



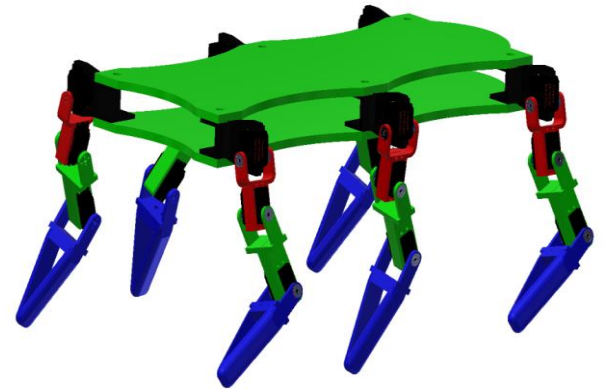
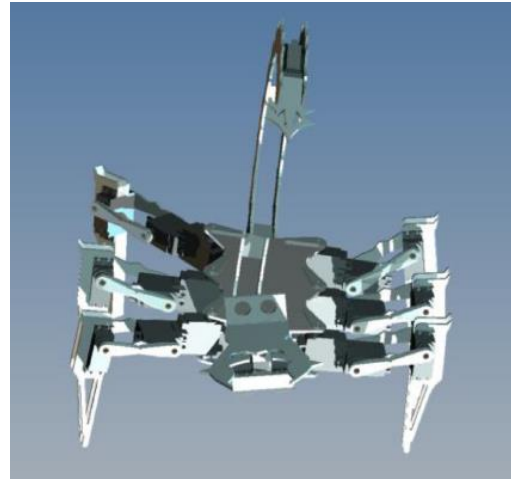
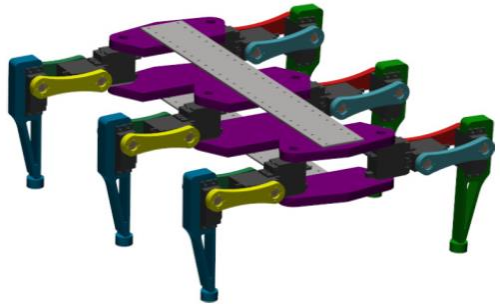
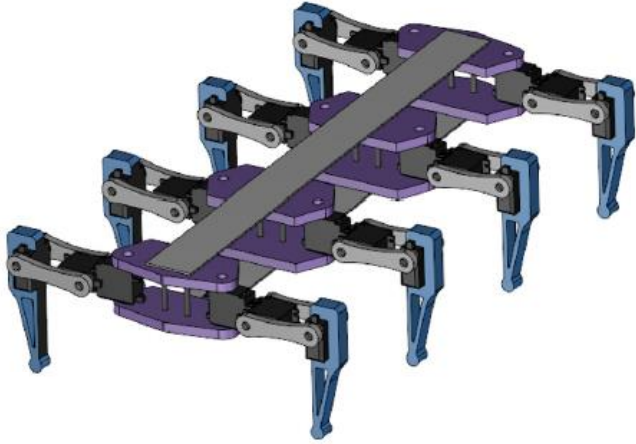
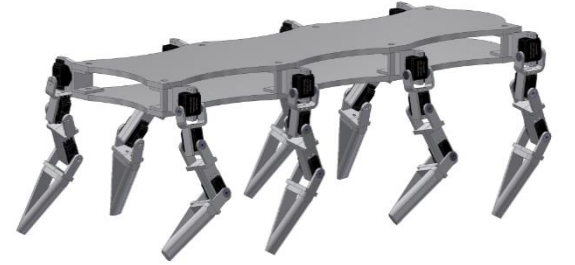
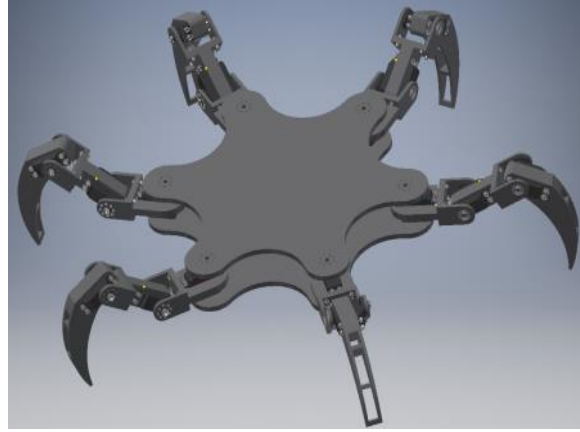
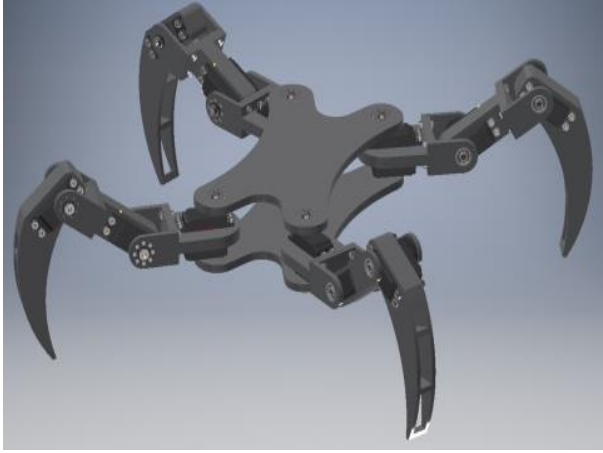
Modelowanie, analiza i wizualizacja maszyn koczających w środowisku Mathematica

Dr hab. inż. Dariusz Grzelczyk

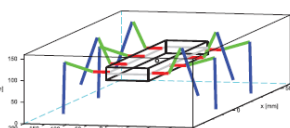
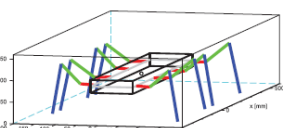
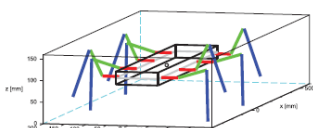
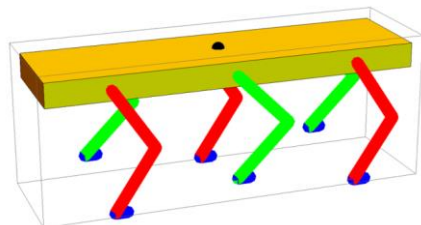
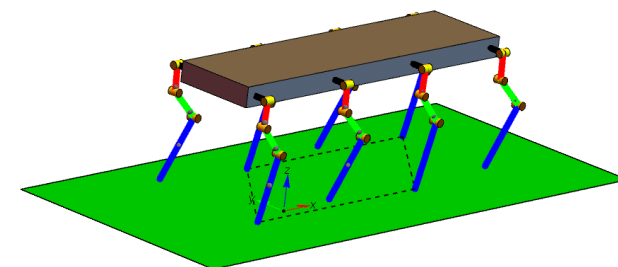
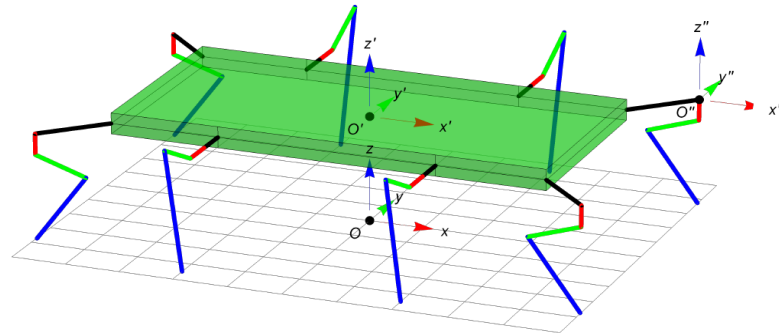
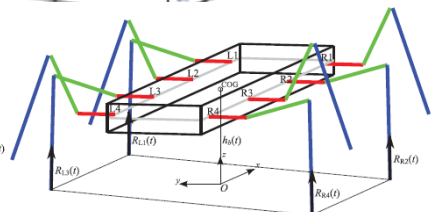
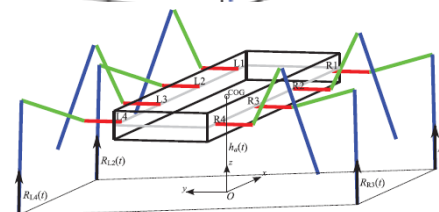
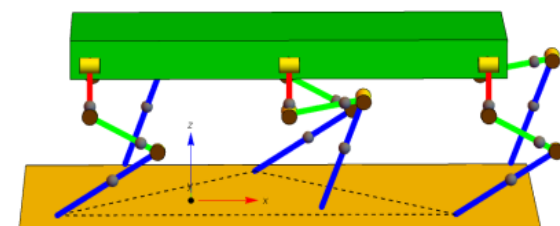
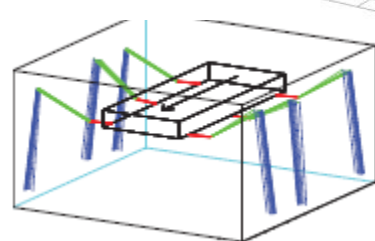
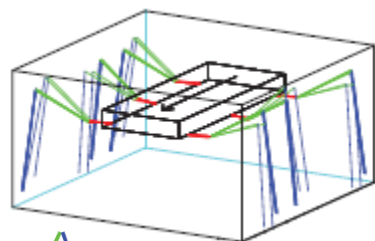
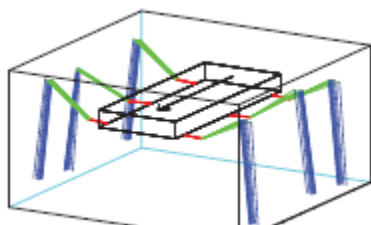
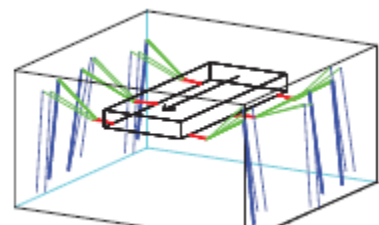
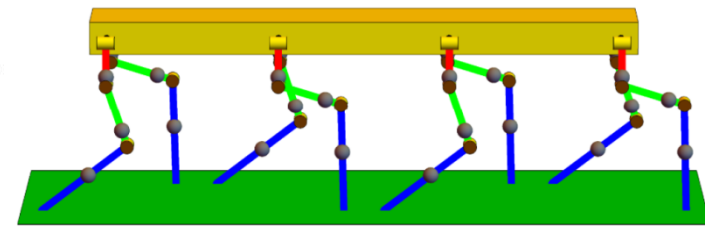
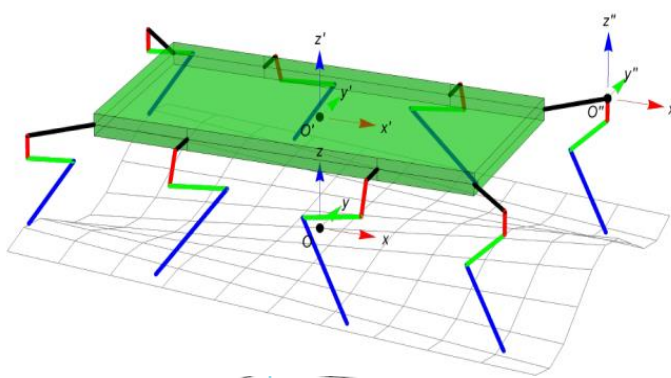
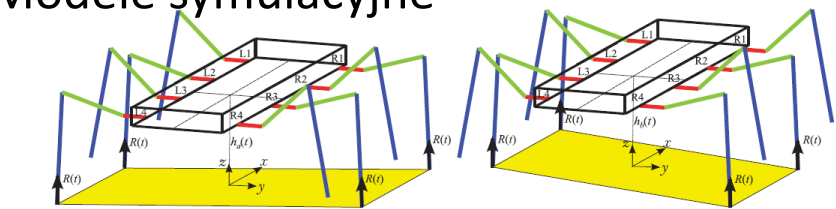
Katedra Automatyki, Biomechaniki i Mechatroniki

- Modelowanie matematyczne kinematyki i dynamiki maszyn koczających wzorowanych biologicznie na owadach i ssakach o różnej liczbie kończyn.
- Przedstawienie różnych wzorców chodu i zbadanie ich wpływu na kinematykę, dynamikę i stabilność robota koczającego w trakcie chodu.
- Opracowanie i sterowanie konstrukcji maszyny koczającej jako stacjonarnej lub mobilnej platformy Stewarta oraz jej stabilizacja na drgającym i niestabilnym podłożu.

Modele CAD



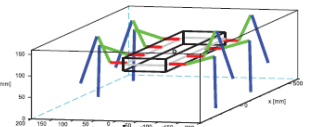
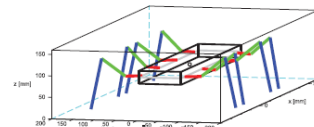
Modele symulacyjne



$t=0$

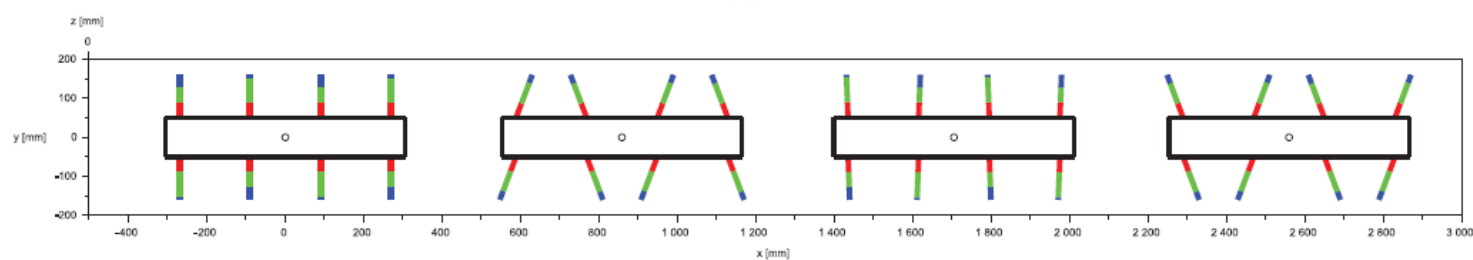
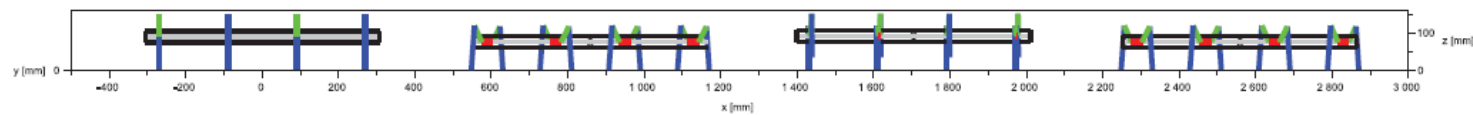
$t=0.25T$

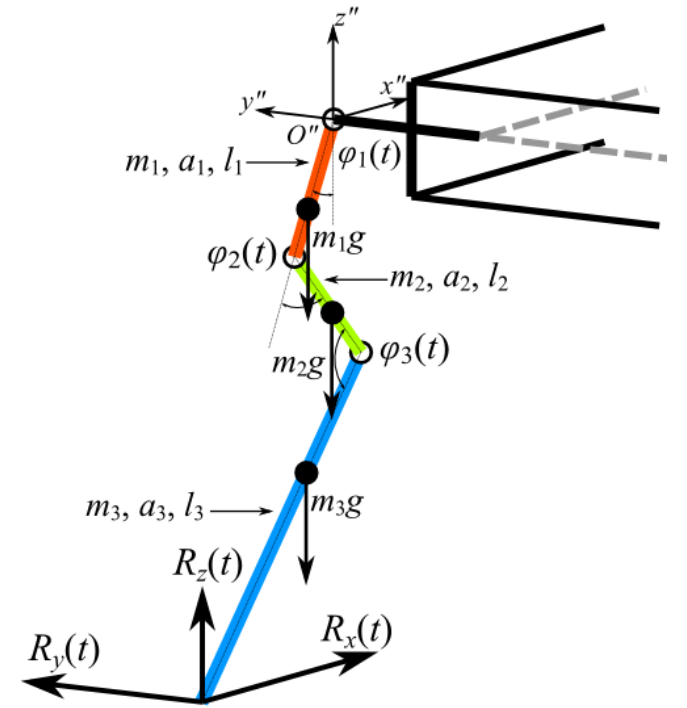
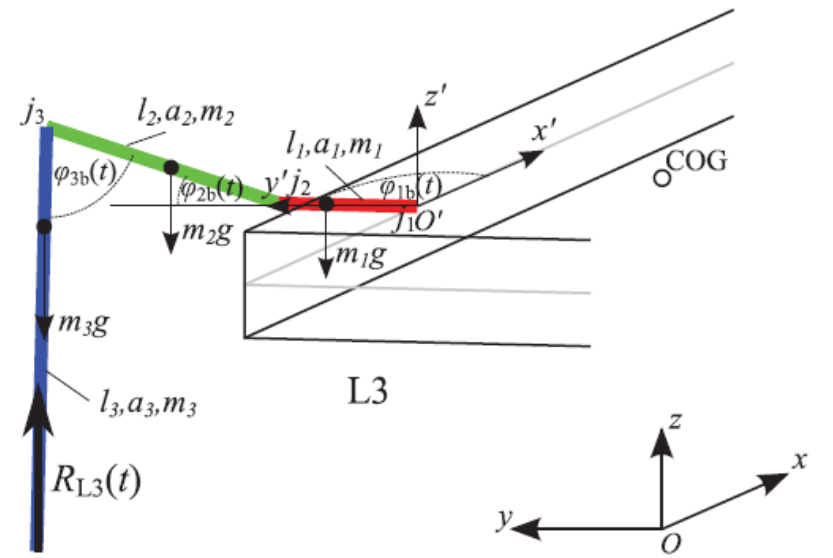
$t=0.50T$

