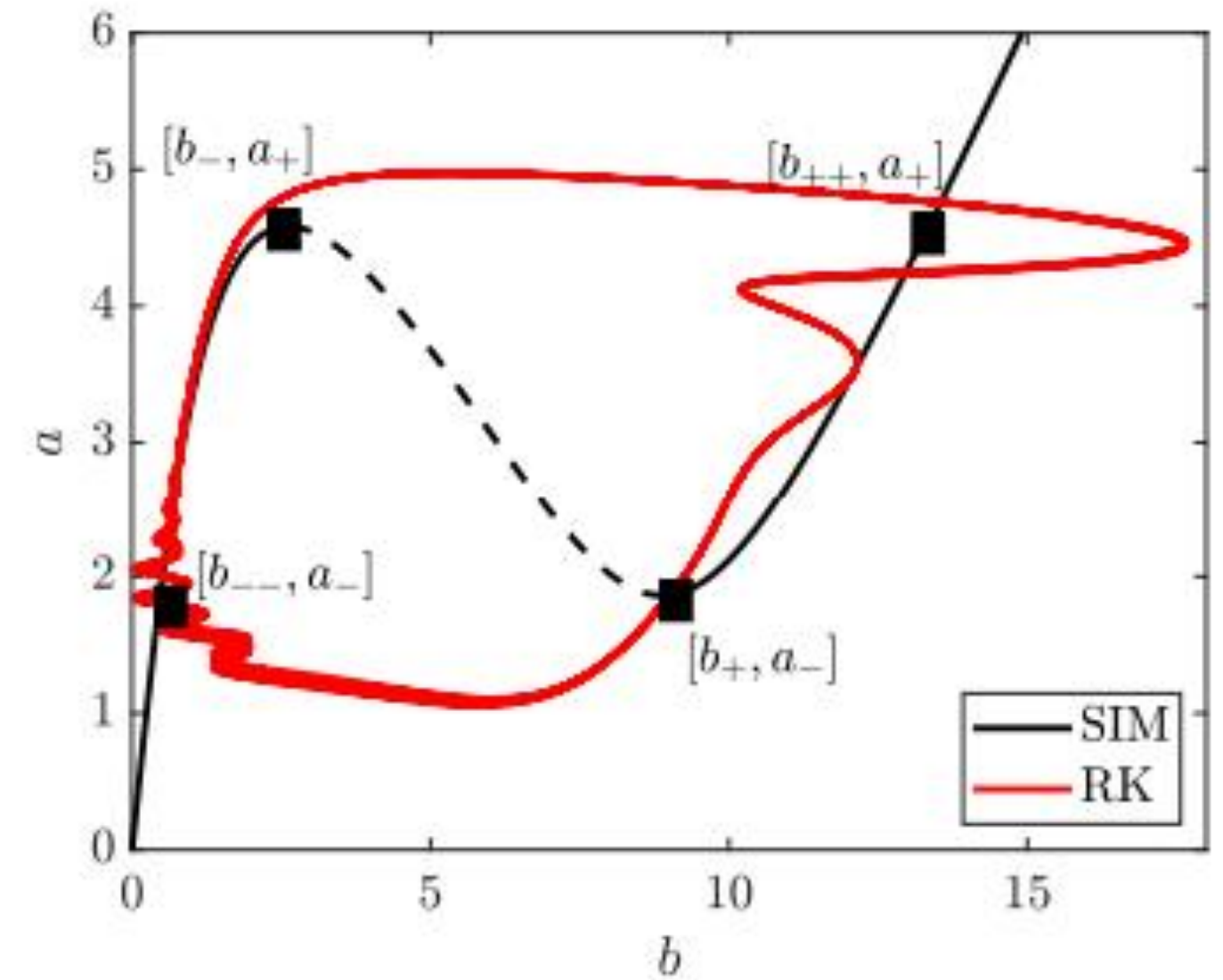
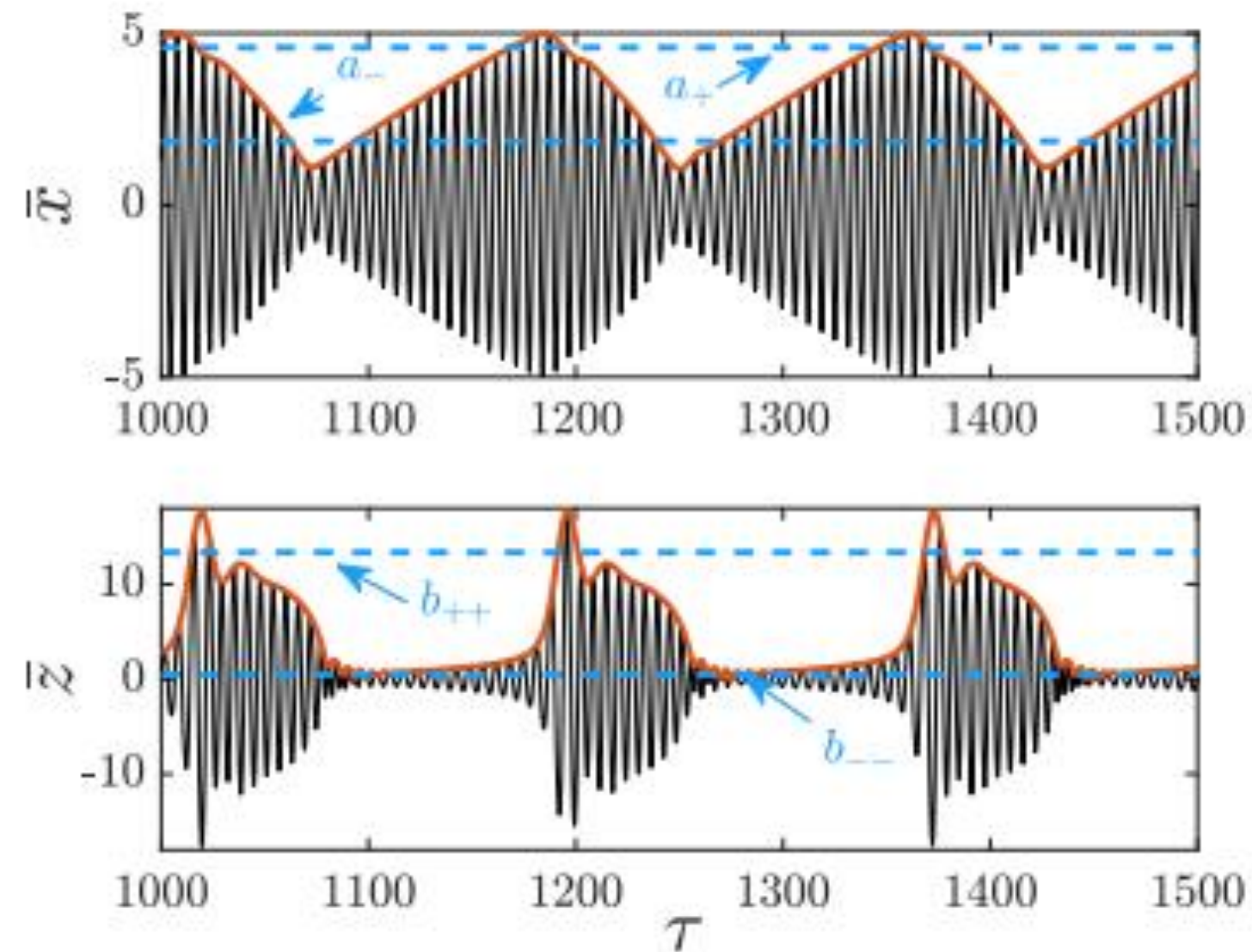
Hardening