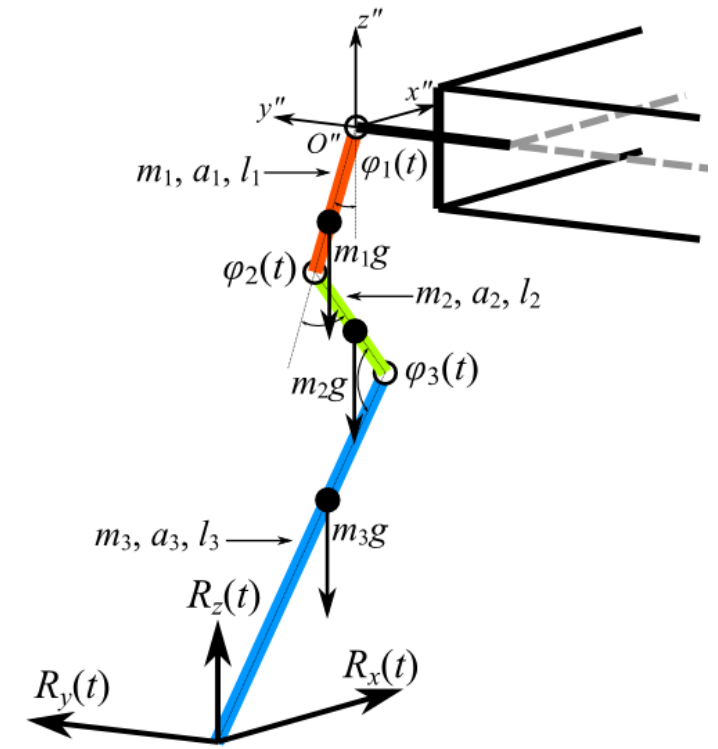
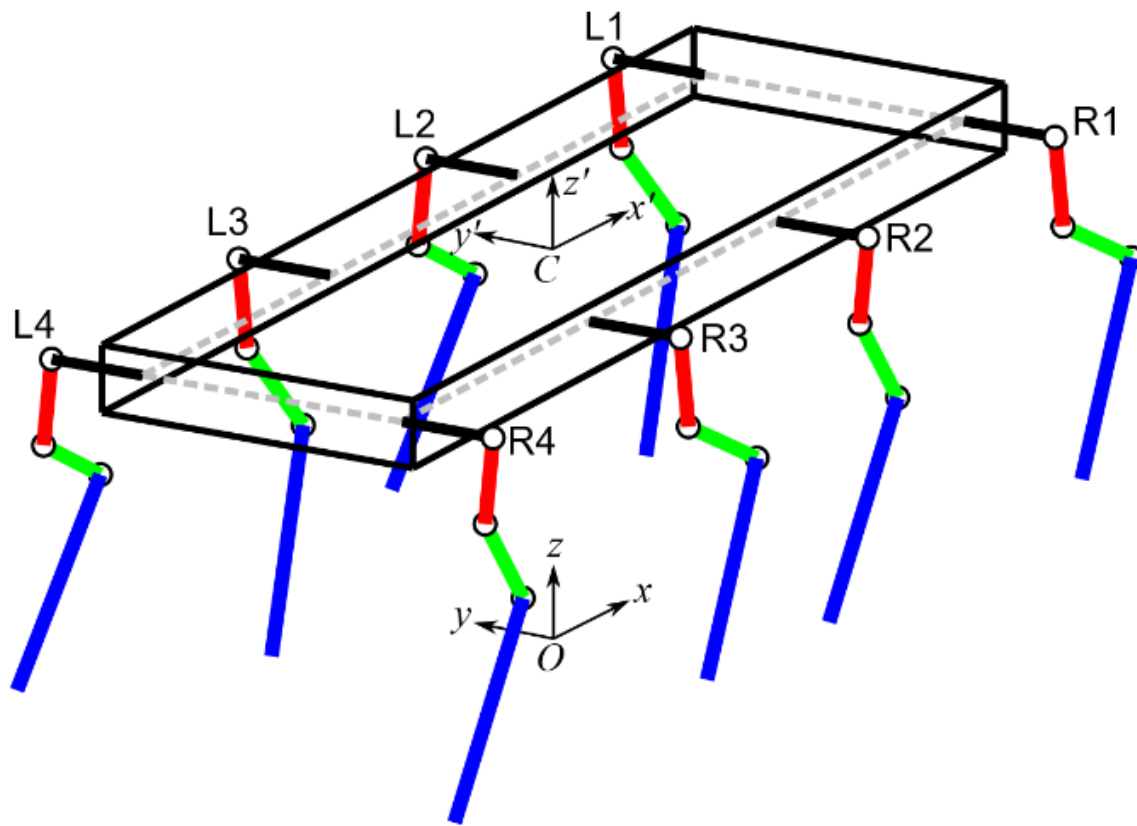


$t=0.75T$

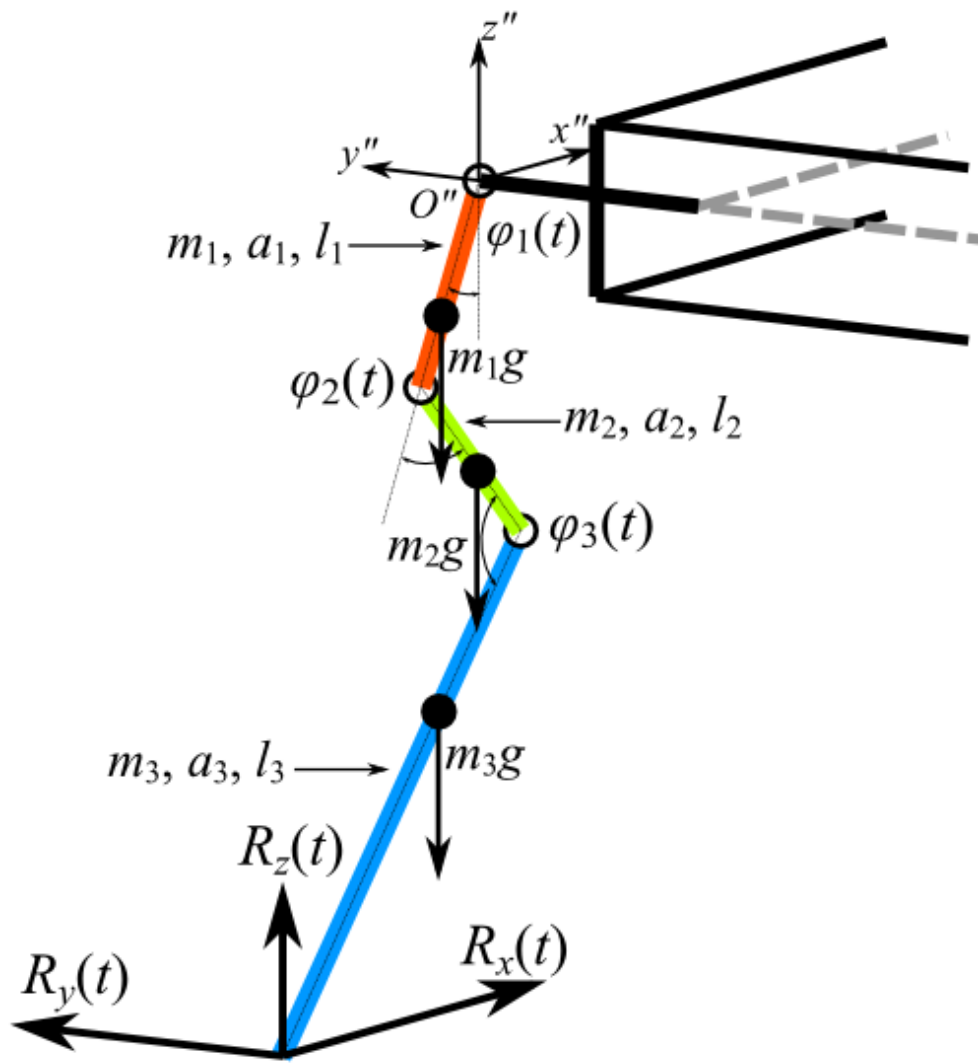
$t=1.00T$







Parameters	Symbol	Unit	Value
Mass of the trunk (without legs)	M	[kg]	1.0
Masses of legs' links (with servos)	$m_1; m_2; m_3$	[kg]	0.111; 0.140; 0.124
Lengths of legs' links	$l_1; l_2; l_3$	[m]	0.065; 0.100; 0.165
Positions of links' mass centers	$a_1; a_2; a_3$	[m]	0.052; 0.075; 0.075
Distances between the legs	$L; H$	[m]	0.263; 0.210



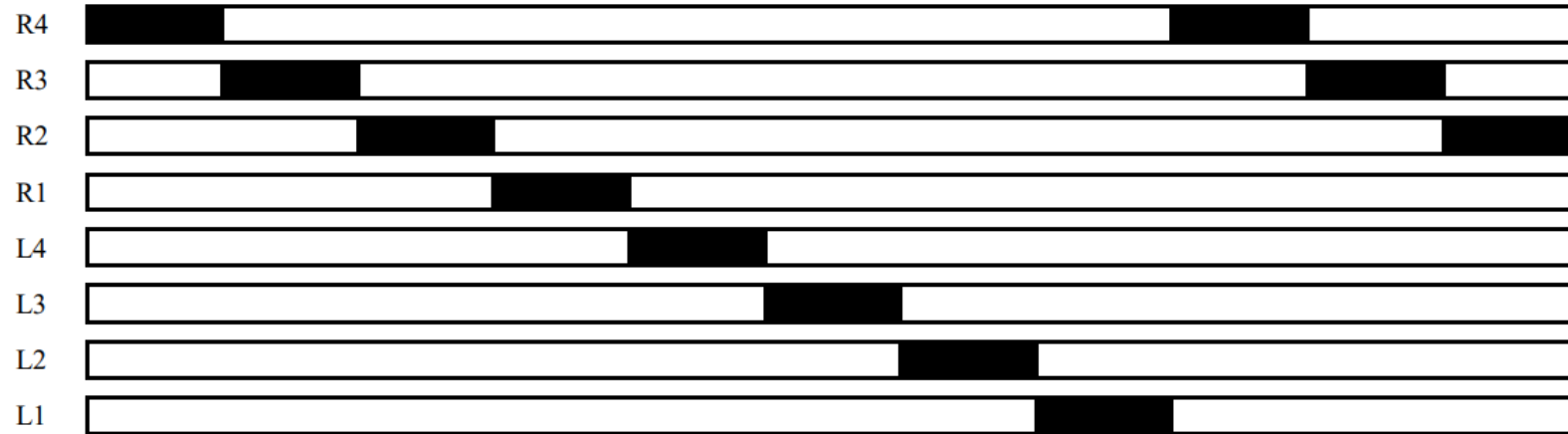
$$\begin{cases} x''(t) = l_2 \sin \varphi_2(t) - l_3 \sin(\pi - \varphi_2(t) - \varphi_3(t)), \\ y''(t) = (-l_1 - l_2 \cos \varphi_2(t) - l_3 \cos(\pi - \varphi_2(t) - \varphi_3(t))) \sin \varphi_1(t), \\ z''(t) = (-l_1 - l_2 \cos \varphi_2(t) - l_3 \cos(\pi - \varphi_2(t) - \varphi_3(t))) \cos \varphi_1(t), \end{cases}$$

$$\begin{cases} \varphi_1(t) = \operatorname{atan} \left(\frac{y''(t)}{-z''(t)} \right), \\ \varphi_2(t) = \operatorname{atan} \left(\frac{x''(t)}{d_1(t)} \right) + \operatorname{acos} \left(\frac{l_2^2 + [d_2(t)]^2 - l_3^2}{2l_2 d_2(t)} \right), \\ \varphi_3(t) = \operatorname{acos} \left(\frac{l_2^2 + l_3^2 - [d_2(t)]^2}{2l_2 l_3} \right), \end{cases}$$

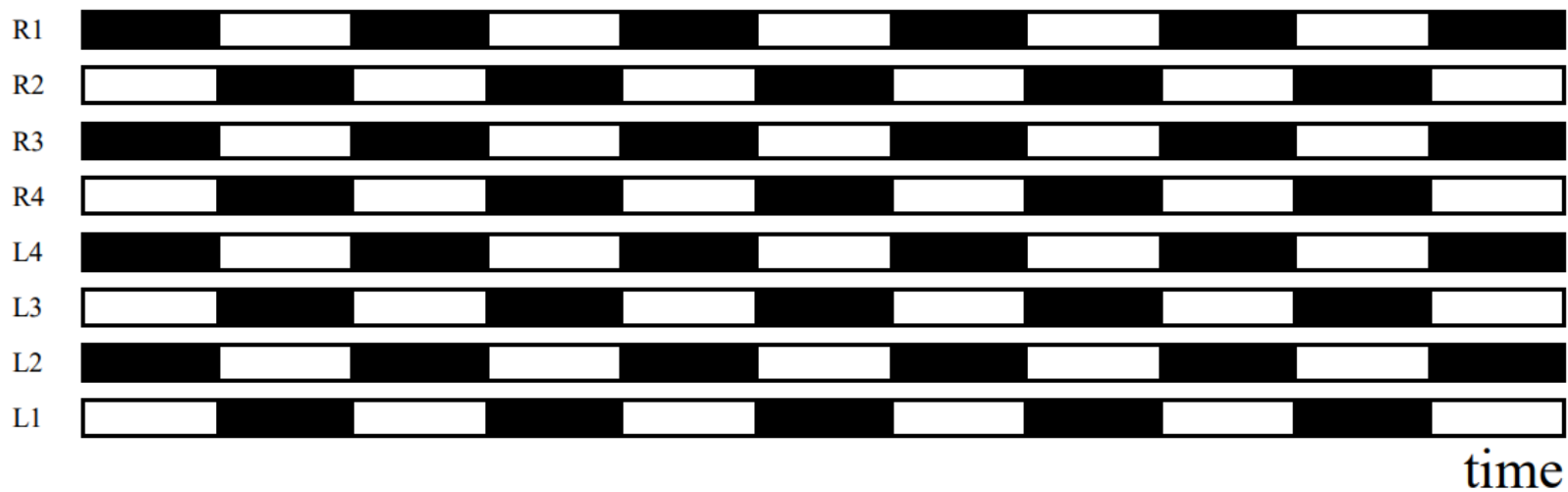
$$d_1(t) = \sqrt{[y''(t)]^2 + [z''(t)]^2} - l_1$$

$$d_2(t) = \sqrt{[d_1(t)]^2 + [x''(t)]^2}$$

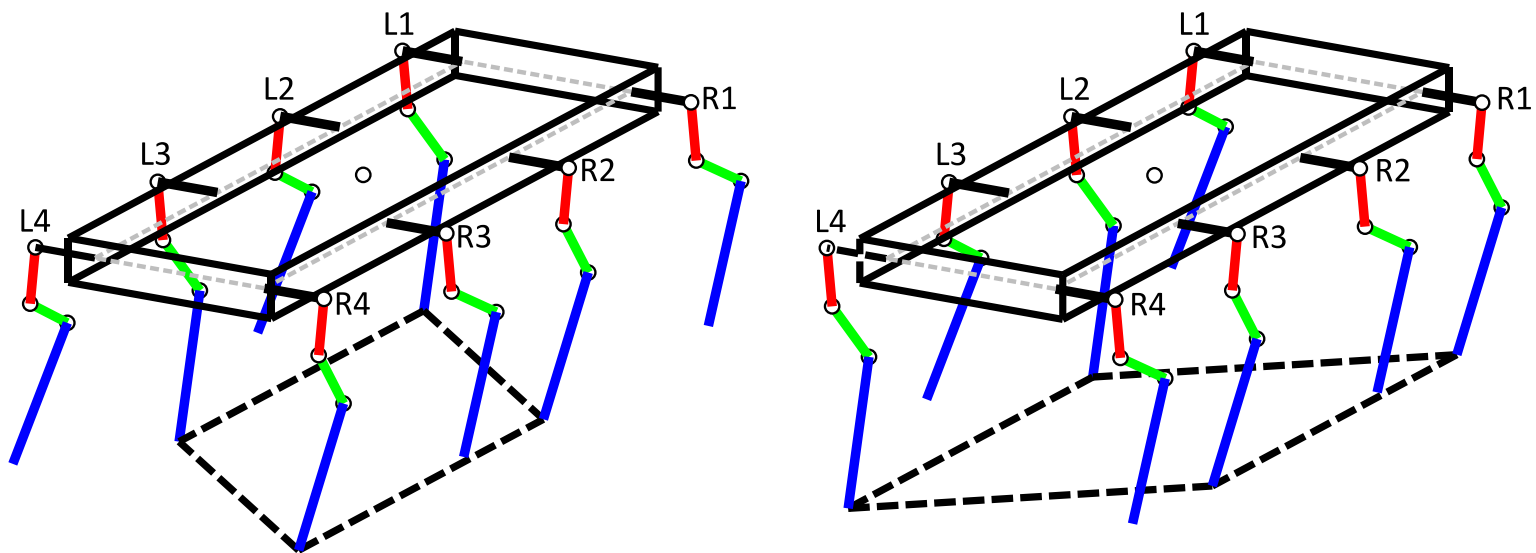
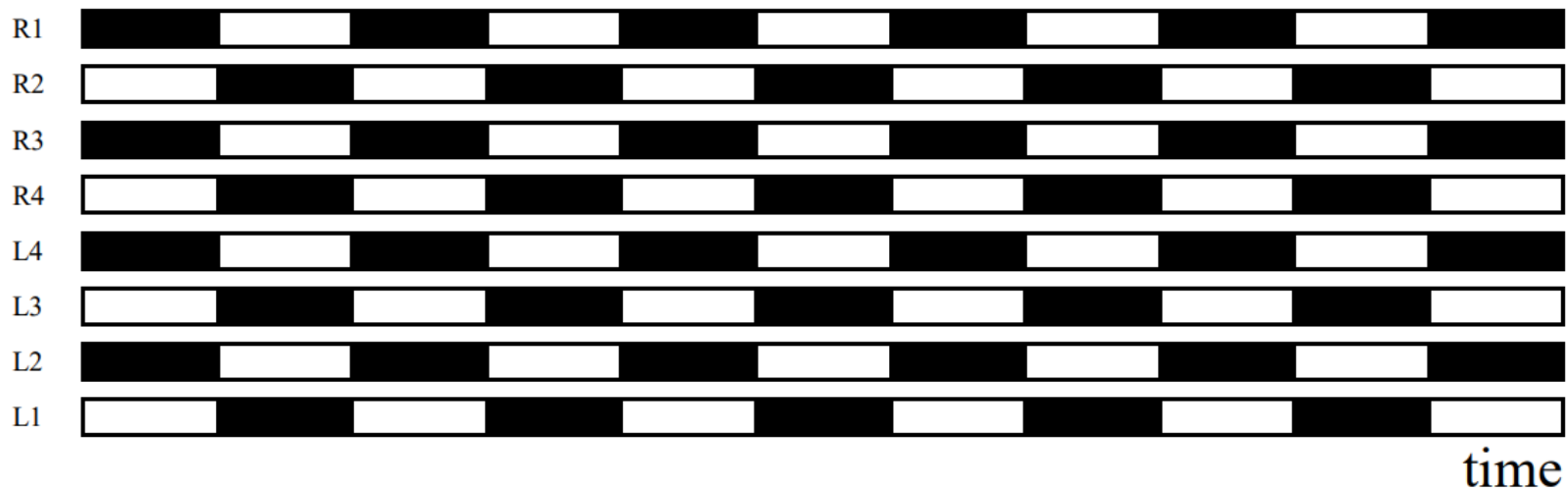
(a) wave gait ($\beta = 7/8$)



(b) tetrapod gait ($\beta = 1/2$)



(b) tetrapod gait ($\beta = 1/2$)



Wzorce chodu

CPG1: Two uncoupled Hopf oscillators

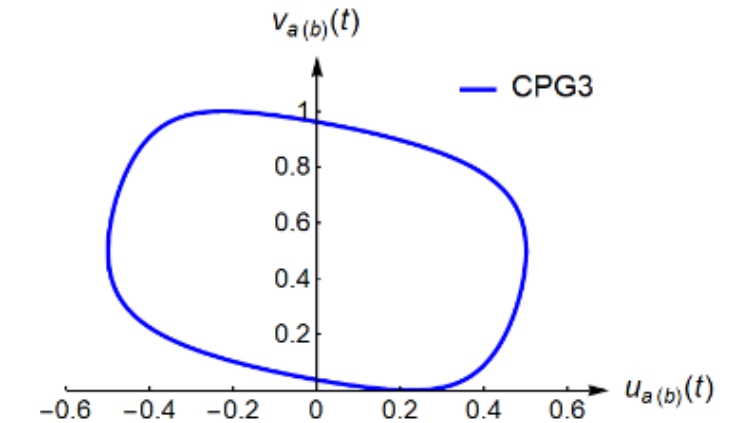
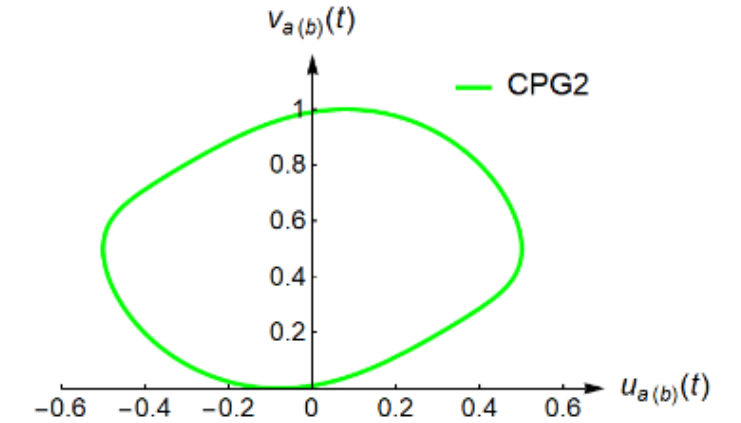
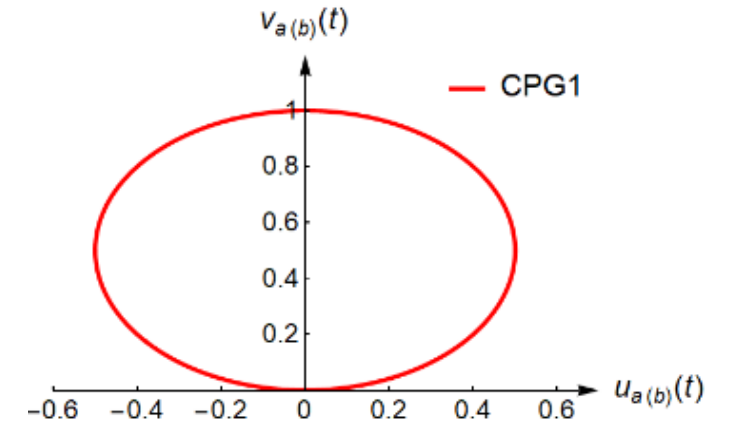
$$\begin{cases} \dot{u}_a(t) = (\sigma - u_a^2(t) - v_a^2(t))u_a(t) + \omega v_a(t), \\ \dot{v}_a(t) = (\sigma - u_a^2(t) - v_a^2(t))v_a(t) - \omega u_a(t), \\ \dot{u}_b(t) = (\sigma - u_b^2(t) - v_b^2(t))u_b(t) + \omega v_b(t), \\ \dot{v}_b(t) = (\sigma - u_b^2(t) - v_b^2(t))v_b(t) - \omega u_b(t), \end{cases}$$

CPG2: Two uncoupled hybrid van der Pol-Rayleigh oscillators

$$\begin{cases} \dot{u}_a(t) = v_a(t), \\ \dot{v}_a(t) = \varepsilon(1 - u_a^2(t))v_a(t) + \delta(1 - v_a^2(t))v_a(t) - \omega^2 u_a(t), \\ \dot{u}_b(t) = v_b(t), \\ \dot{v}_b(t) = \varepsilon(1 - u_b^2(t))v_b(t) + \delta(1 - v_b^2(t))v_b(t) - \omega^2 u_b(t), \end{cases}$$

CPG3: The Toda-Rayleigh lattice

$$\begin{cases} \dot{u}_a(t) = v_a(t), \\ \dot{v}_a(t) = \omega^2 \left(e^{u_b(t) - u_a(t)} - e^{u_a(t) - u_b(t)} \right) + \eta(1 - v_a^2(t))v_a(t), \\ \dot{u}_b(t) = v_b(t), \\ \dot{v}_b(t) = \omega^2 \left(e^{u_a(t) - u_b(t)} - e^{u_b(t) - u_a(t)} \right) + \eta(1 - v_b^2(t))v_b(t), \end{cases}$$



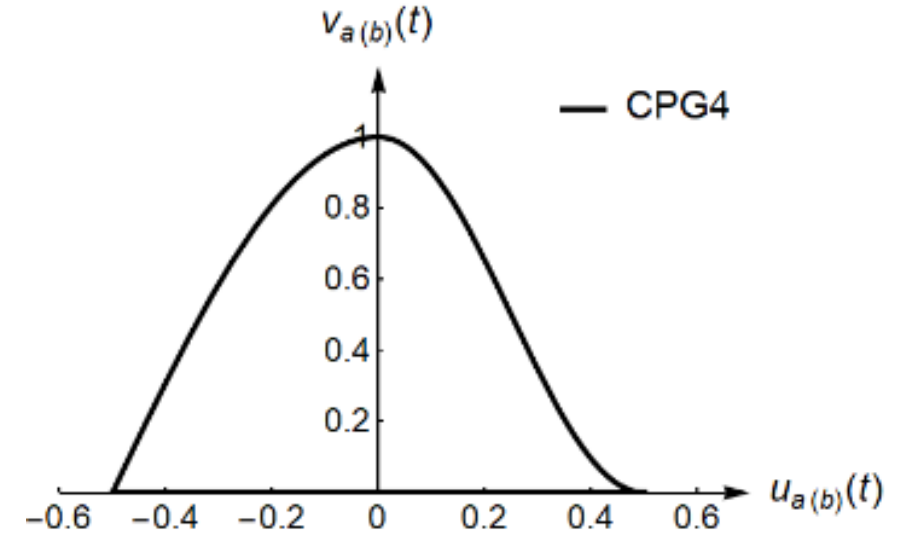
Zaproponowany wzorzec chodu

$$\begin{cases} u_a(t) = f_x(\text{mod}[t, T]), \\ v_a(t) = f_{za}(\text{mod}[t, T]), \\ u_b(t) = -u_1(t), \\ v_b(t) = f_{zb}(\text{mod}[t, T]), \end{cases}$$

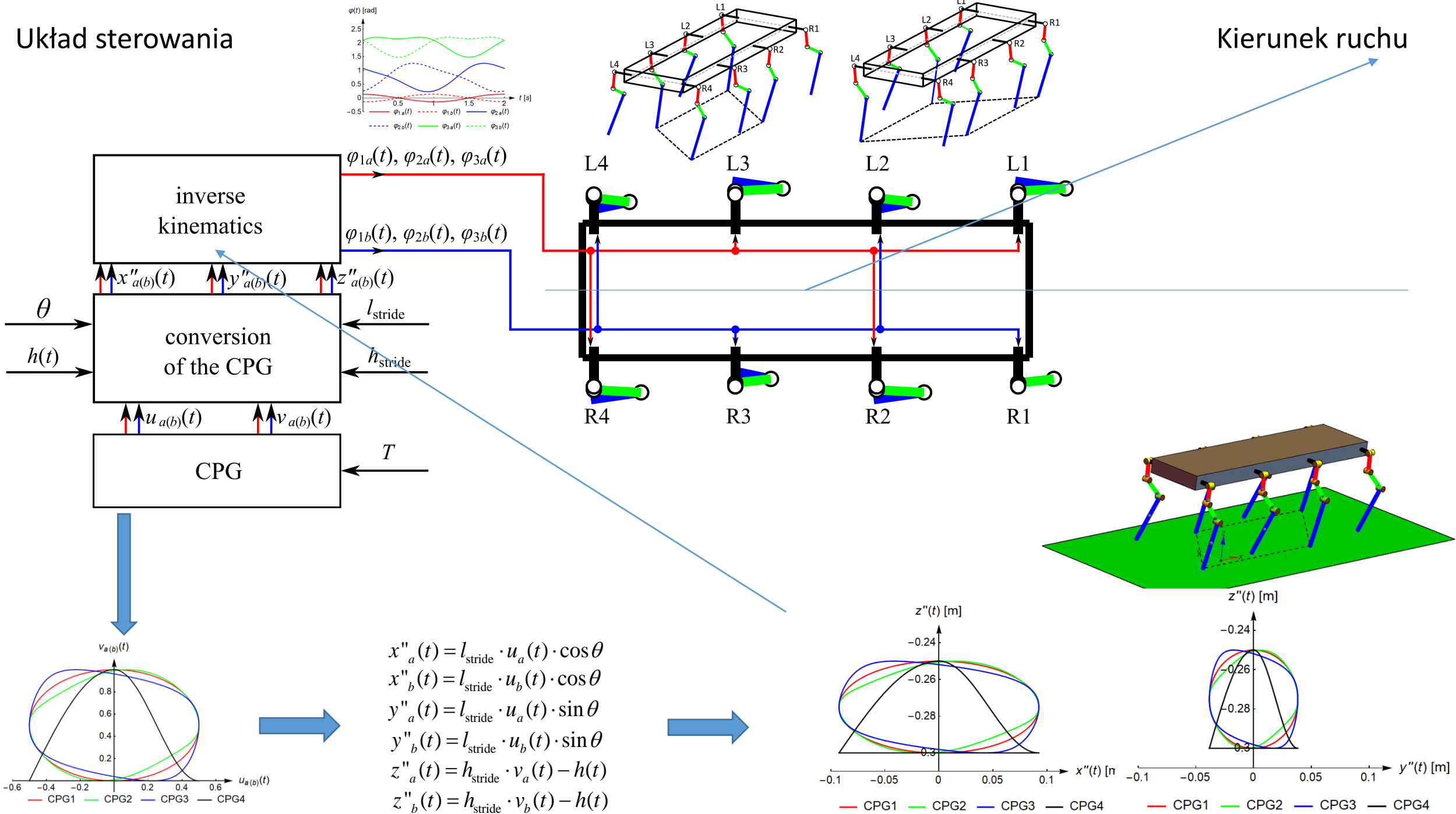
$$f_x(t) = \begin{cases} \frac{2}{T}t & \text{if } t \in [0, 0.25T], \\ \frac{1}{2} - \frac{2}{T}(t - 0.25T) & \text{if } t \in (0.25T, 0.75T], \\ -\frac{1}{2} + \frac{2}{T}(t - 0.75T) & \text{if } (0.75T, T], \end{cases}$$

$$f_{za}(t) = \begin{cases} \sin^2\left(\frac{2\pi}{T}(t + 0.25T)\right) & \text{if } t \in [0, 0.25T], \\ 0 & \text{if } t \in (0.25T, 0.75T], \\ -\sin\left(\frac{2\pi}{T}(t + 0.75T)\right) & \text{if } (0.75T, T], \end{cases}$$

$$f_{zb}(t) = f_{za}(\text{mod}[t - 0.5T, T])$$



Układ sterowania

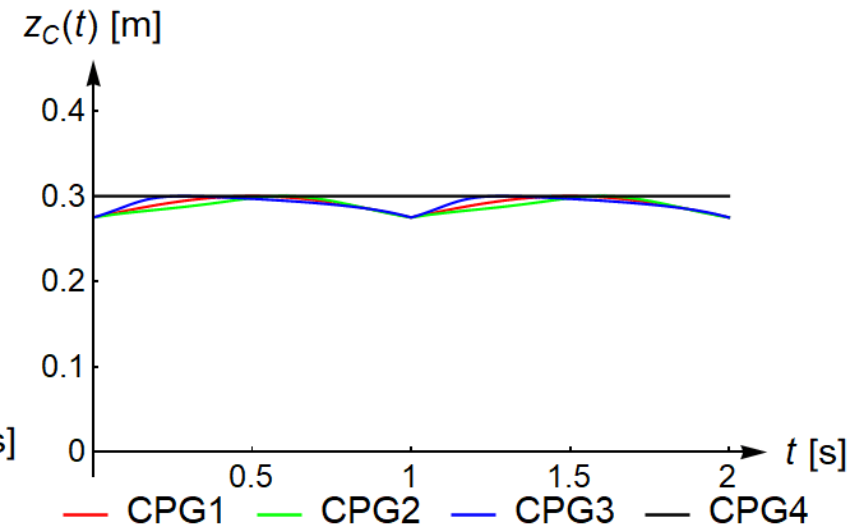
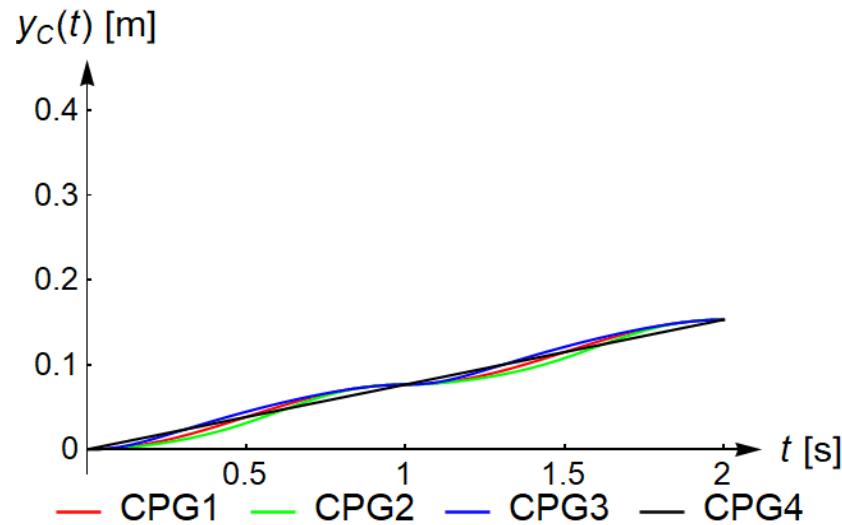
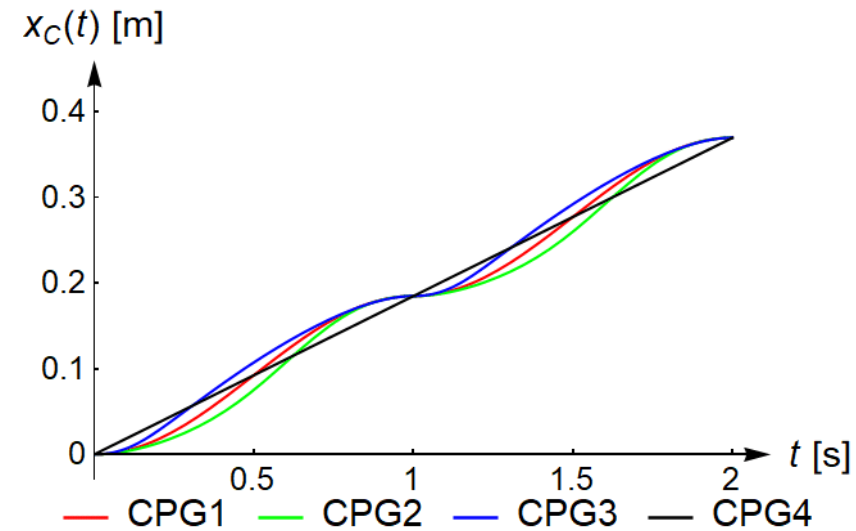