Softening

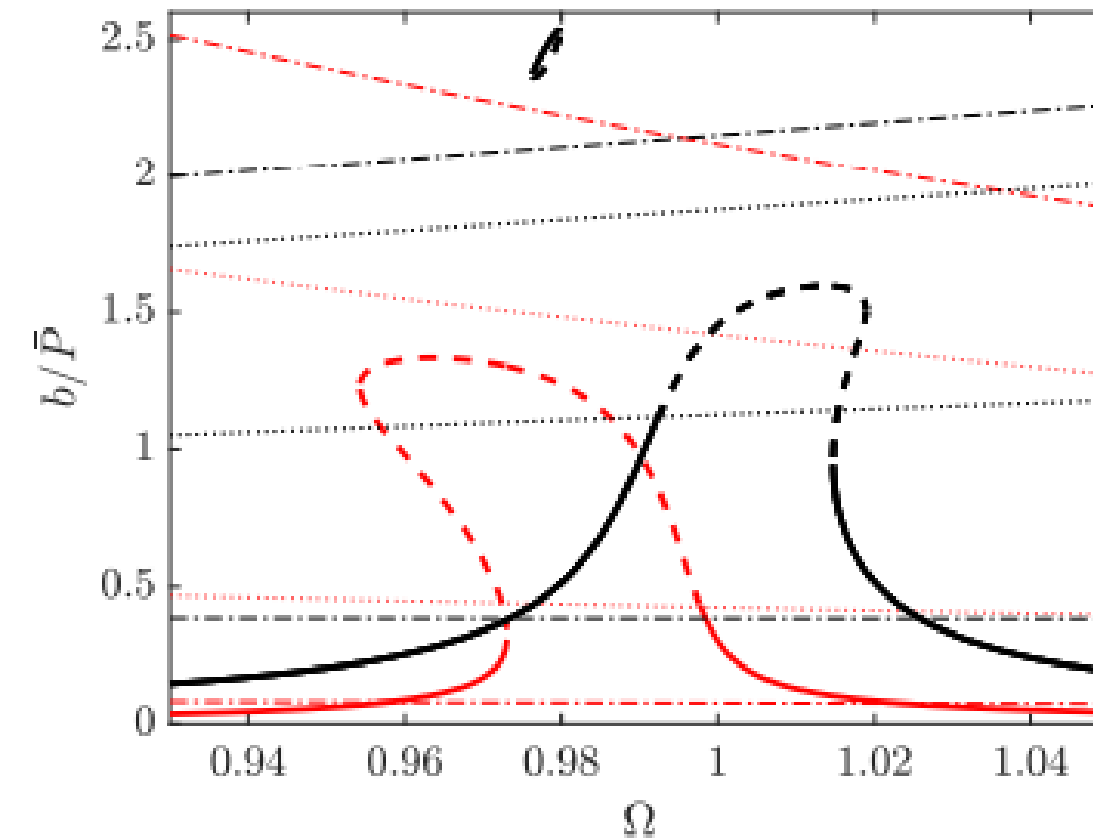
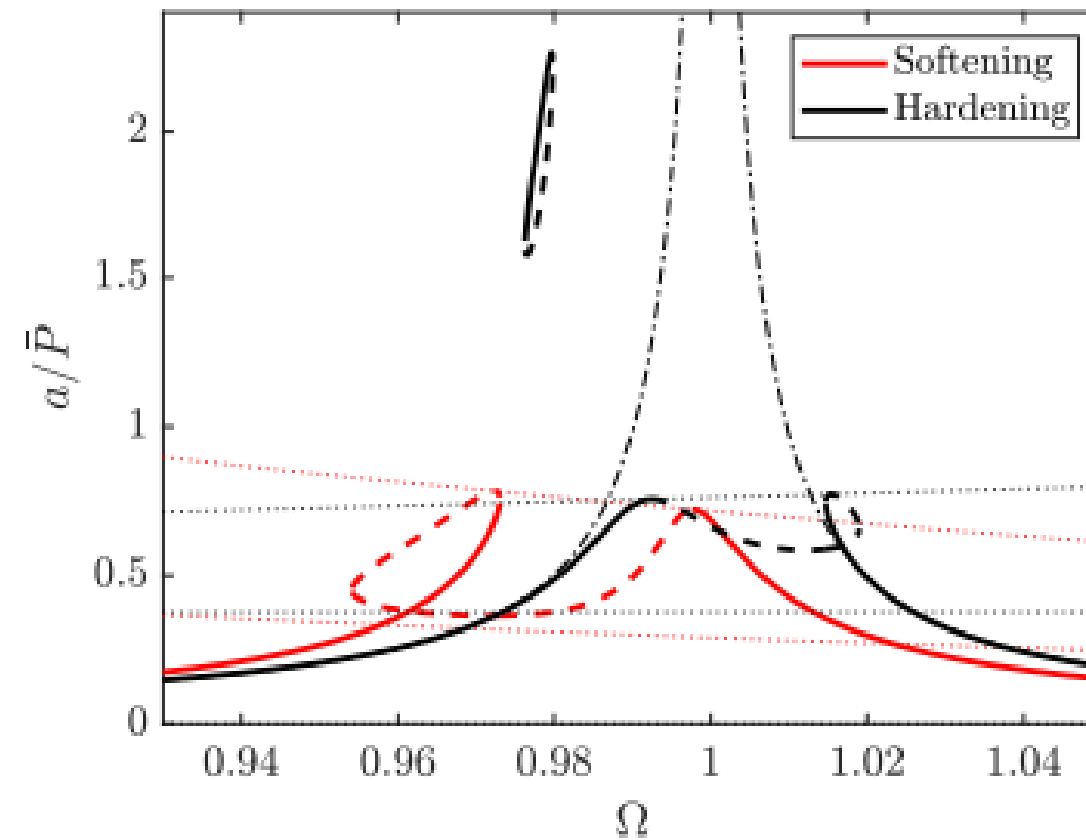