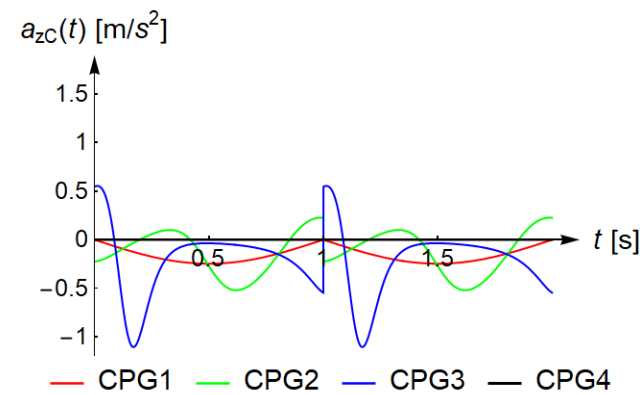
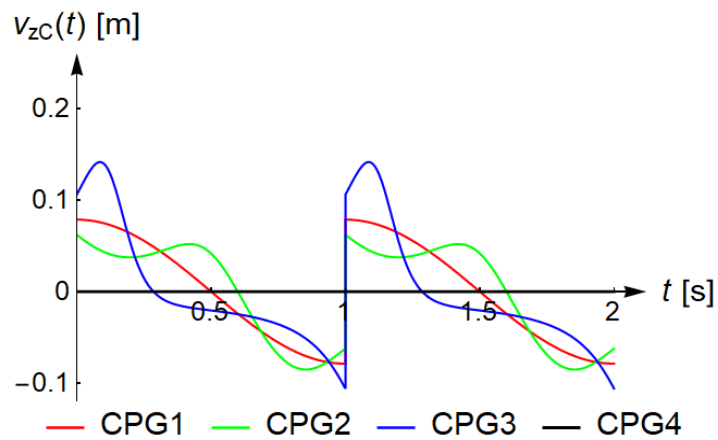
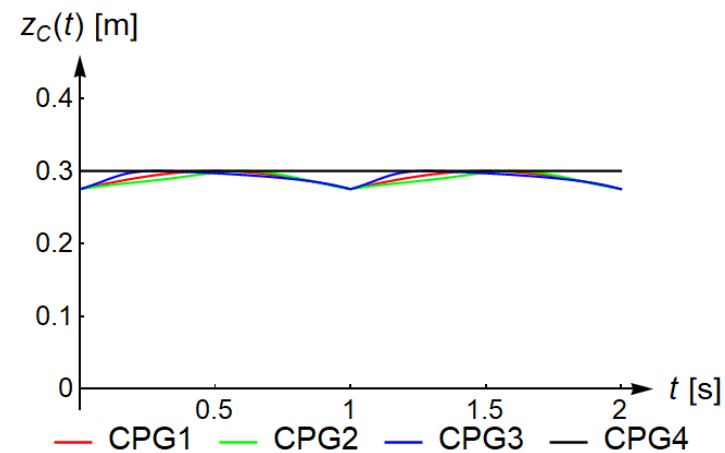
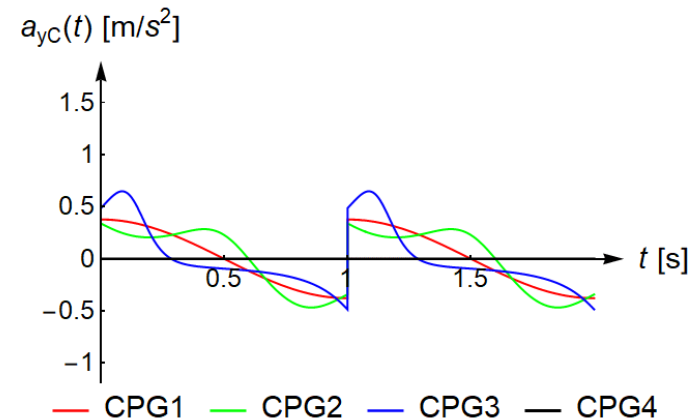
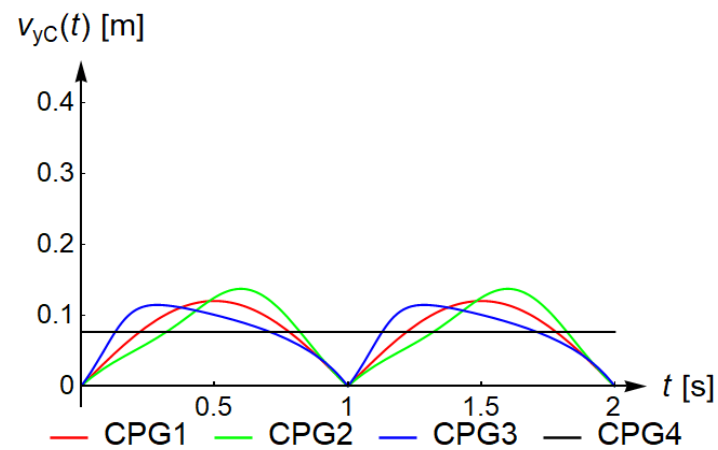
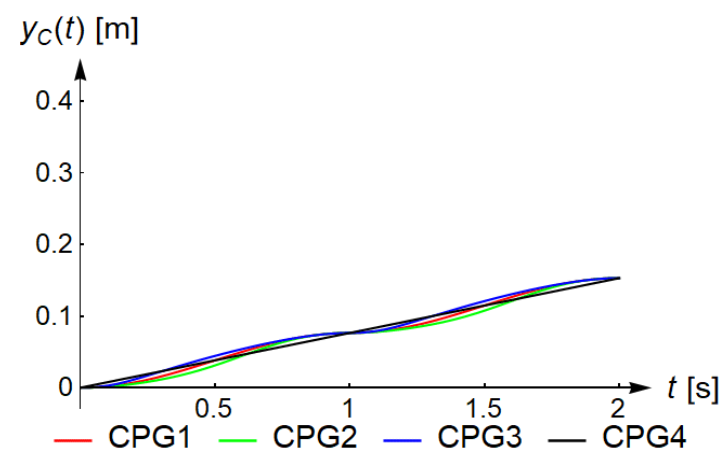
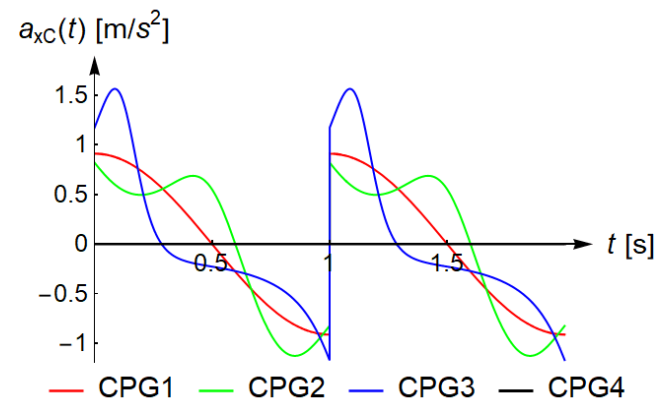
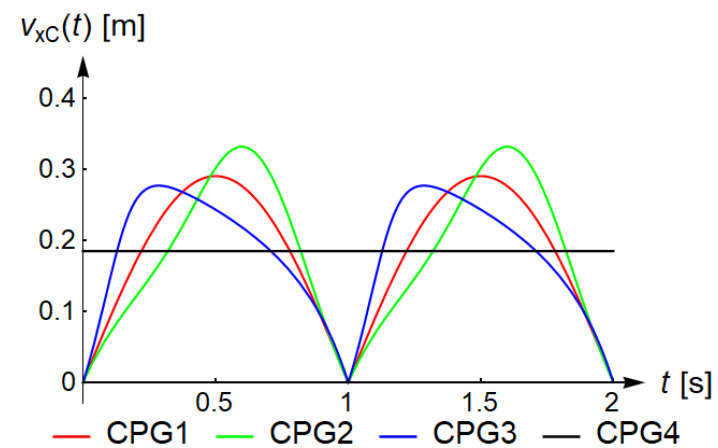
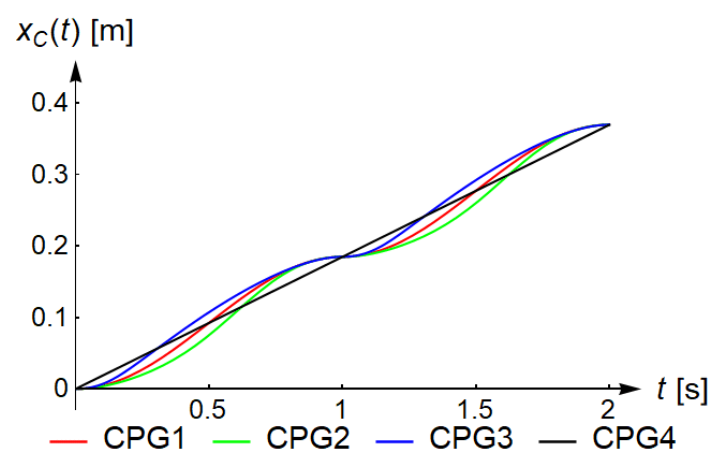
Kinematyka robota

$$x_C(t) = \int_0^t v_{x_C}(\tau) d\tau \quad y_C(t) = \int_0^t v_{y_C}(\tau) d\tau \quad z_C(t) = \begin{cases} -z''_a(t) & \text{if } |z''_a(t)| \geq |z''_b(t)|, \\ -z''_b(t) & \text{if } |z''_a(t)| < |z''_b(t)|, \end{cases}$$

gdzie:

$$v_{x_C}(t) = \begin{cases} -\dot{x}''_a(t) & \text{if } |z''_a(t)| \geq |z''_b(t)|, \\ -\dot{x}''_b(t) & \text{if } |z''_a(t)| < |z''_b(t)|, \end{cases} \quad v_{y_C}(t) = \begin{cases} -\dot{y}''_a(t) & \text{if } |z''_a(t)| \geq |z''_b(t)|, \\ -\dot{y}''_b(t) & \text{if } |z''_a(t)| < |z''_b(t)|. \end{cases}$$





COM:

$$x_{COM}(t) = \frac{(M + M_L)x_C(t) + \sum_{j=1}^4 \sum_{i=1}^3 m_i x_i^{(Lj)}(t) + \sum_{j=1}^4 \sum_{i=1}^3 m_i x_i^{(Rj)}(t)}{M + M_L + 8 \sum_{i=1}^3 m_i},$$

$$y_{COM}(t) = \frac{(M + M_L)y_C(t) + \sum_{j=1}^4 \sum_{i=1}^3 m_i y_i^{(Lj)}(t) + \sum_{j=1}^4 \sum_{i=1}^3 m_i y_i^{(Rj)}(t)}{M + M_L + 8 \sum_{i=1}^3 m_i},$$

$$z_{COM}(t) = \frac{(M + M_L)z_C(t) + \sum_{j=1}^4 \sum_{i=1}^3 m_i z_i^{(Lj)}(t) + \sum_{j=1}^4 \sum_{i=1}^3 m_i z_i^{(Rj)}(t)}{M + M_L + 8 \sum_{i=1}^3 m_i}.$$

ZMP:

$$x_{ZMP}(t) = \frac{\Sigma_A(t) - \Sigma_B(t)}{\Sigma_E(t)}$$

$$y_{ZMP}(t) = \frac{\Sigma_C(t) - \Sigma_D(t)}{\Sigma_E(t)}$$

$$\Sigma_A(t) = (M + M_L)(\ddot{z}_C(t) + g_z)x_C(t) + \sum_{j=1}^4 \sum_{i=1}^3 m_i \left(\ddot{z}_i^{(Lj)}(t) + g_z \right) x_i^{(Lj)}(t) + \sum_{j=1}^4 \sum_{i=1}^3 m_i \left(\ddot{z}_i^{(Rj)}(t) + g_z \right) x_i^{(Rj)}(t),$$

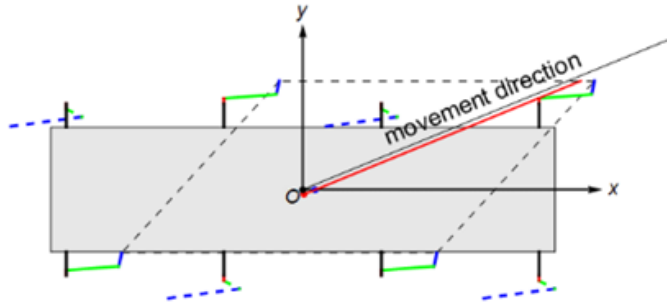
$$\Sigma_B(t) = (M + M_L)(\ddot{x}_C(t) + g_x)z_C(t) + \sum_{j=1}^4 \sum_{i=1}^3 m_i \left(\ddot{x}_i^{(Lj)}(t) + g_x \right) z_i^{(Lj)}(t) + \sum_{j=1}^4 \sum_{i=1}^3 m_i \left(\ddot{x}_i^{(Rj)}(t) + g_x \right) z_i^{(Rj)}(t),$$

$$\Sigma_C(t) = (M + M_L)(\ddot{z}_C(t) + g_z)y_C(t) + \sum_{j=1}^4 \sum_{i=1}^3 m_i \left(\ddot{z}_i^{(Lj)}(t) + g_z \right) y_i^{(Lj)}(t) + \sum_{j=1}^4 \sum_{i=1}^3 m_i \left(\ddot{z}_i^{(Rj)}(t) + g_z \right) y_i^{(Rj)}(t),$$

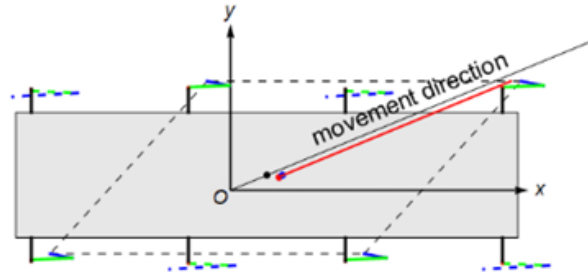
$$\Sigma_D(t) = (M + M_L)(\ddot{y}_C(t) + g_y)z_C(t) + \sum_{j=1}^4 \sum_{i=1}^3 m_i \left(\ddot{y}_i^{(Lj)}(t) + g_y \right) z_i^{(Lj)}(t) + \sum_{j=1}^4 \sum_{i=1}^3 m_i \left(\ddot{y}_i^{(Rj)}(t) + g_y \right) z_i^{(Rj)}(t),$$

$$\Sigma_E(t) = (M + M_L)(\ddot{z}_C(t) + g_z) + \sum_{j=1}^4 \sum_{i=1}^3 m_i \left(\ddot{z}_i^{(Lj)}(t) + g_z \right) + \sum_{j=1}^4 \sum_{i=1}^3 m_i \left(\ddot{z}_i^{(Rj)}(t) + g_z \right).$$

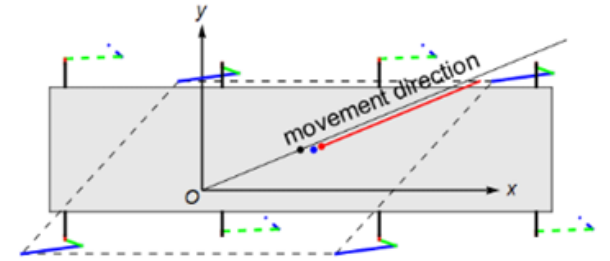
(a) phase *a* of a single robot stride



$t = 0$ s

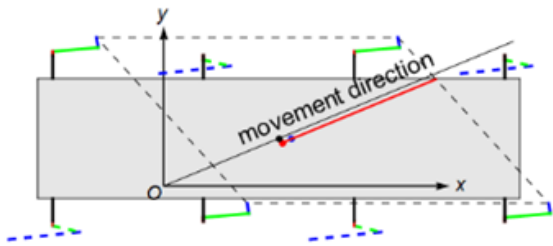


$t = 0.4$ s

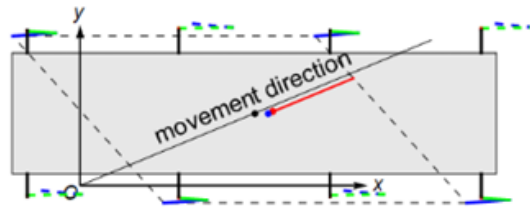


$t = 0.8$ s

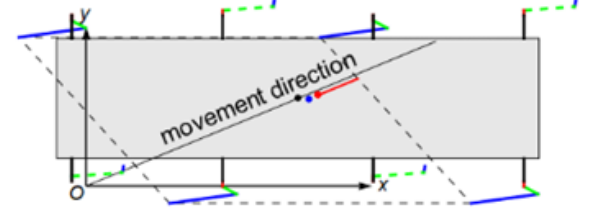
(b) phase *b* of a single robot stride



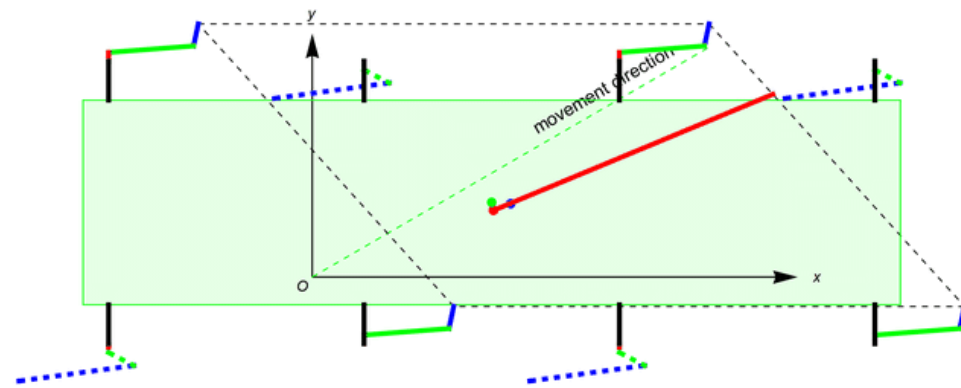
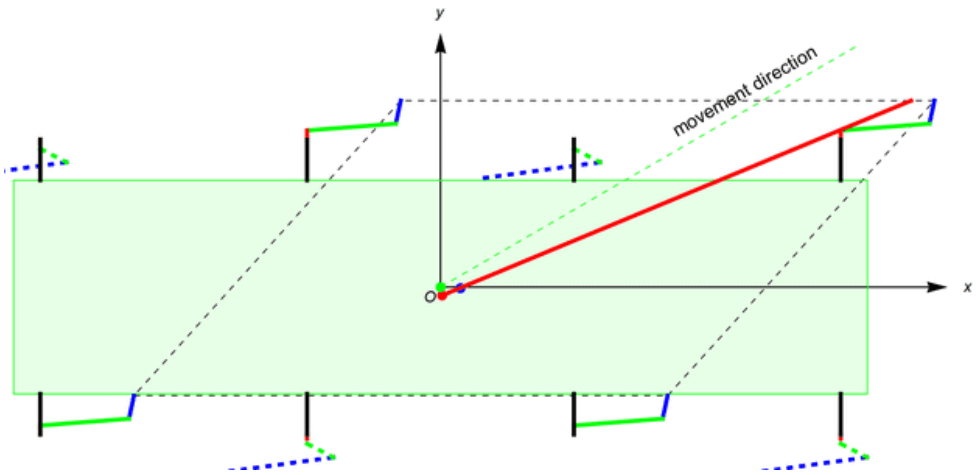
$t = 1.2$ s



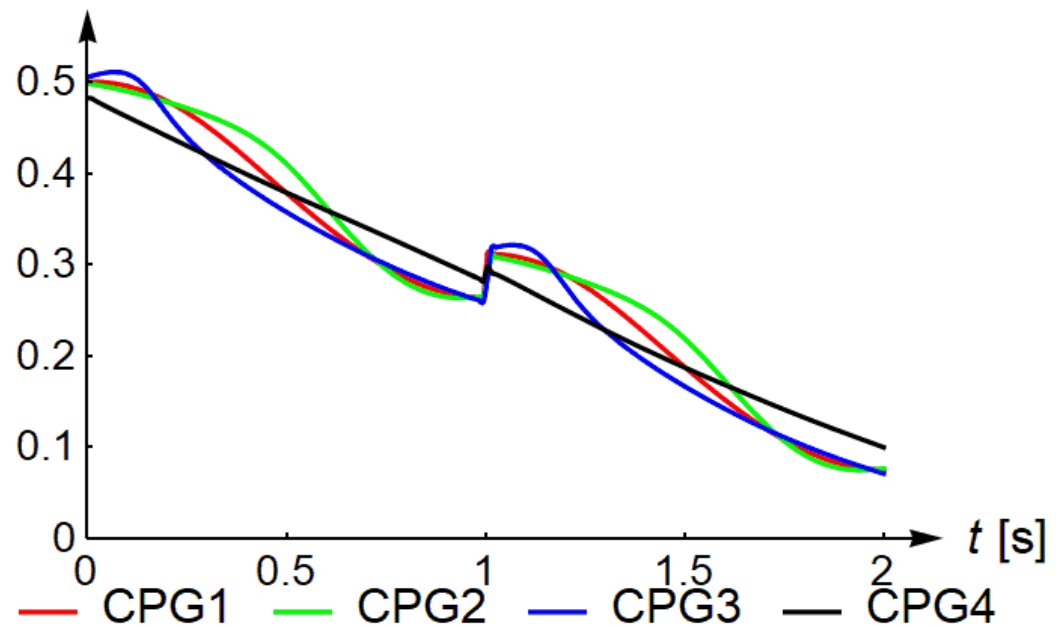
$t = 1.6$ s



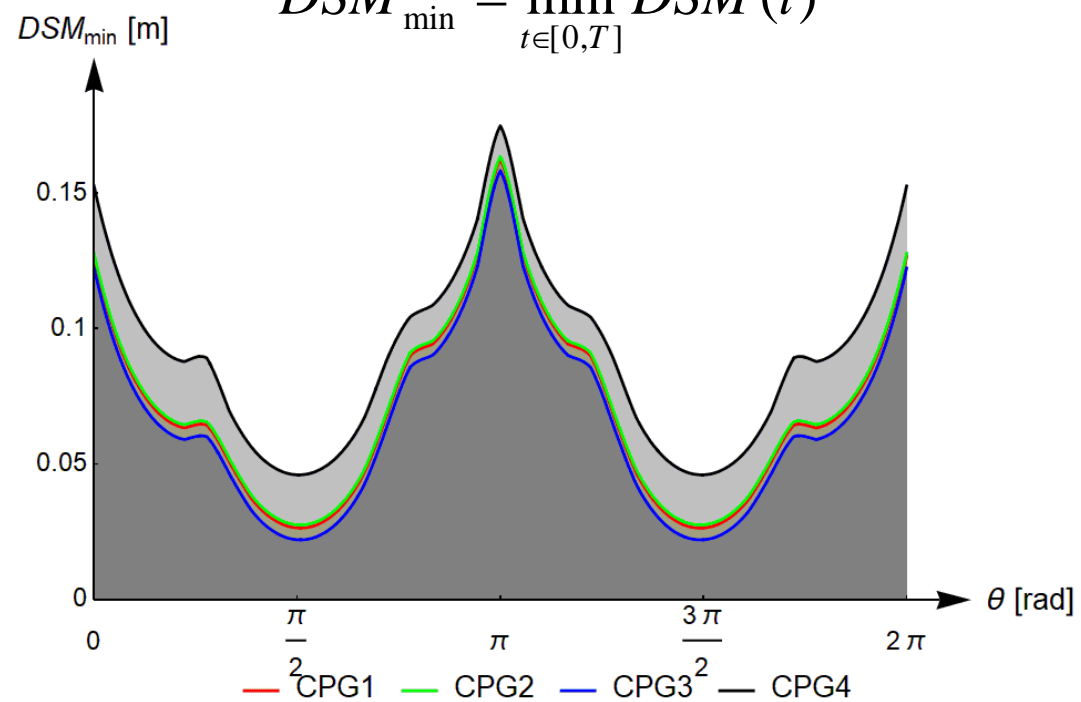
$t = 2.0$ s



$DSM(t)$ [m]



$$DSM_{\min} = \min_{t \in [0, T]} DSM(t)$$



Sily reakcji podłoża:

$$\begin{aligned} & (M + M_L) \ddot{\mathbf{r}}_C(t) + \sum_{j=1}^4 \sum_{i=1}^3 m_i \ddot{\mathbf{r}}_i^{(Lj)}(t) + \sum_{j=1}^4 \sum_{i=1}^3 m_i \ddot{\mathbf{r}}_i^{(Rj)}(t) = \\ & = \sum_{j=1}^4 \mathbf{R}^{(Lj)}(t) + \sum_{j=1}^4 \mathbf{R}^{(Rj)}(t) + \left(M + M_L + 8 \sum_{i=1}^3 m_i \right) \mathbf{g}, \end{aligned}$$

$$(M + M_L) \ddot{x}_C(t) + \sum_{j=1}^4 \sum_{i=1}^3 m_i \ddot{x}_i^{(Lj)}(t) + \sum_{j=1}^4 \sum_{i=1}^3 m_i \ddot{x}_i^{(Rj)}(t) = \sum_{j=1}^4 R_x^{(Lj)}(t) + \sum_{j=1}^4 R_x^{(Rj)}(t),$$

$$(M + M_L) \ddot{y}_C(t) + \sum_{j=1}^4 \sum_{i=1}^3 m_i \ddot{y}_i^{(Lj)}(t) + \sum_{j=1}^4 \sum_{i=1}^3 m_i \ddot{y}_i^{(Rj)}(t) = \sum_{j=1}^4 R_y^{(Lj)}(t) + \sum_{j=1}^4 R_y^{(Rj)}(t),$$

$$(M + M_L) \ddot{z}_C(t) + \sum_{j=1}^4 \sum_{i=1}^3 m_i \ddot{z}_i^{(Lj)}(t) + \sum_{j=1}^4 \sum_{i=1}^3 m_i \ddot{z}_i^{(Rj)}(t) + \left(M + M_L + 8 \sum_{i=1}^3 m_i \right) g = \sum_{j=1}^4 R_z^{(Lj)}(t) + \sum_{j=1}^4 R_z^{(Rj)}(t).$$

Założenia:

$$R_x^{(L1)}(t) = R_x^{(L3)}(t) = R_x^{(R2)}(t) = R_x^{(R4)}(t) = R_{ax}(t)$$

$$R_x^{(L2)}(t) = R_x^{(L4)}(t) = R_x^{(R1)}(t) = R_x^{(R3)}(t) = R_{bx}(t)$$

$$R_y^{(L1)}(t) = R_y^{(L3)}(t) = R_y^{(R2)}(t) = R_y^{(R4)}(t) = R_{ay}(t)$$

$$R_y^{(L2)}(t) = R_y^{(L4)}(t) = R_y^{(R1)}(t) = R_y^{(R3)}(t) = R_{by}(t)$$

$$R_z^{(L1)}(t) = R_z^{(L3)}(t) = R_z^{(R2)}(t) = R_z^{(R4)}(t) = R_{az}(t)$$

$$R_z^{(L2)}(t) = R_z^{(L4)}(t) = R_z^{(R1)}(t) = R_z^{(R3)}(t) = R_{bz}(t)$$

$$\mu_{ax}(t) = \frac{R_{ax}(t)}{R_{az}(t)}$$

$$\mu_{ay}(t) = \frac{R_{ay}(t)}{R_{az}(t)}$$



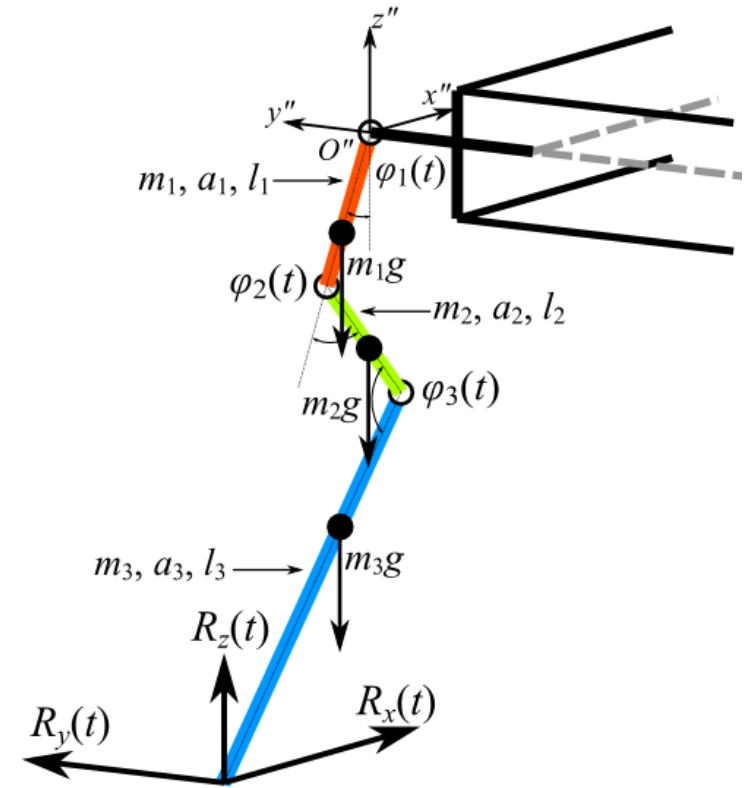
$$\mu_a(t) = \frac{\sqrt{R_{ax}^2(t) + R_{ay}^2(t)}}{R_{az}(t)}$$

$$\mu_{bx}(t) = \frac{R_{bx}(t)}{R_{bz}(t)}$$

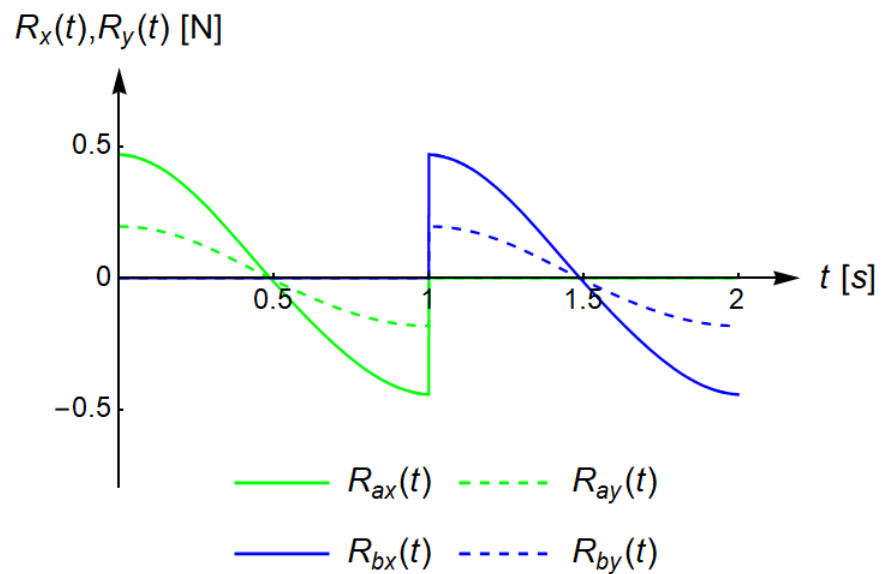
$$\mu_{by}(t) = \frac{R_{by}(t)}{R_{bz}(t)}$$



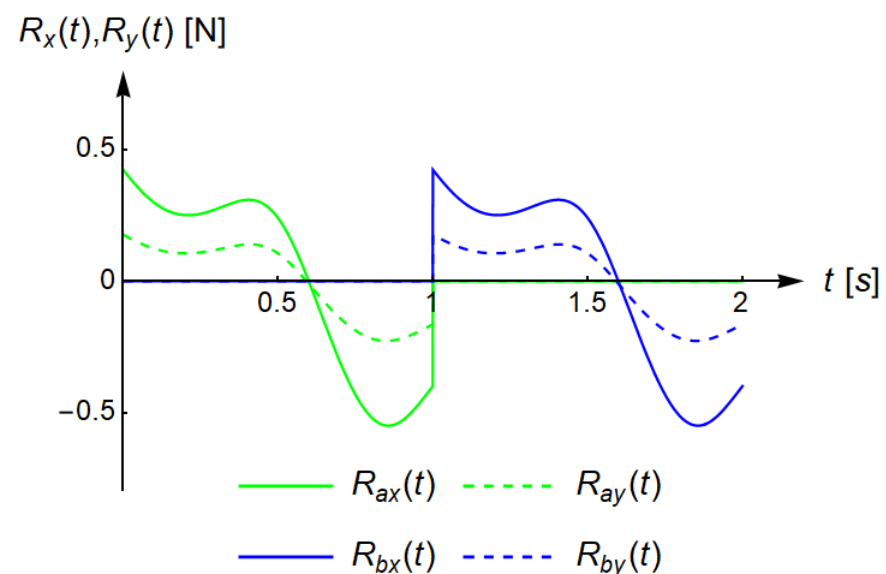
$$\mu_b(t) = \frac{\sqrt{R_{bx}^2(t) + R_{by}^2(t)}}{R_{bz}(t)}$$