TIME SIGNALS: QUASI PERIODIC

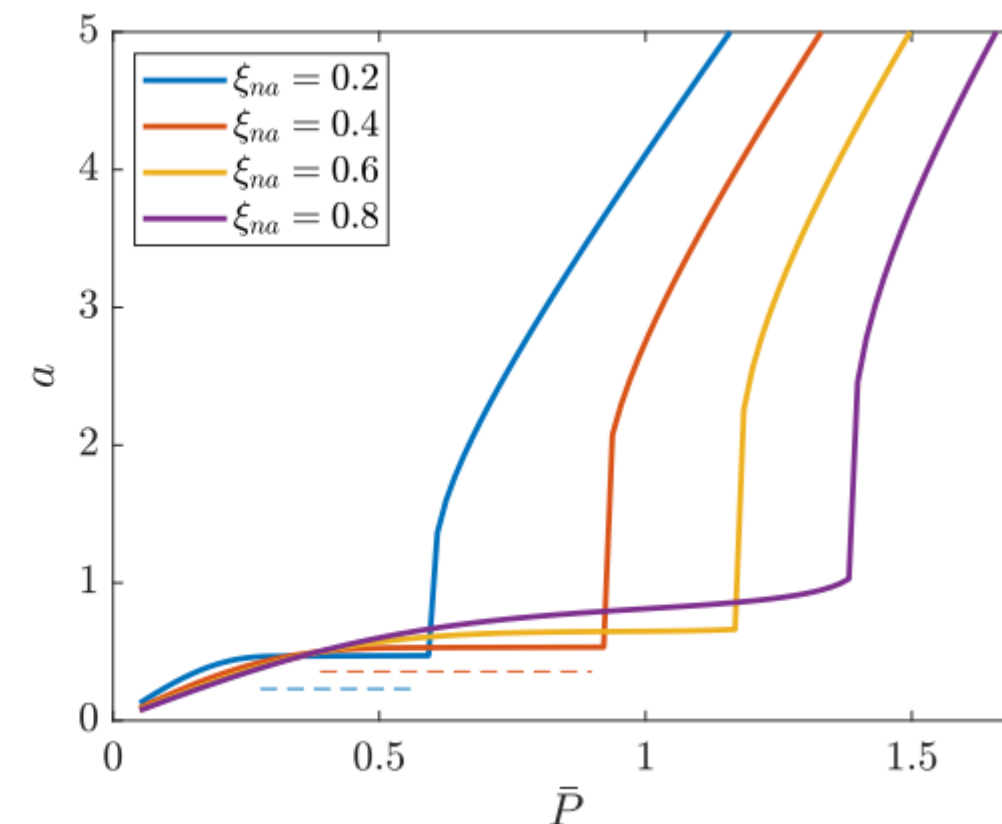
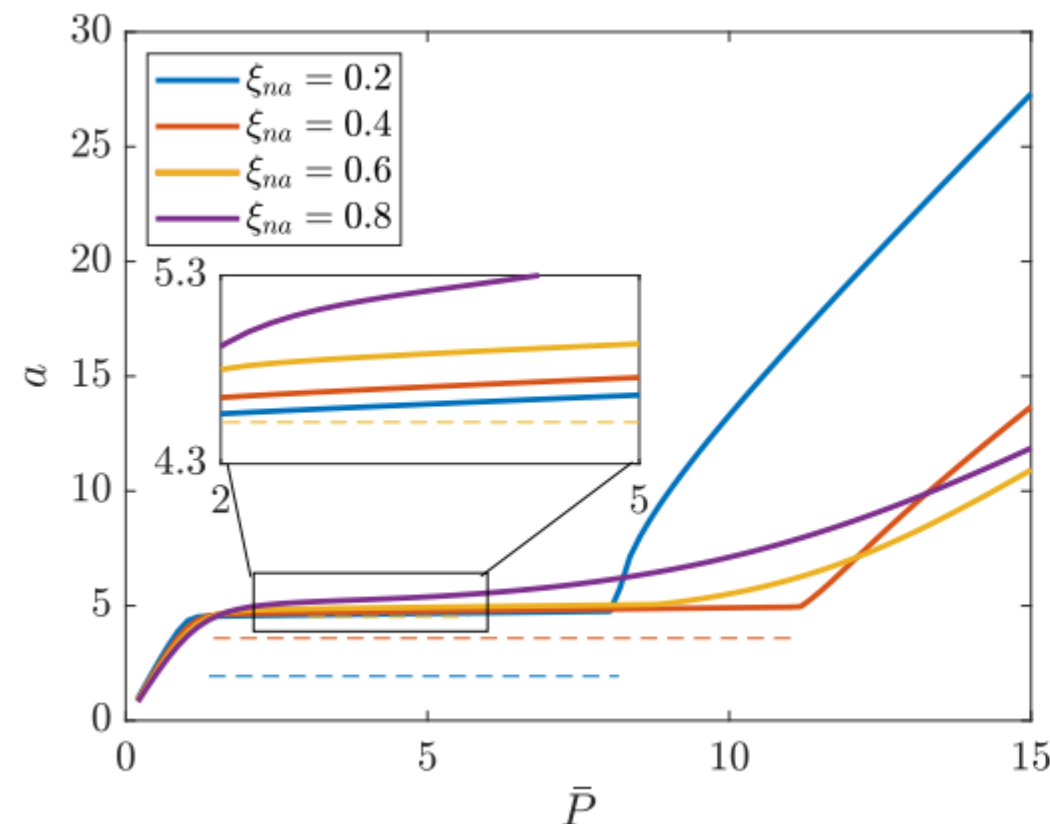


HARDENING VS SOFTENING: WHO'S BETTER?

Same saturation
No isola!