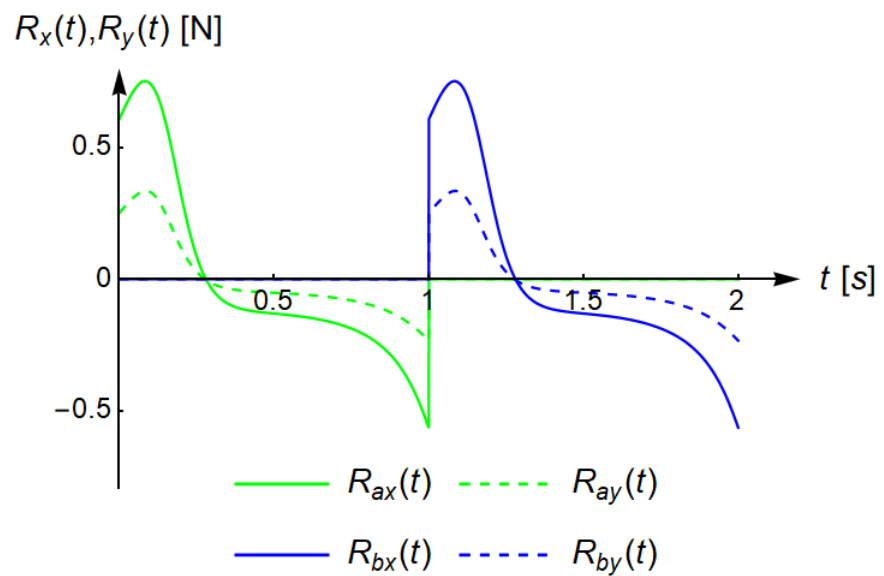
CPG1



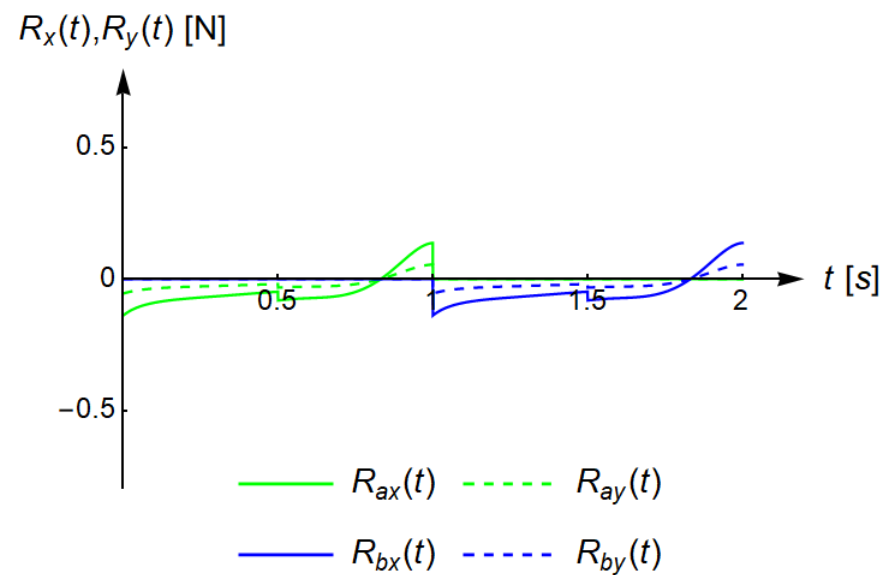
CPG2



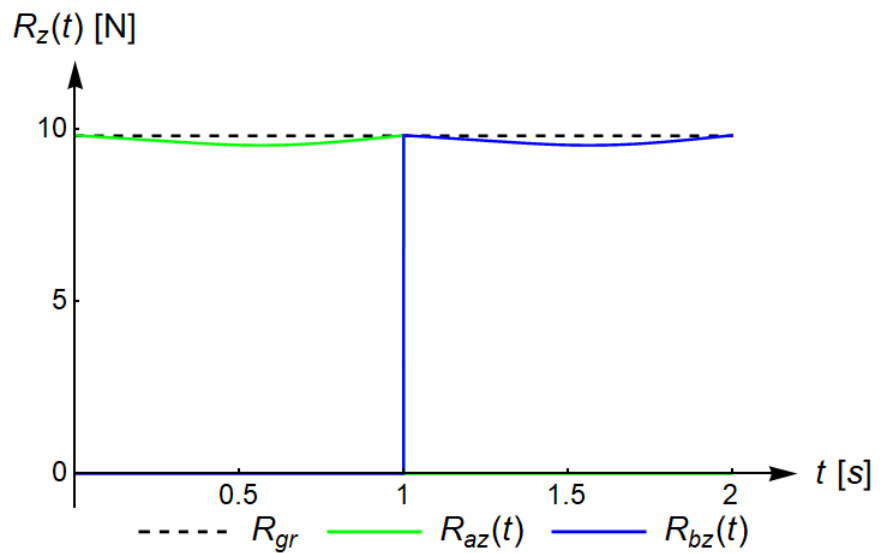
CPG3



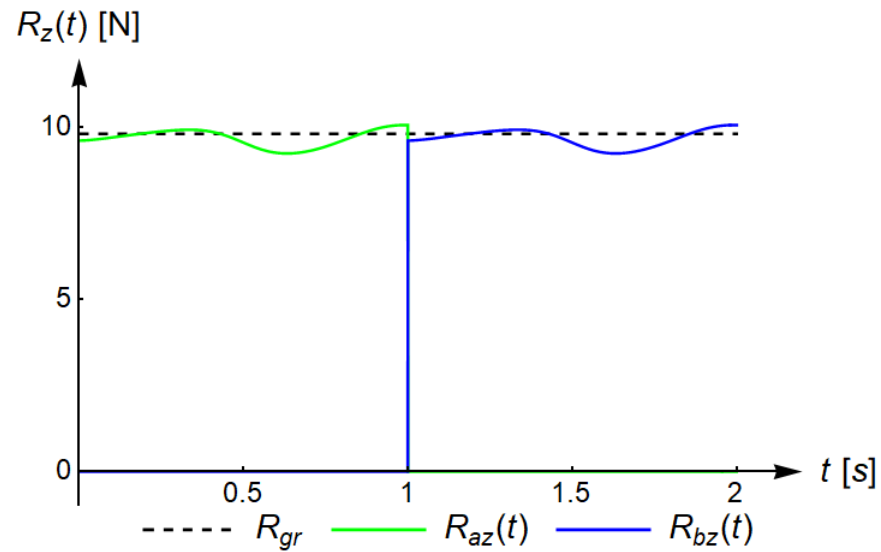
CPG4



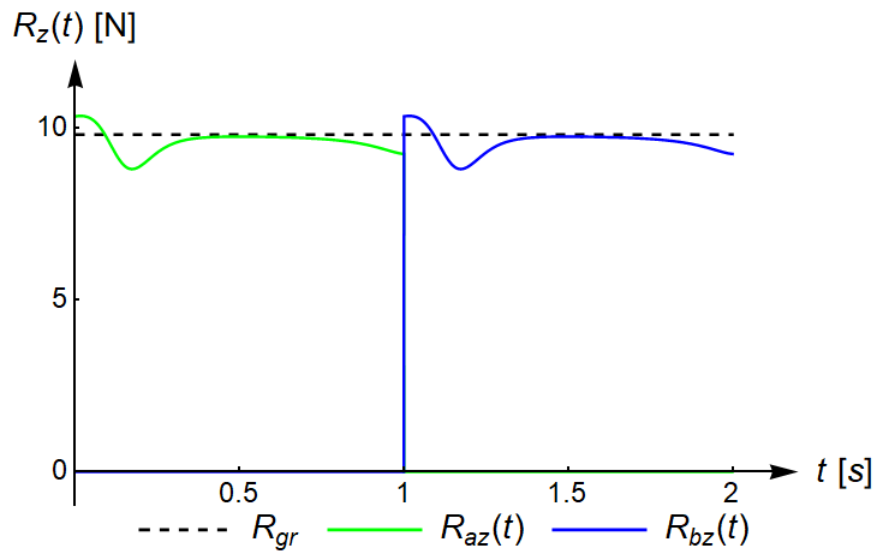
CPG1



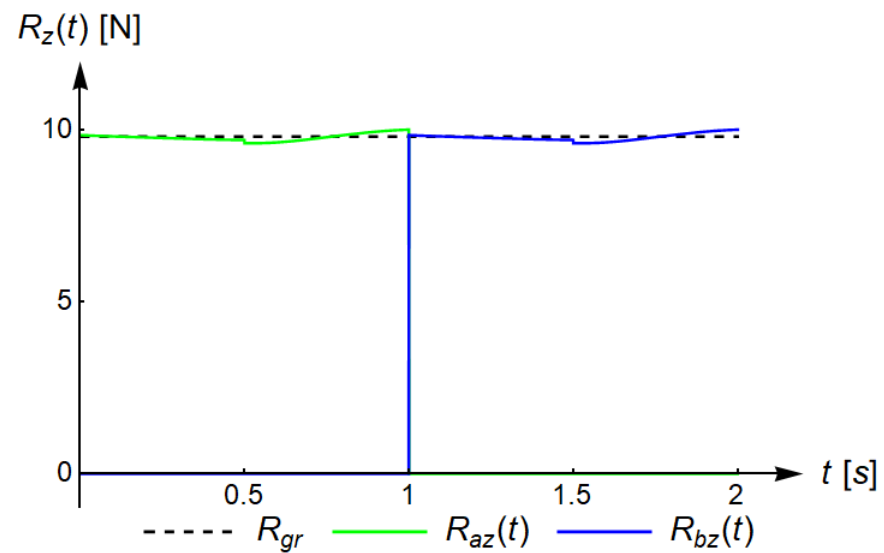
CPG2



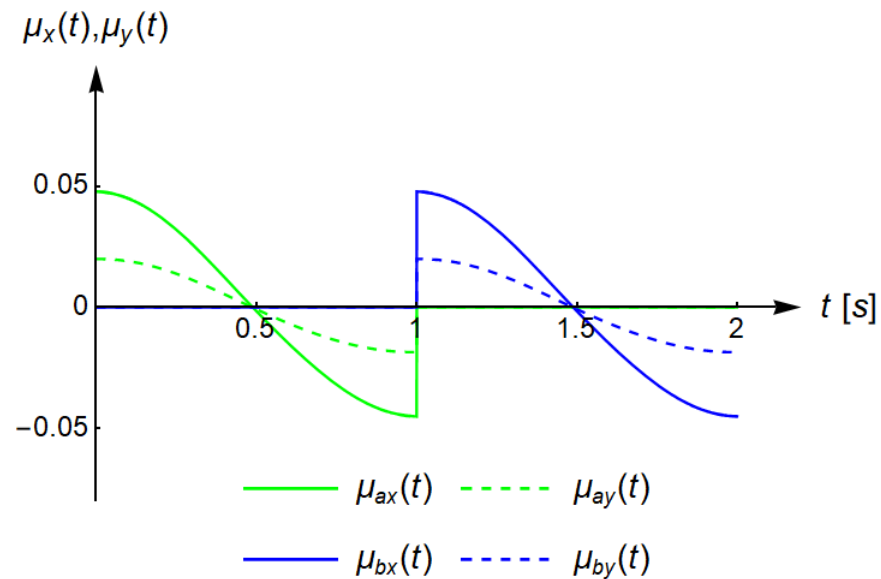
CPG3



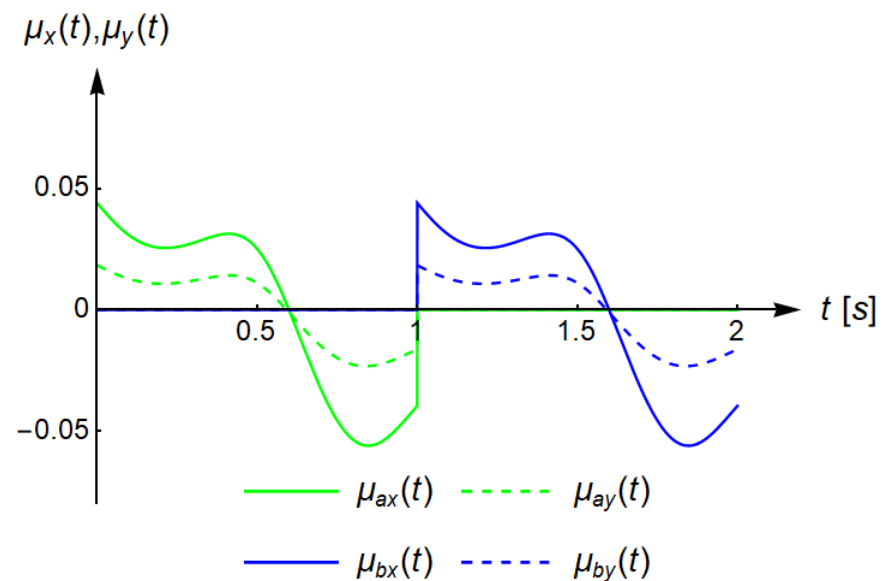
CPG4



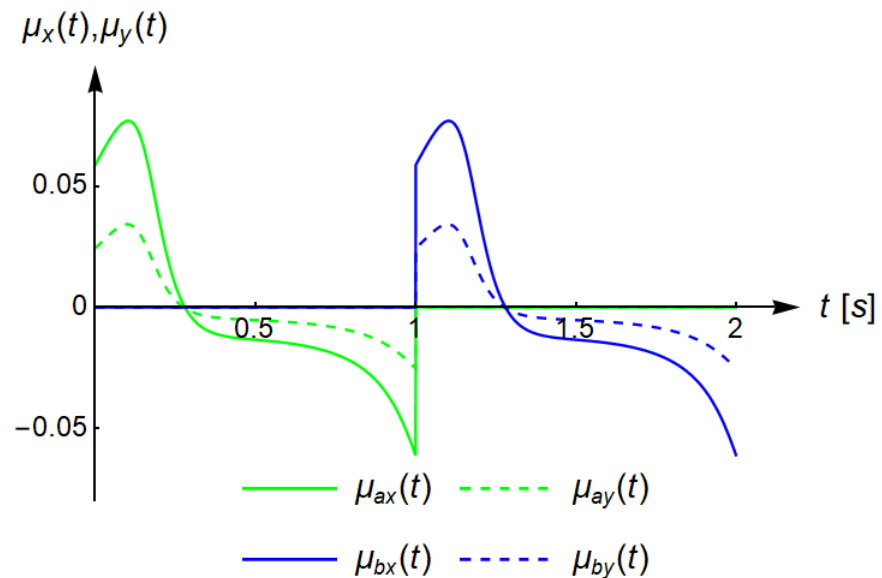
CPG1



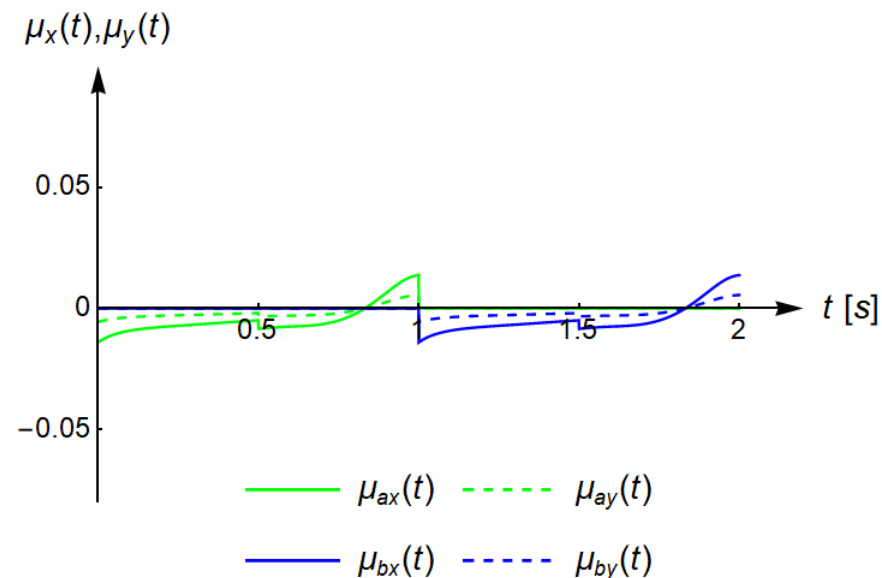
CPG2

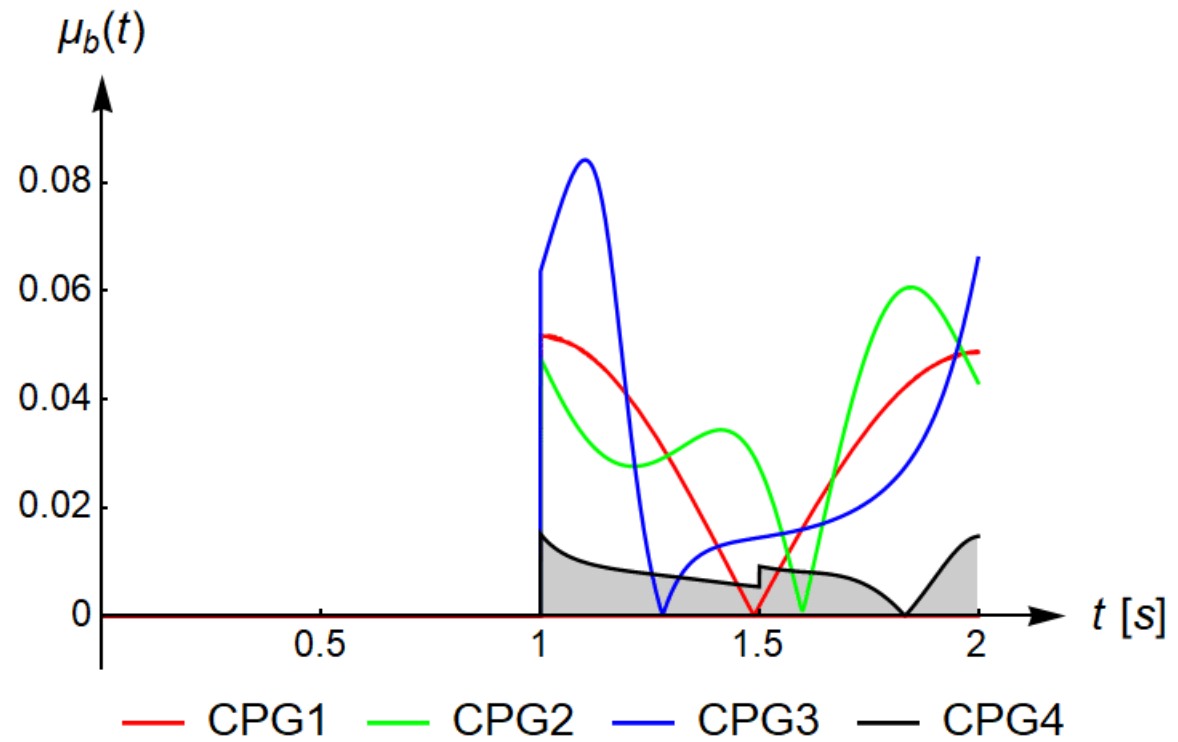
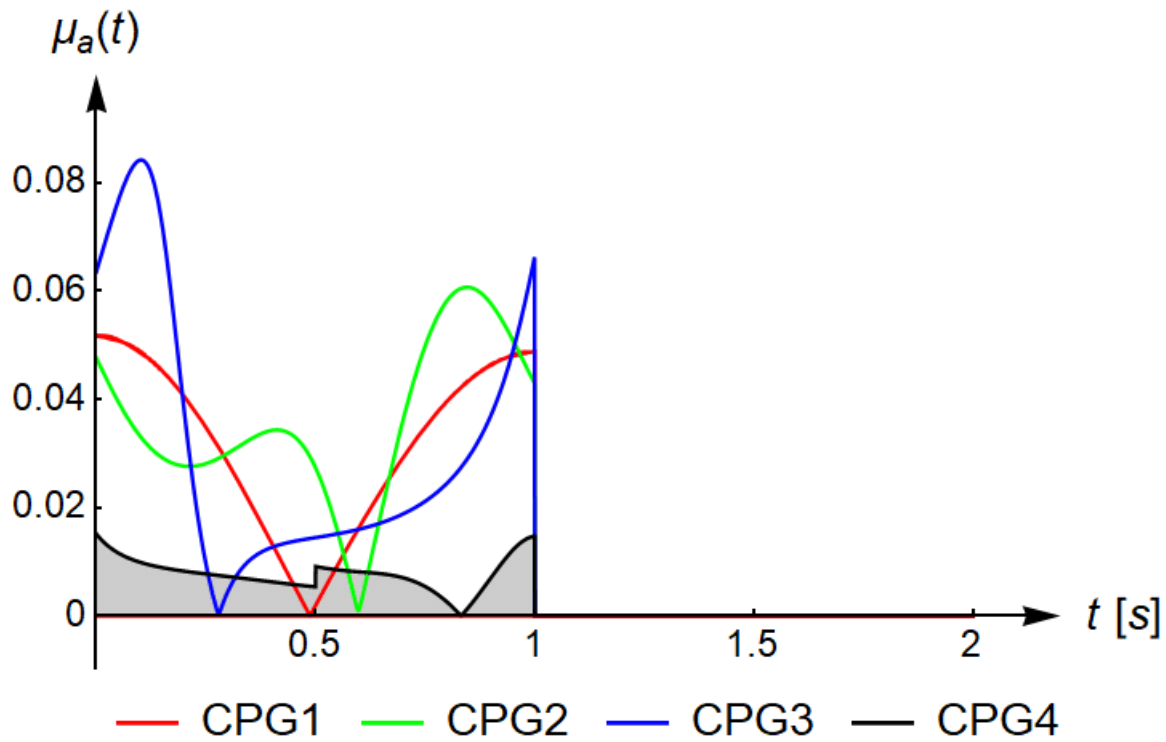


CPG3

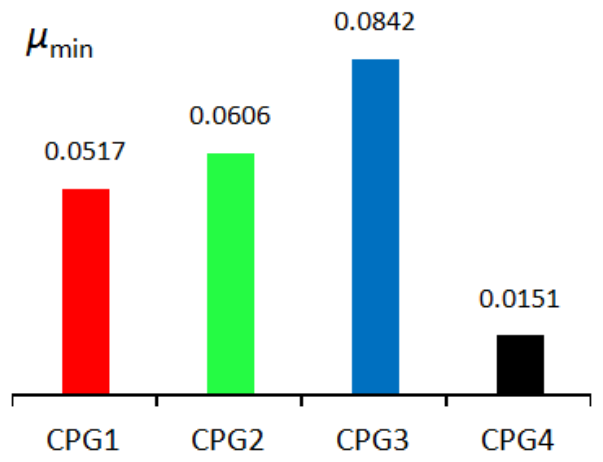


CPG4



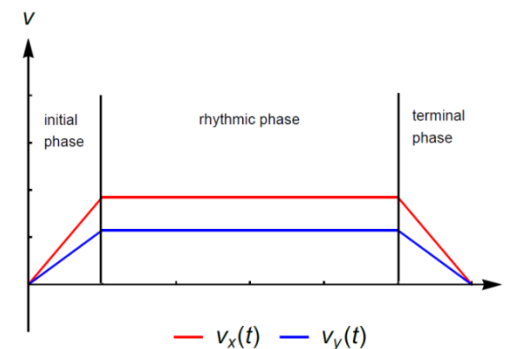
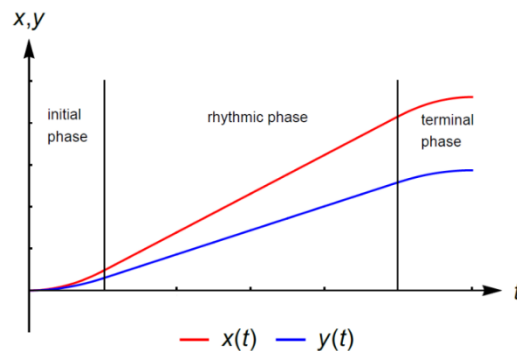


$$\mu_{\min} = \max_{t \in [0, T]} \mu_a(t) = \max_{t \in [0, T]} \mu_b(t)$$

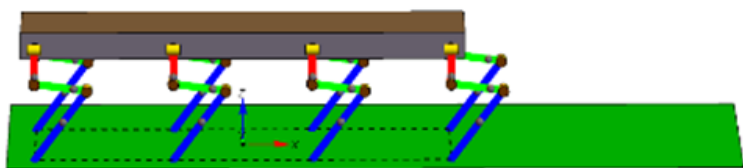


$$\theta = \pi/8$$

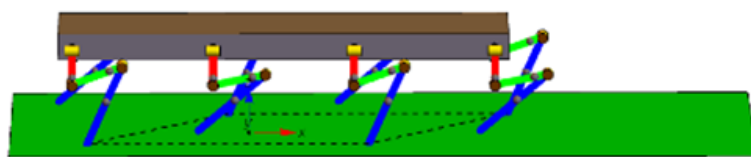
$$P(t) = \begin{cases} \frac{2}{T}t & \text{if } t \in [0, 0.5T], \\ 1 & \text{if } t \in (0.5T, (n+0.5)T], \\ 1 - \frac{2}{T}(t - (n+0.5)T) & \text{if } t \in ((n+0.5)T, (n+1)T]. \end{cases}$$