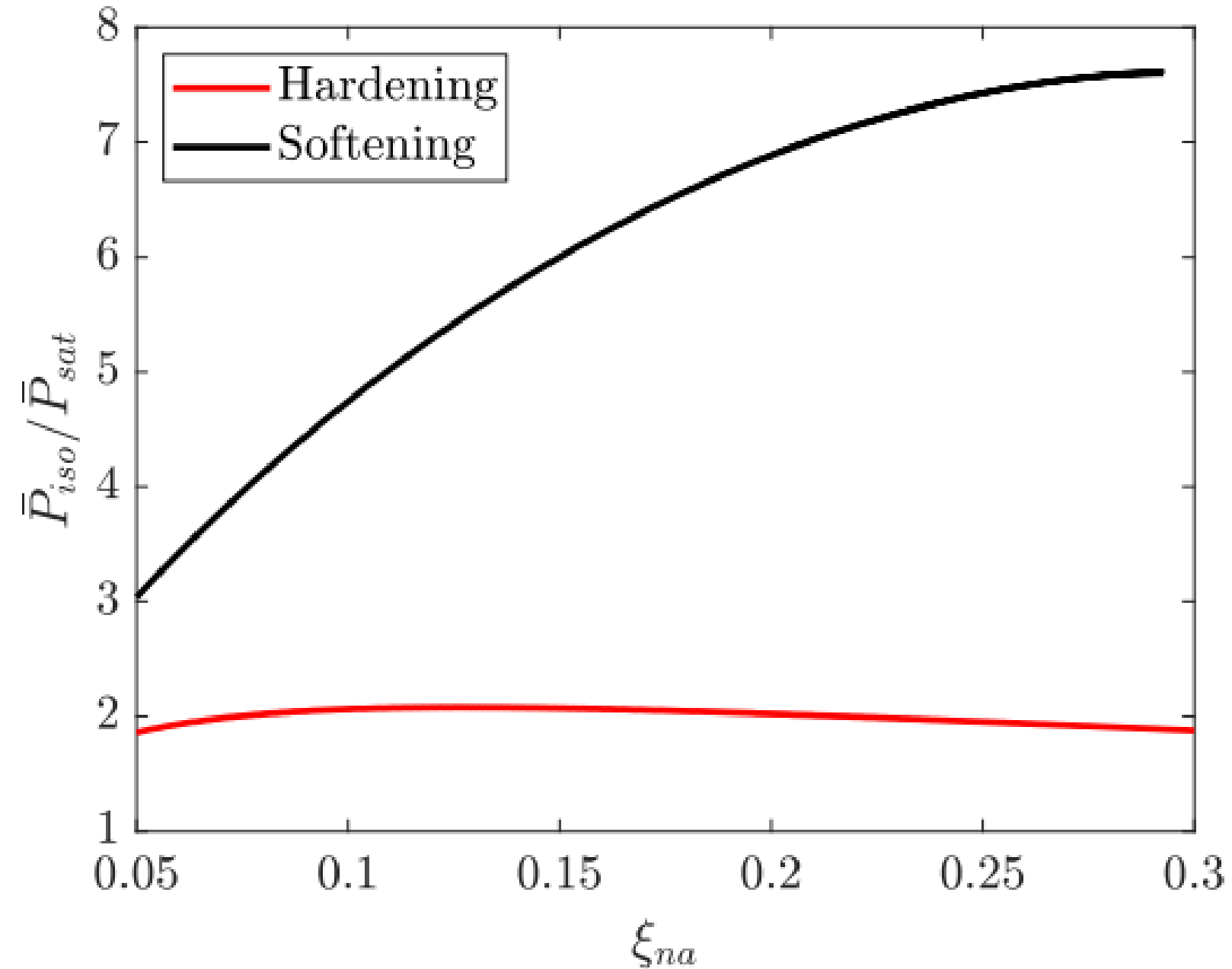
Larger force
range for saturation



FORCE RANGE INDEX

Ratio of: Force when Isola appear/ Force when saturation starts

Larger force range for saturation

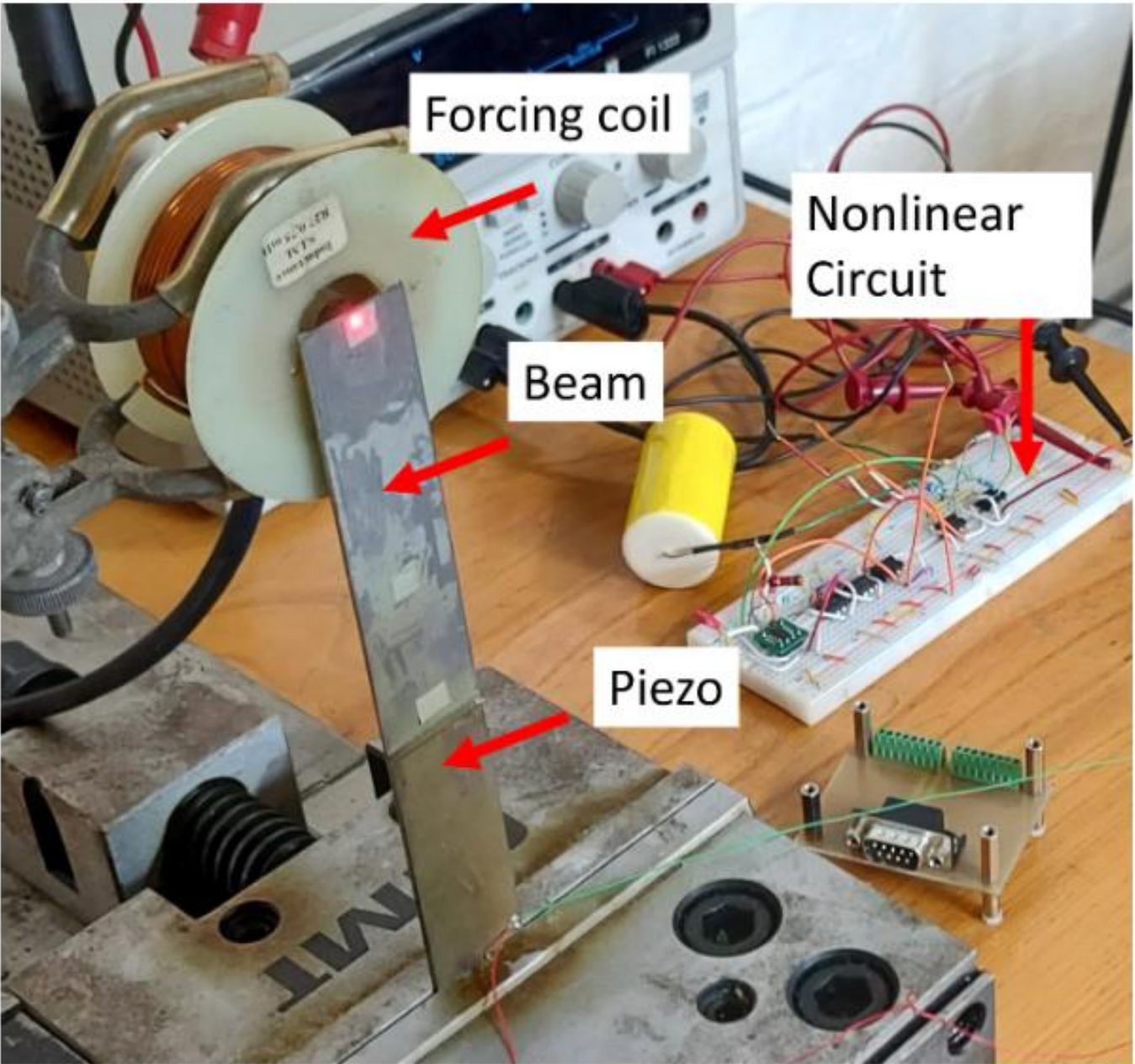
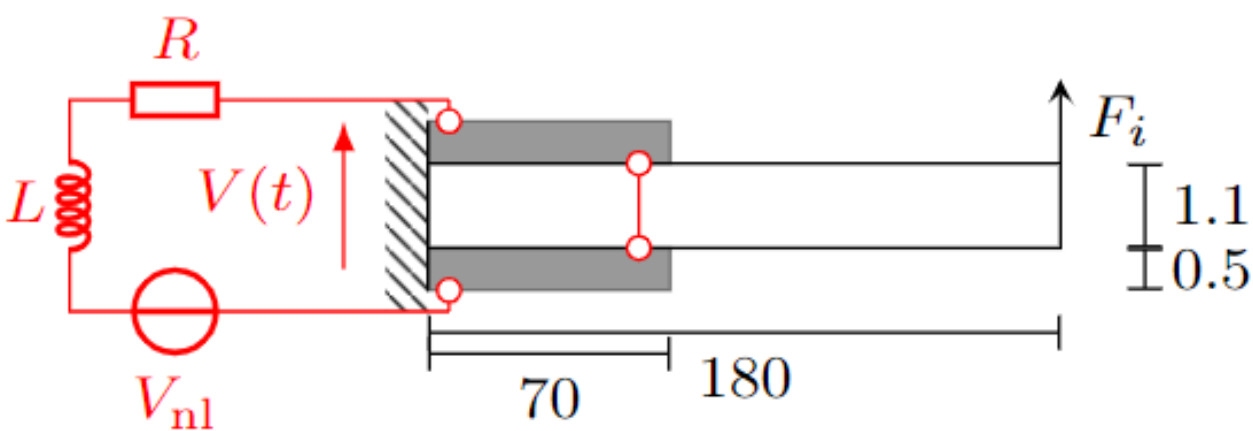
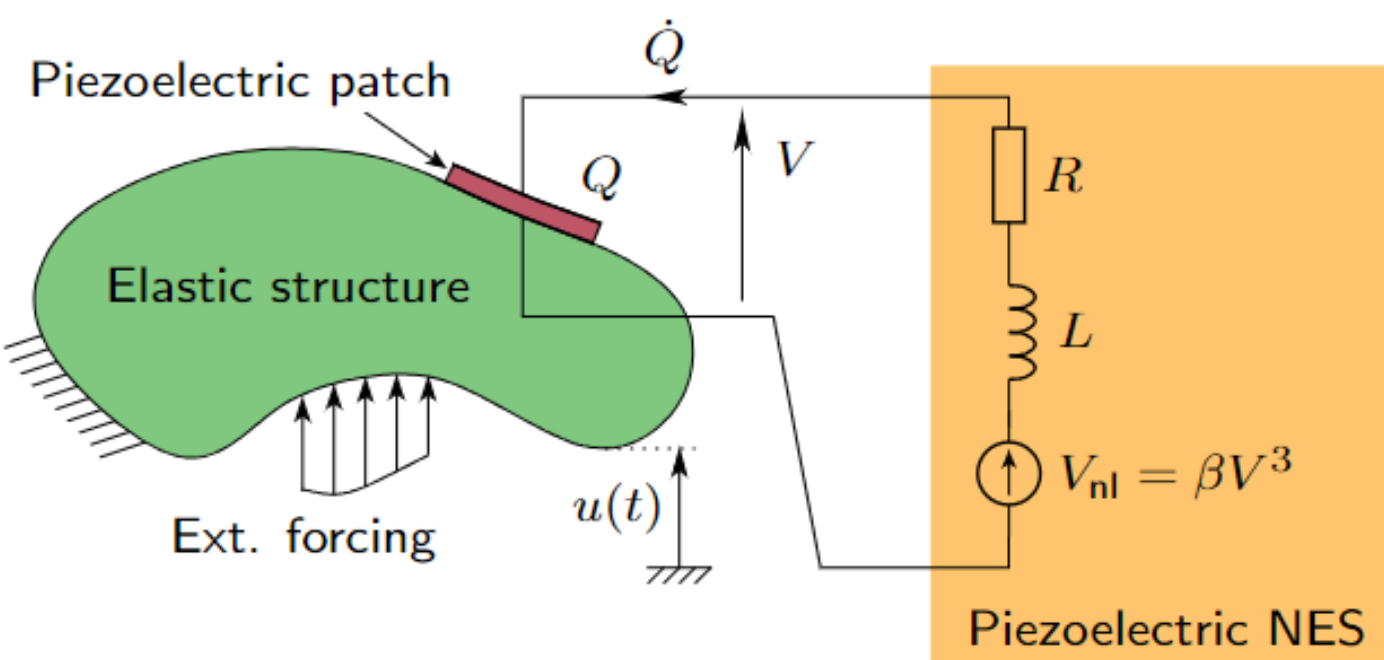