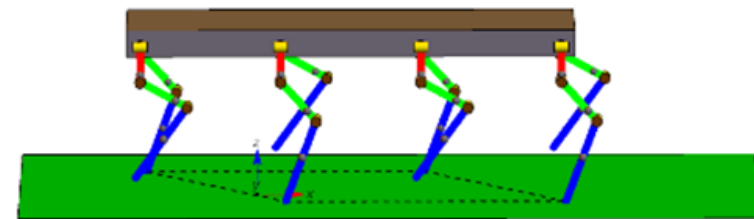
$$h(t) = (0.21 - 0.1e^{-0.3t}\sin 2t + 0.015t) \text{ m}$$



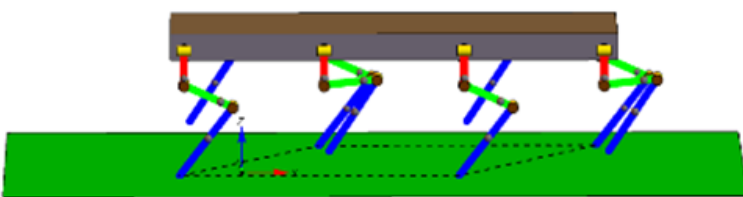
$t = 0 \text{ s}$



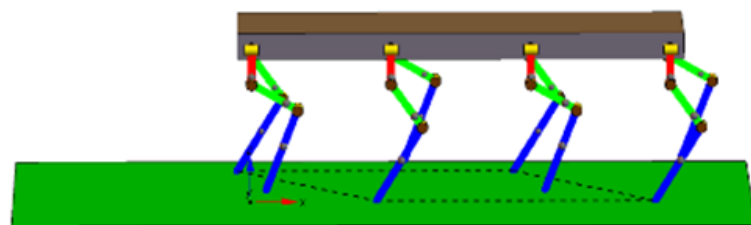
$t = 1.2 \text{ s}$



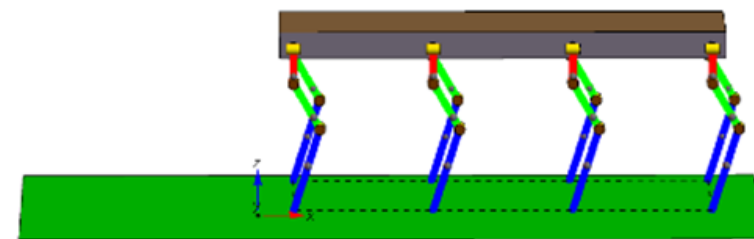
$t = 2.4 \text{ s}$



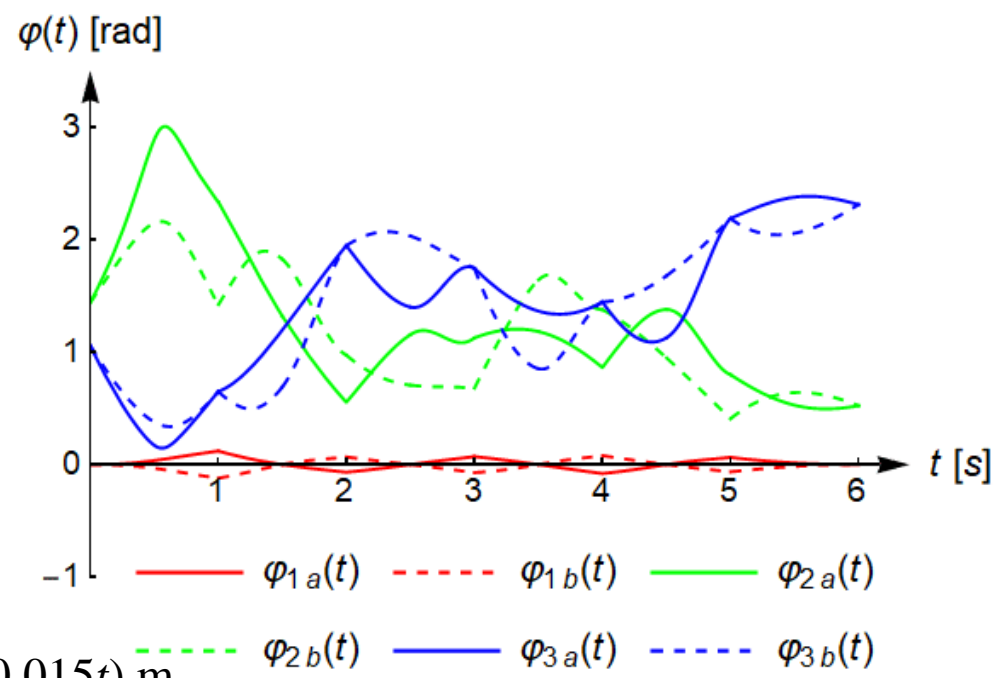
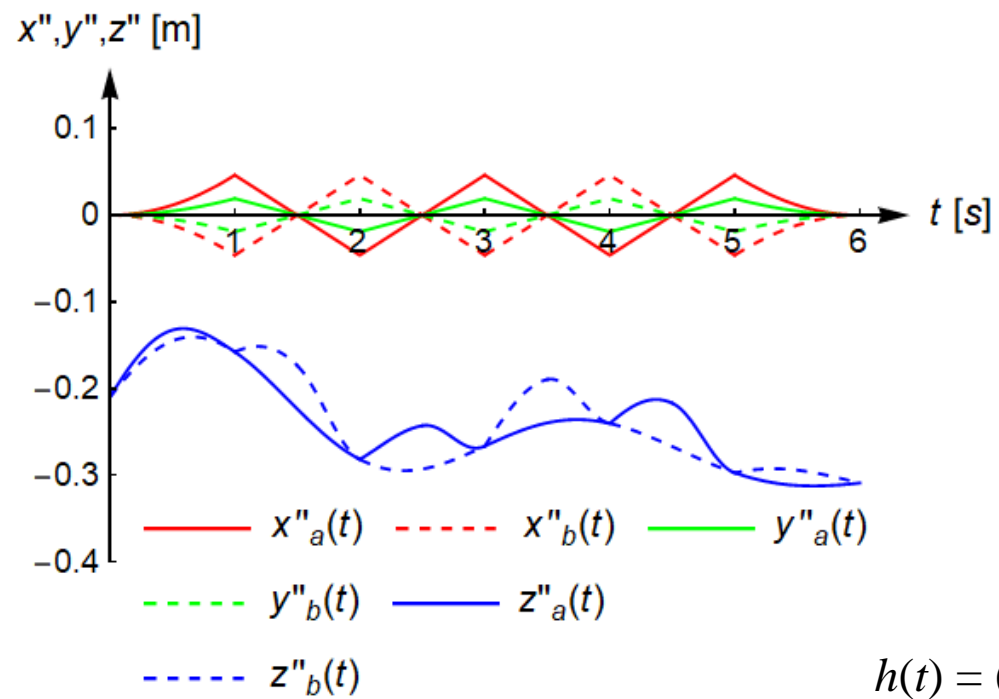
$t = 3.6 \text{ s}$



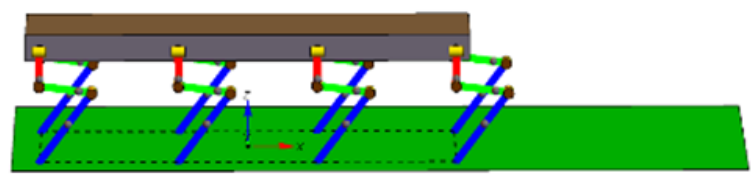
$t = 4.8 \text{ s}$



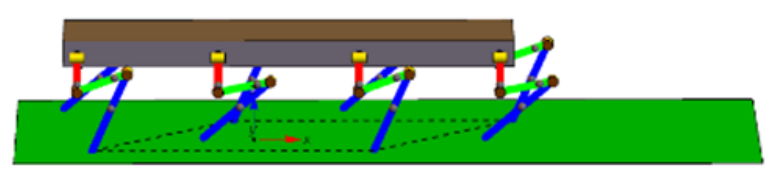
$t = 6 \text{ s}$



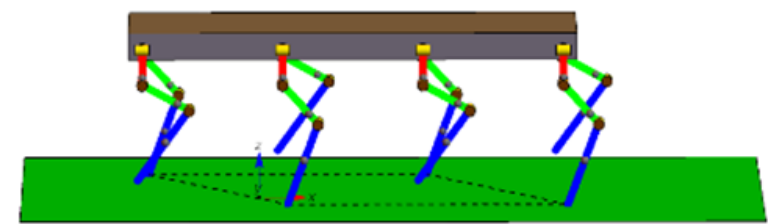
$$h(t) = (0.21 - 0.1e^{-0.3t}\sin 2t + 0.015t) \text{ m}$$



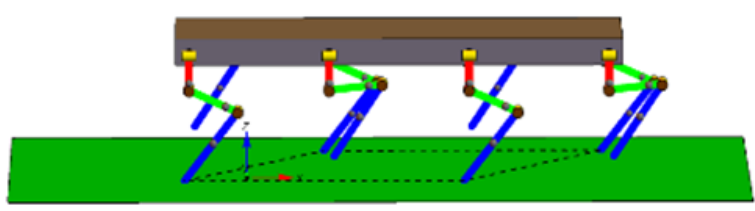
$t = 0 \text{ s}$



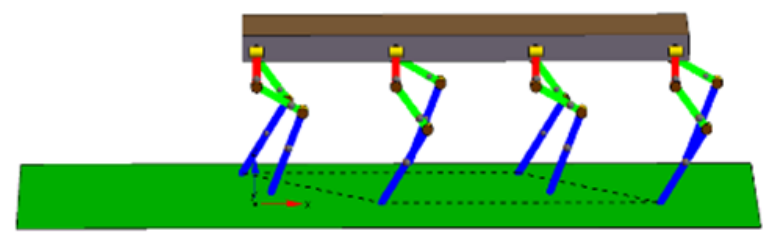
$t = 1.2 \text{ s}$



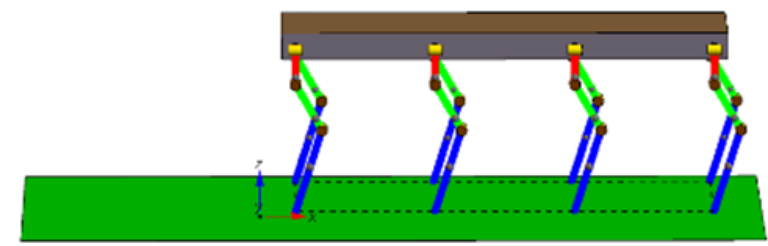
$t = 2.4 \text{ s}$



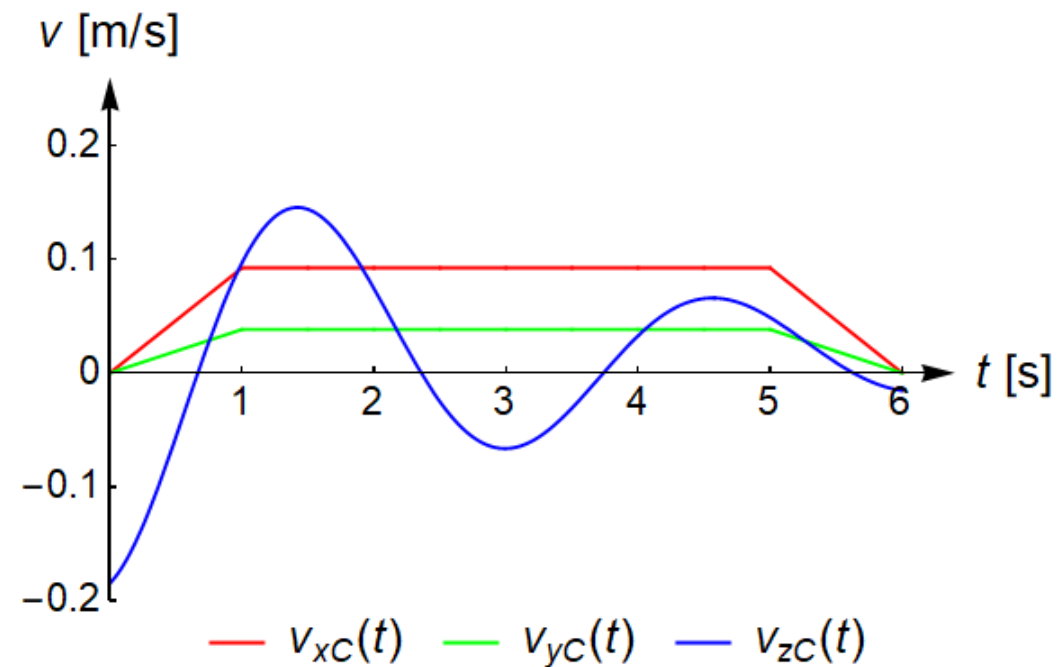
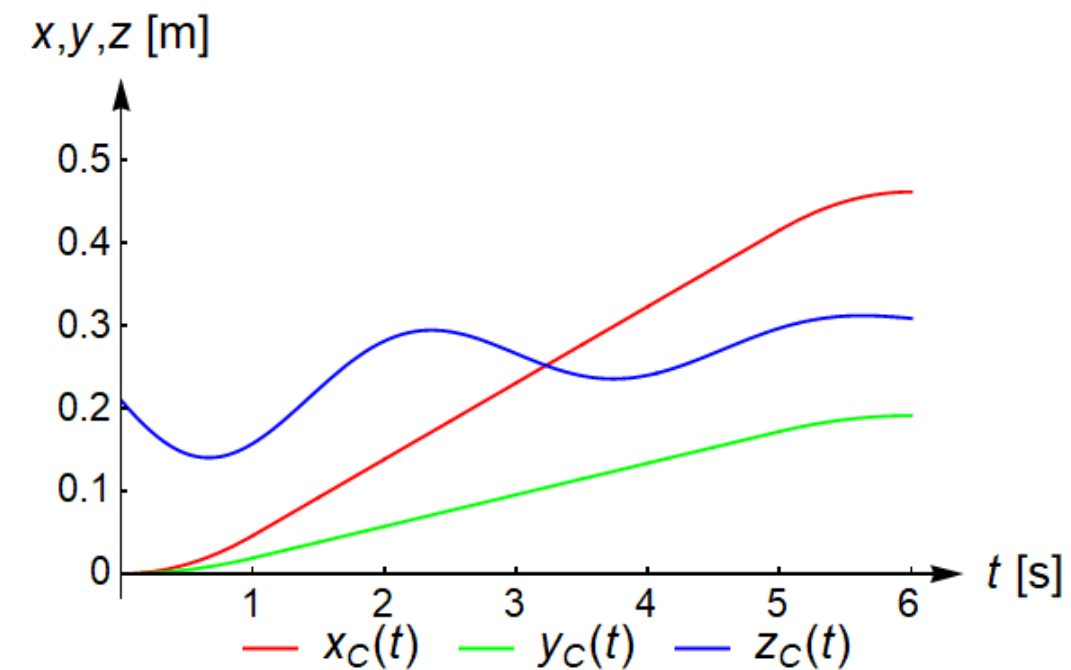
$t = 3.6 \text{ s}$



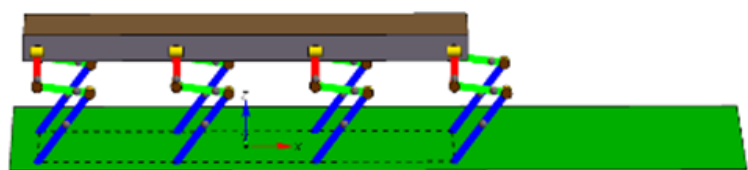
$t = 4.8 \text{ s}$



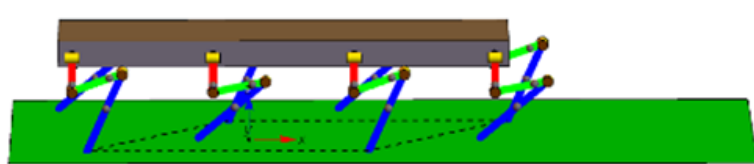
$t = 6 \text{ s}$



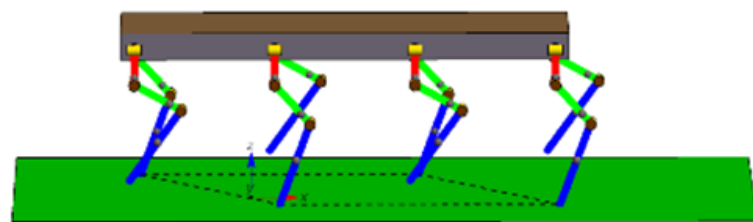
$$h(t) = (0.21 - 0.1e^{-0.3t}\sin 2t + 0.015t) \text{ m}$$



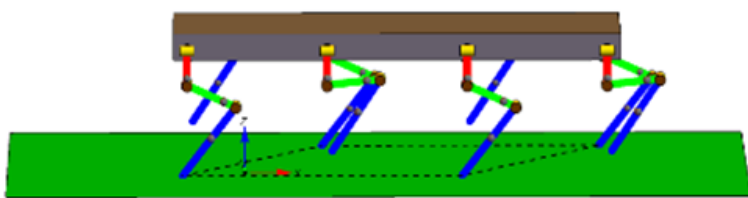
$t = 0 \text{ s}$



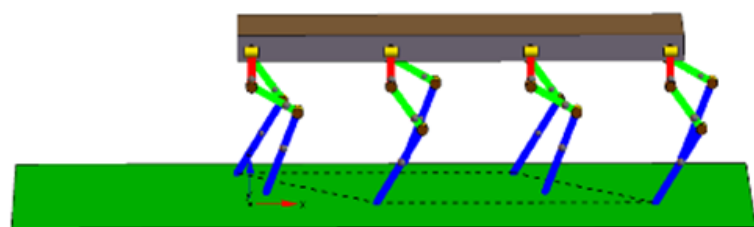
$t = 1.2 \text{ s}$



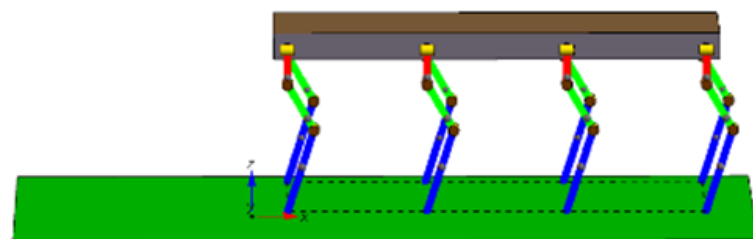
$t = 2.4 \text{ s}$



$t = 3.6 \text{ s}$

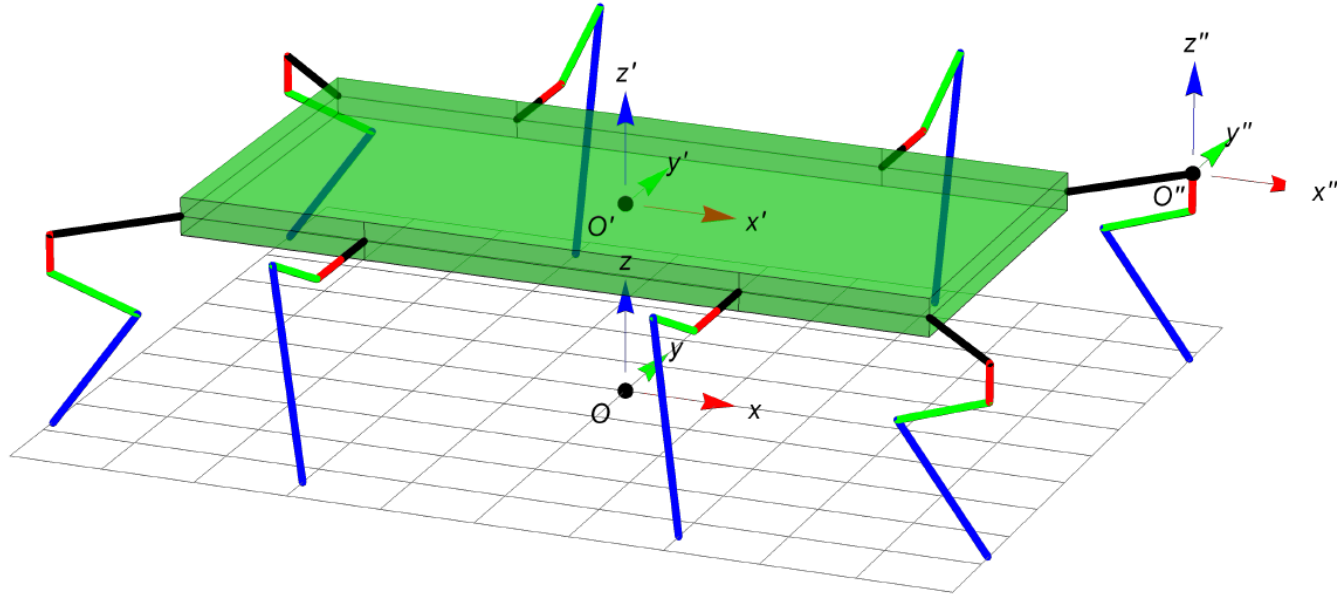


$t = 4.8 \text{ s}$



$t = 6 \text{ s}$

General model of the robot:



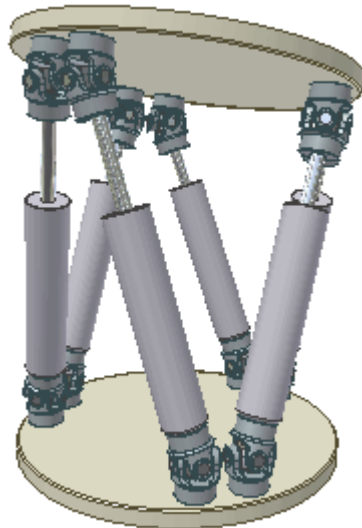
$$z = z_G(x, y, t)$$

$$\Delta \mathbf{r}_G(t) = [\Delta x_G(t), \Delta y_G(t), \Delta z_G(t)]^T$$

$$\mathbf{R}_G^{(x)}(\alpha_G(t)) = \begin{bmatrix} 1 & 0 & 0 \\ 0 & \cos \alpha_G(t) & -\sin \alpha_G(t) \\ 0 & \sin \alpha_G(t) & \cos \alpha_G(t) \end{bmatrix}$$

$$\mathbf{R}_G^{(y)}(\beta_G(t)) = \begin{bmatrix} \cos \beta_G(t) & 0 & \sin \beta_G(t) \\ 0 & 1 & 0 \\ -\sin \beta_G(t) & 0 & \cos \beta_G(t) \end{bmatrix}$$

$$\mathbf{R}_G^{(z)}(\gamma_G(t)) = \begin{bmatrix} \cos \gamma_G(t) & -\sin \gamma_G(t) & 0 \\ \sin \gamma_G(t) & \cos \gamma_G(t) & 0 \\ 0 & 0 & 1 \end{bmatrix}$$



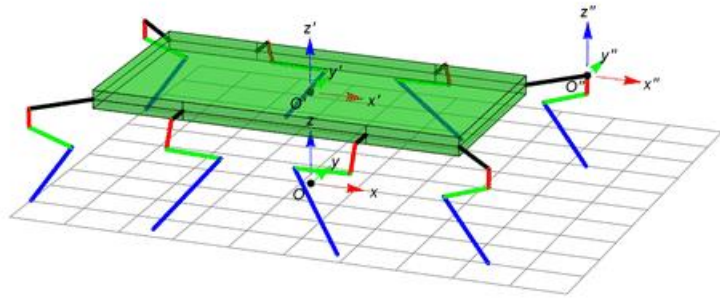
$$\mathbf{R}_R^{(x)}(\alpha_R(t)) = \begin{bmatrix} 1 & 0 & 0 \\ 0 & \cos \alpha_R(t) & -\sin \alpha_R(t) \\ 0 & \sin \alpha_R(t) & \cos \alpha_R(t) \end{bmatrix}$$

$$\mathbf{R}_R^{(y)}(\beta_R(t)) = \begin{bmatrix} \cos \beta_R(t) & 0 & \sin \beta_R(t) \\ 0 & 1 & 0 \\ -\sin \beta_R(t) & 0 & \cos \beta_R(t) \end{bmatrix}$$

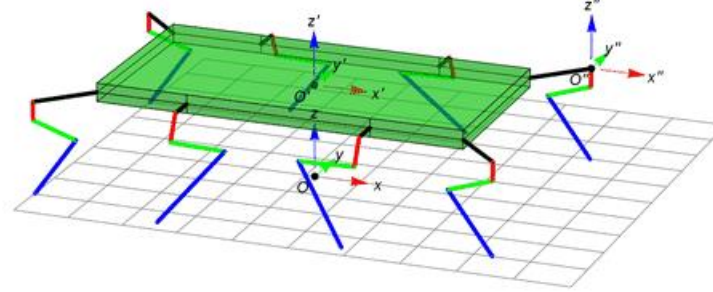
$$\mathbf{R}_R^{(z)}(\gamma_R(t)) = \begin{bmatrix} \cos \gamma_R(t) & -\sin \gamma_R(t) & 0 \\ \sin \gamma_R(t) & \cos \gamma_R(t) & 0 \\ 0 & 0 & 1 \end{bmatrix}$$

$$\Delta \mathbf{r}_R(t) = [\Delta x_R(t), \Delta y_R(t), \Delta z_R(t)]^T$$

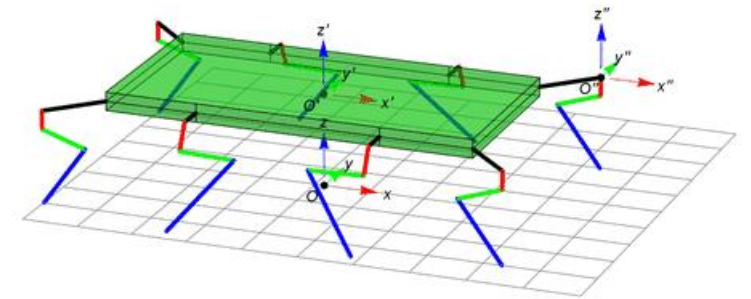
Control during standing



$$\Delta\alpha_R(t) \neq 0$$

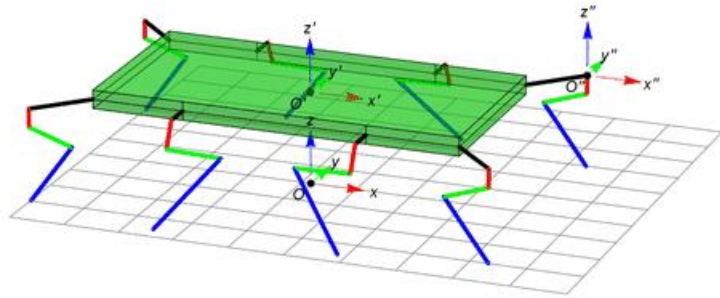


$$\Delta\beta_R(t) \neq 0$$

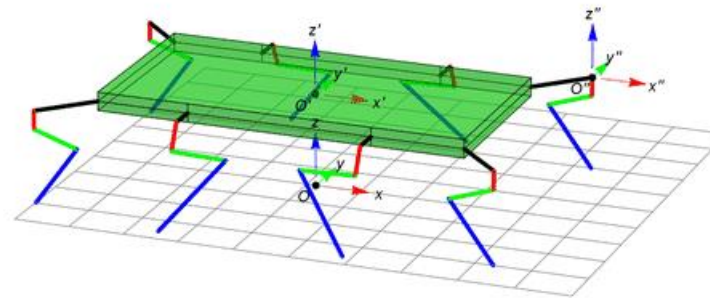


$$\Delta\gamma_R(t) \neq 0$$

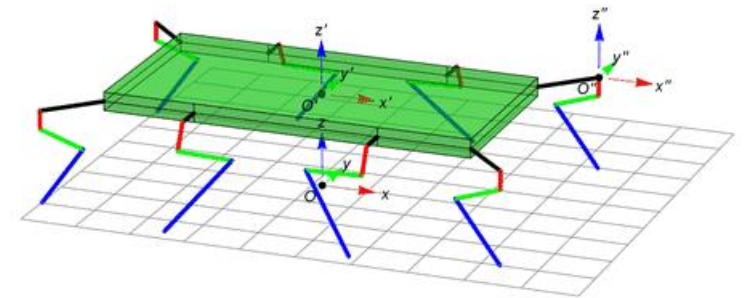
Control during walking



$$\Delta\alpha_R(t) \neq 0$$

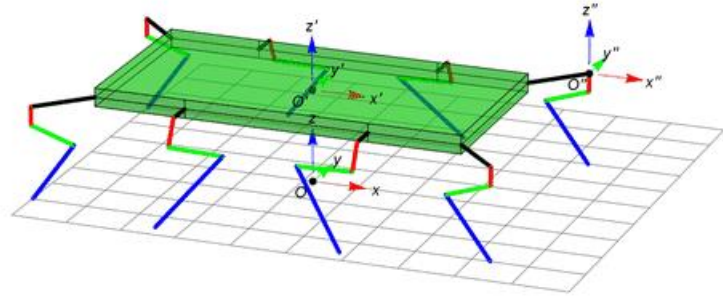


$$\Delta\beta_R(t) \neq 0$$

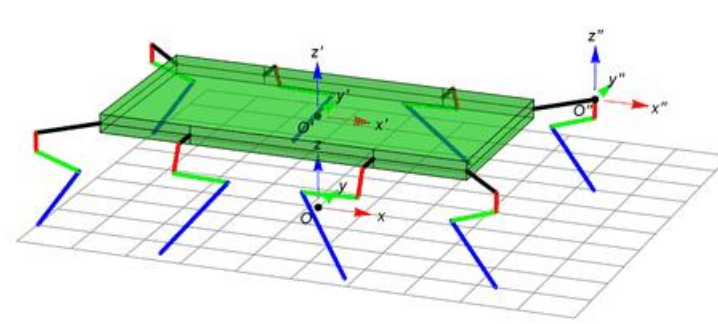


$$\Delta\gamma_R(t) \neq 0$$

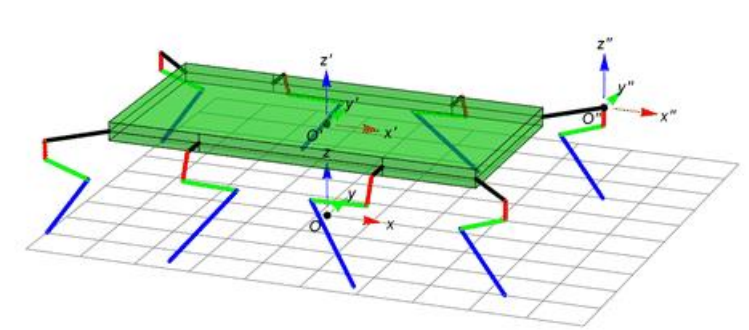
Control during standing



$$\Delta x(t) \neq 0$$

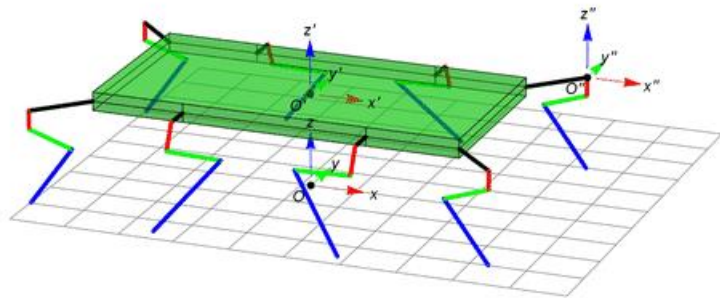


$$\Delta y(t) \neq 0$$

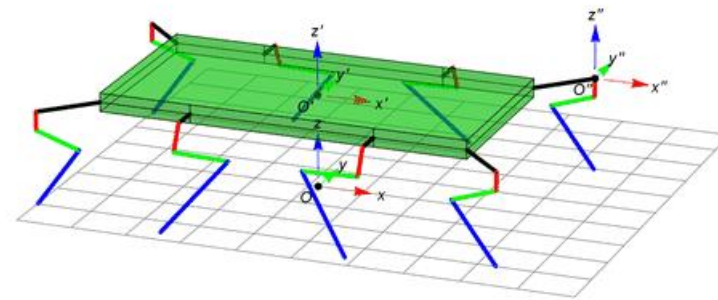


$$\Delta z(t) \neq 0$$

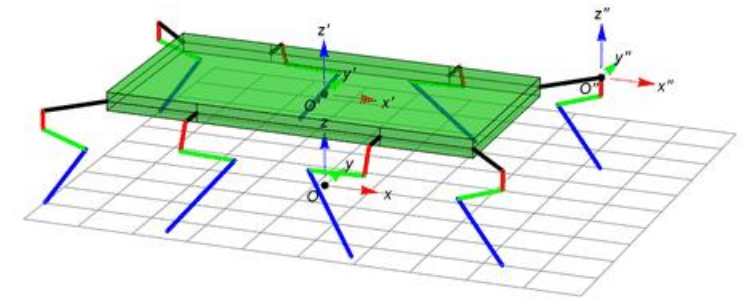
Control during walking



$$\Delta x(t) \neq 0$$

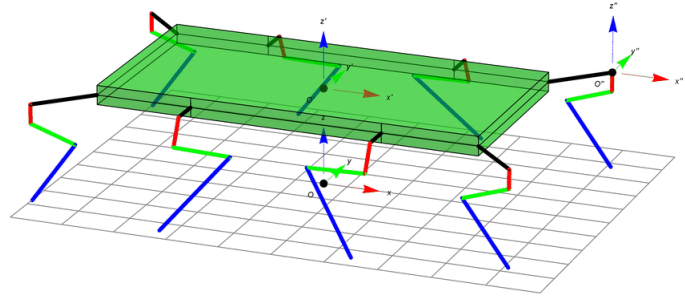


$$\Delta y(t) \neq 0$$

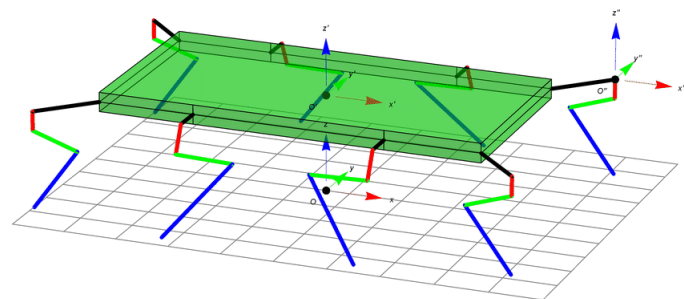


$$\Delta z(t) \neq 0$$

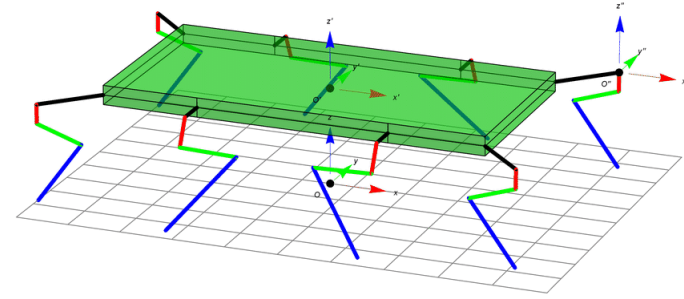
Control on vibrating ground



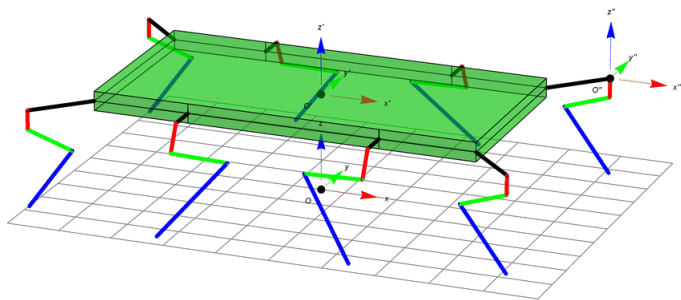
$$\Delta\alpha_R(t) \neq 0$$



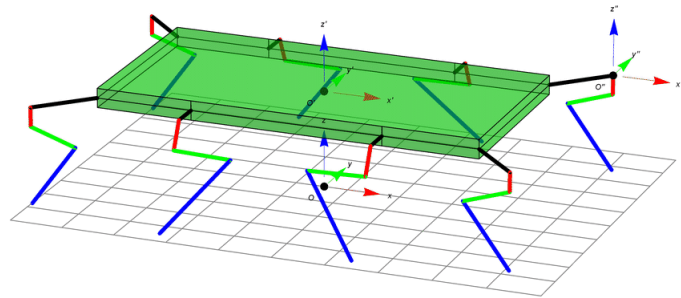
$$\Delta\beta_R(t) \neq 0$$



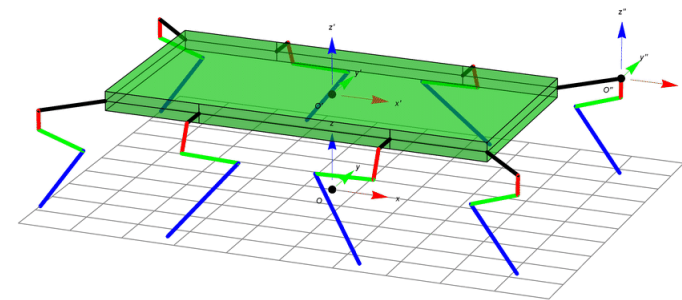
$$\Delta\gamma_R(t) \neq 0$$



$$\Delta x(t) \neq 0$$



$$\Delta y(t) \neq 0$$



$$\Delta z(t) \neq 0$$