(c) Force Range Index

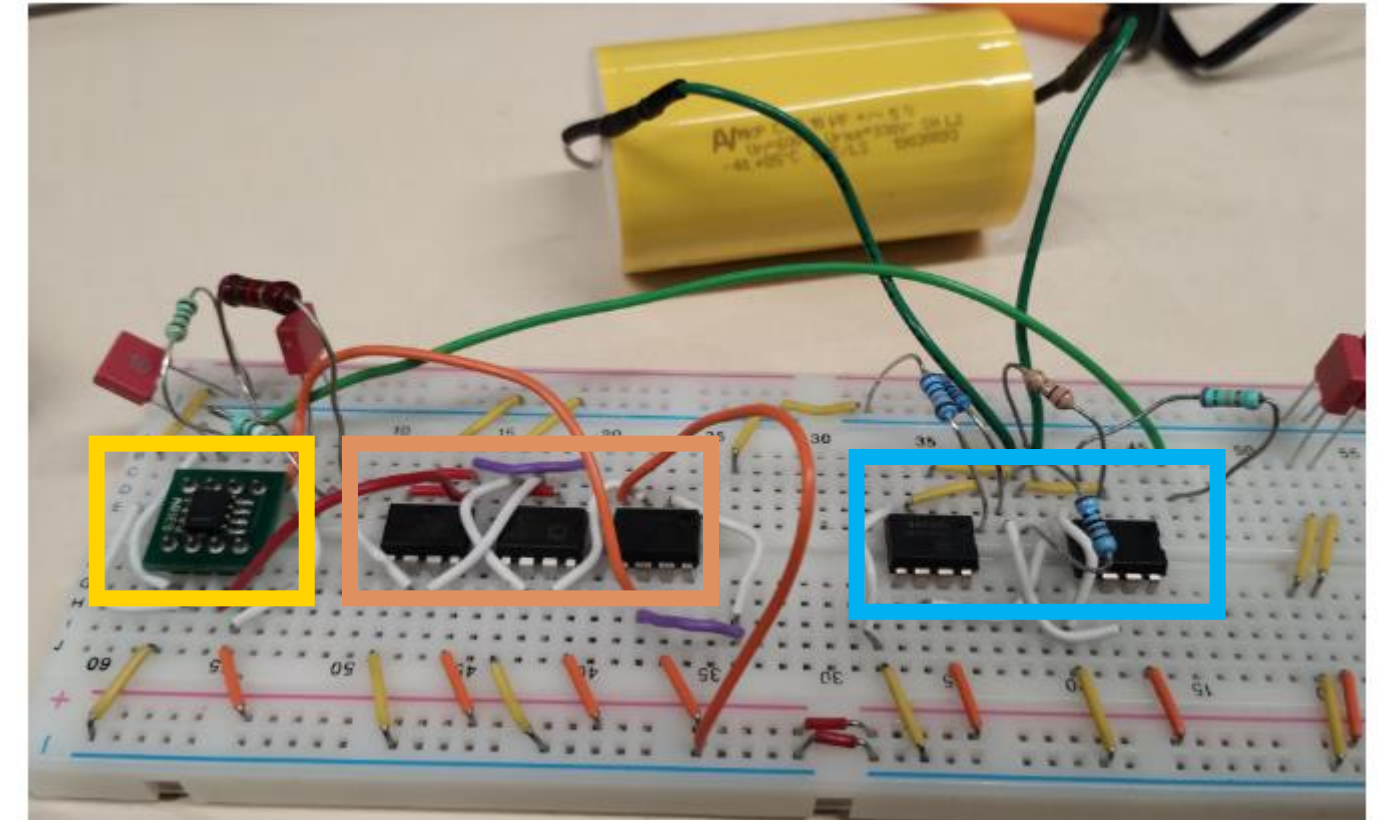
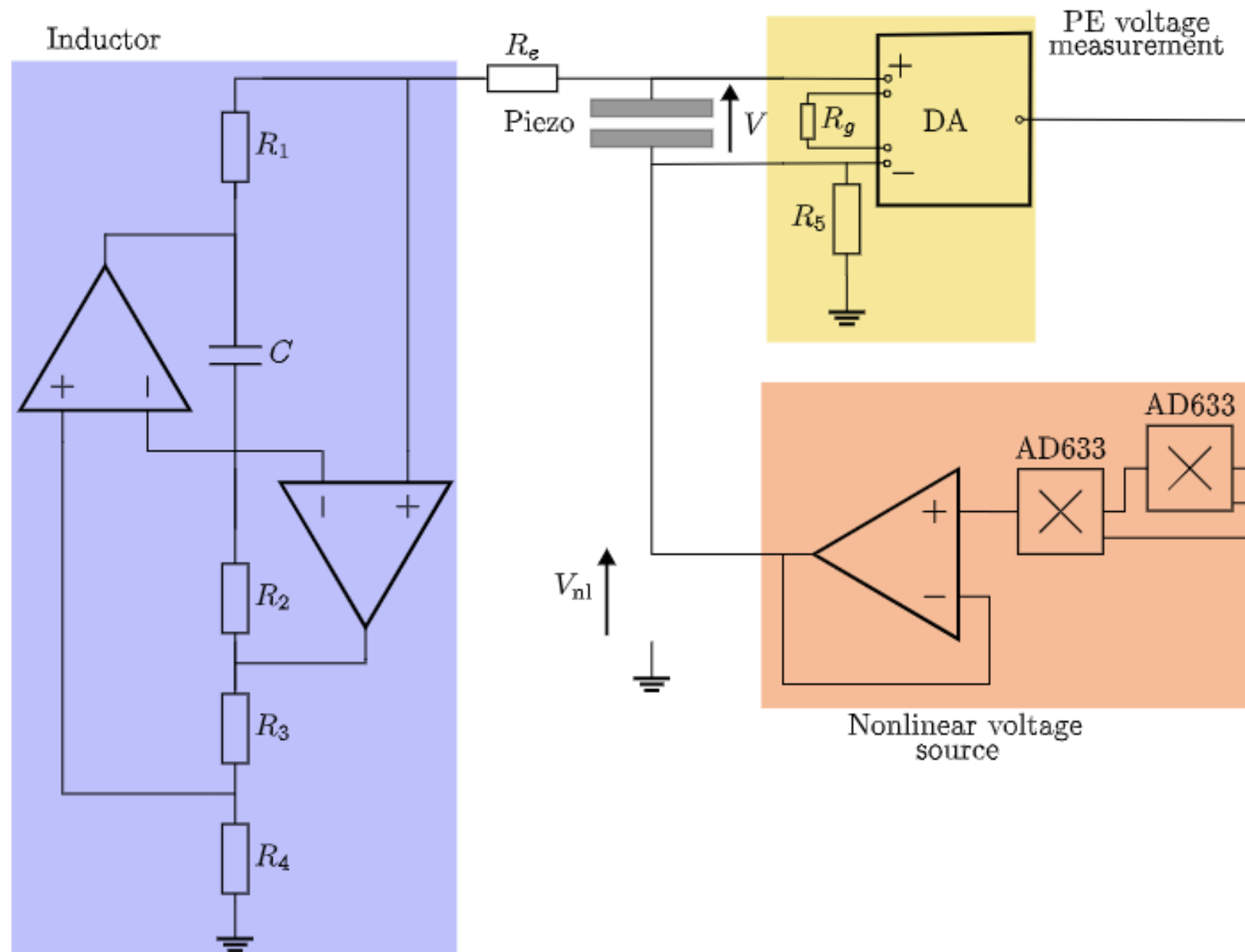
CONTENT

- Resonance Capture Cascade (Transient Load)
- Practical realization
- Harmonic load: Hardening
- Harmonic load: Softening
- **Piezoelectrical NES**

PIEZOELECTRICAL NES

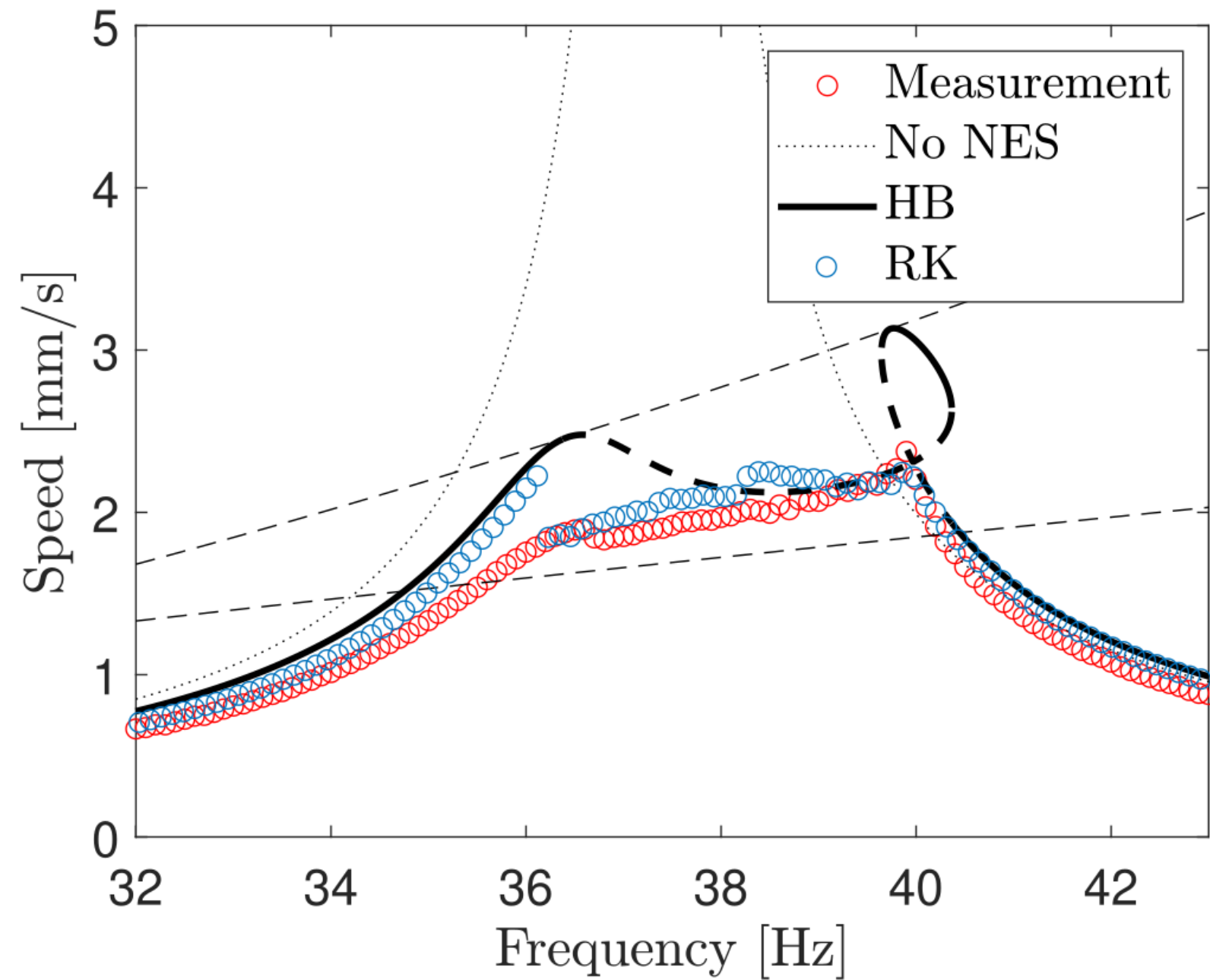


CIRCUIT NONLINEAR

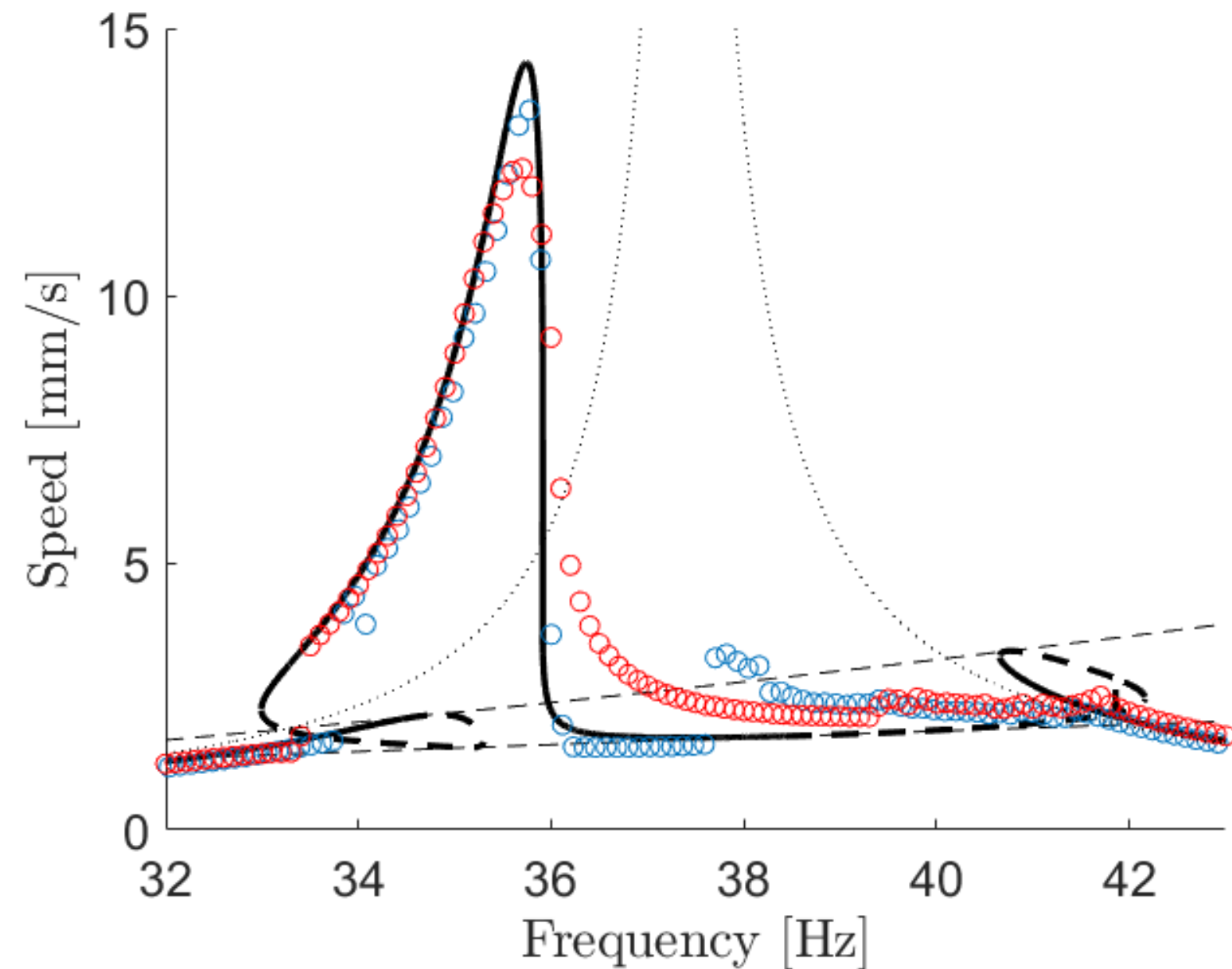


MEASUREMENT AND THEORY

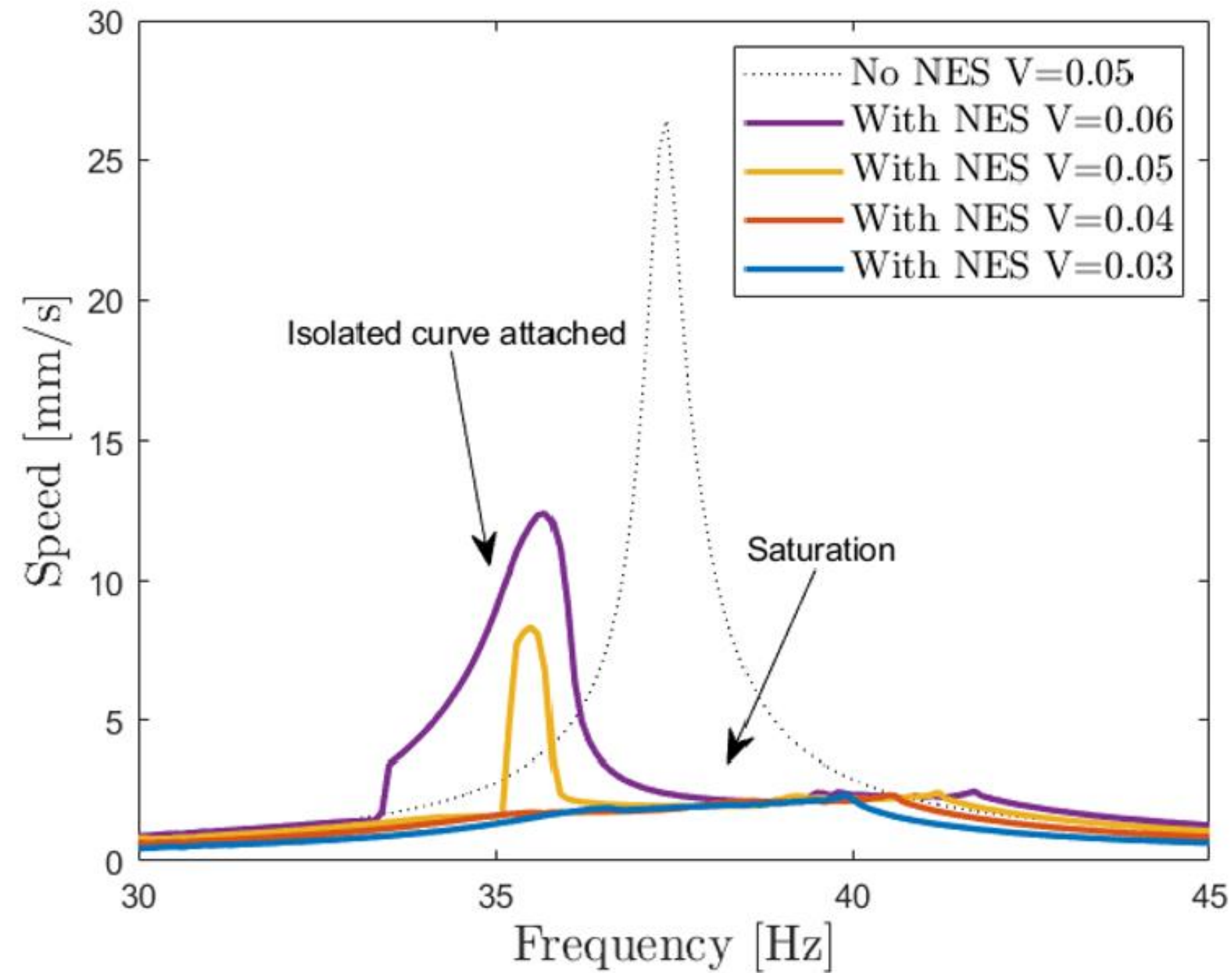
$F = 0,584 \text{ mN}$

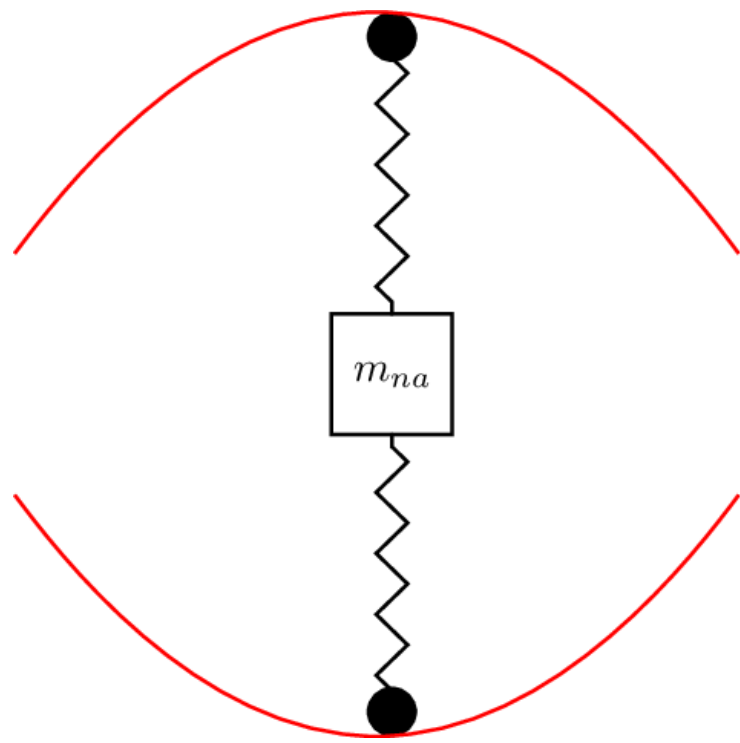


$F = 0,945 \text{ mN}$



SATURATION: EXPERIMENT





THANKS FOR LISTENING

Kevin Dekemele

kevin.dekemele@ugent.be

www.kevindekemele.com

